AMENDED AND RESTATED

LOS REYES PROJECT

Prepared under the supervision of:

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Report date: June 27, 2025

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1. SUMMARY

Prime Mining Corp. ("Prime" or the "Company") has contracted John Sims, CPG ("Independent QP") to prepare a technical report (the "Technical Report") for its wholly owned Los Reyes Project (the "Project" or the "Property") located in the states of Sinaloa and Durango, México. Mr. Sims visited the property in November 2022.

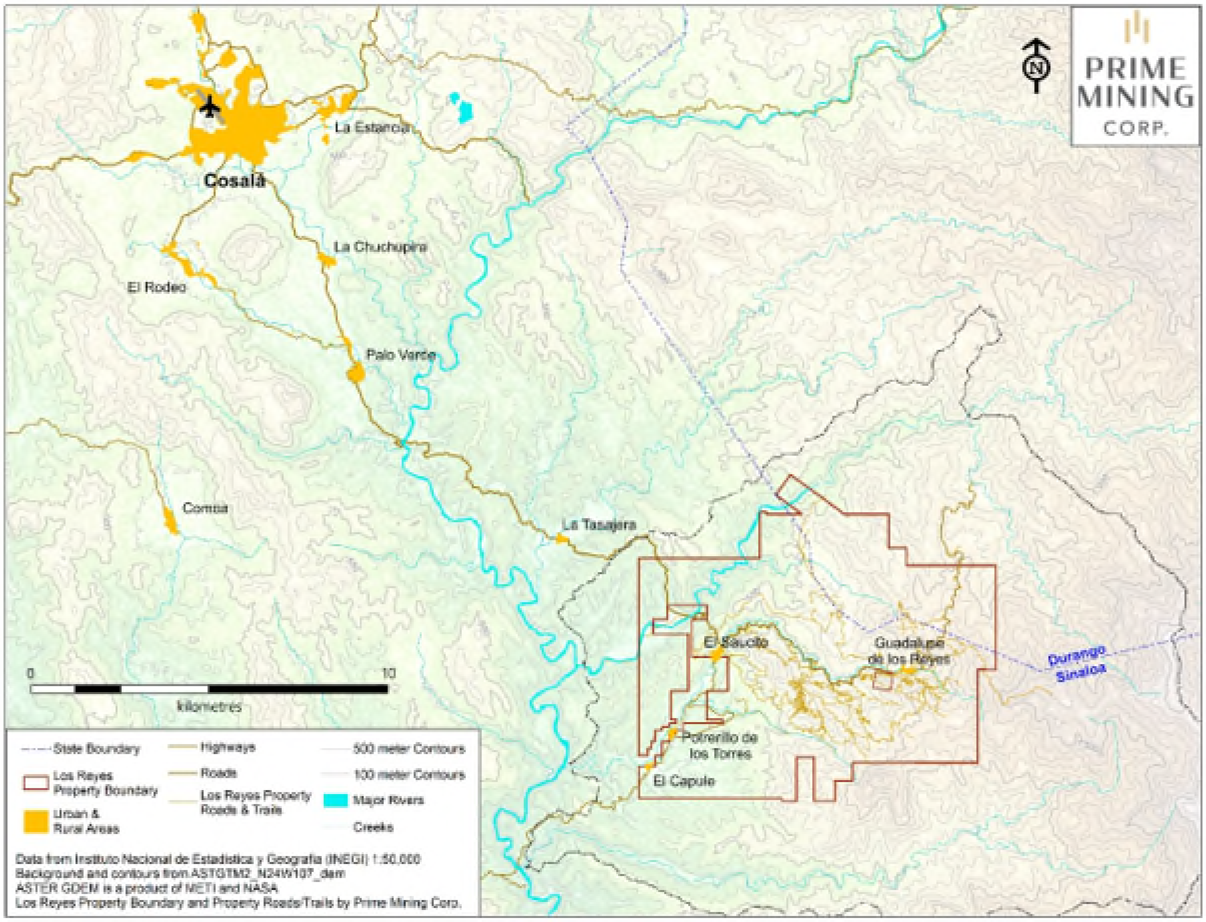
Prime is using this Technical Report to support disclosure of an updated mineral resource estimate (the "MRE") at the Project. The Technical Report conforms to National Instrument 43-101 – *Standards of Disclosure for Mineral Projects* ("NI 43-101"). The effective date of this MRE is October 15, 2024, following a drilling cutoff date of July 17, 2024. There were no material changes to the MRE between this date and the publication of this accompanying NI 43-101 Technical Report. Drilling and interpretation continue at the Project.

1.1 Property Description and Location

The Property is located north of the coastal city of Mazatlán, approximately 110 km by air and 200 km by paved highway (Figure 1-1). The Property is within the municipality of Cosalá (population 17,012) and the closest city to the Property is Cosalá (population 7,888, INEGI 2020) which is located 30 km to the northwest of the Property and connected by a gravel road. En route to the Property from Cosalá are the villages of Palo Verde and La Tasajera. The village of Guadalupe de Los Reyes is on the Property and was the site of Spanish colonial mining (Figure 1-2). The general geographic coordinates of the Property are N-24°17´ and W-106°32' (UTM Zone 13 North 344250E, 2686400N). Coordinates are in WGS 84.

Figure 1-1 Los Reyes General Location

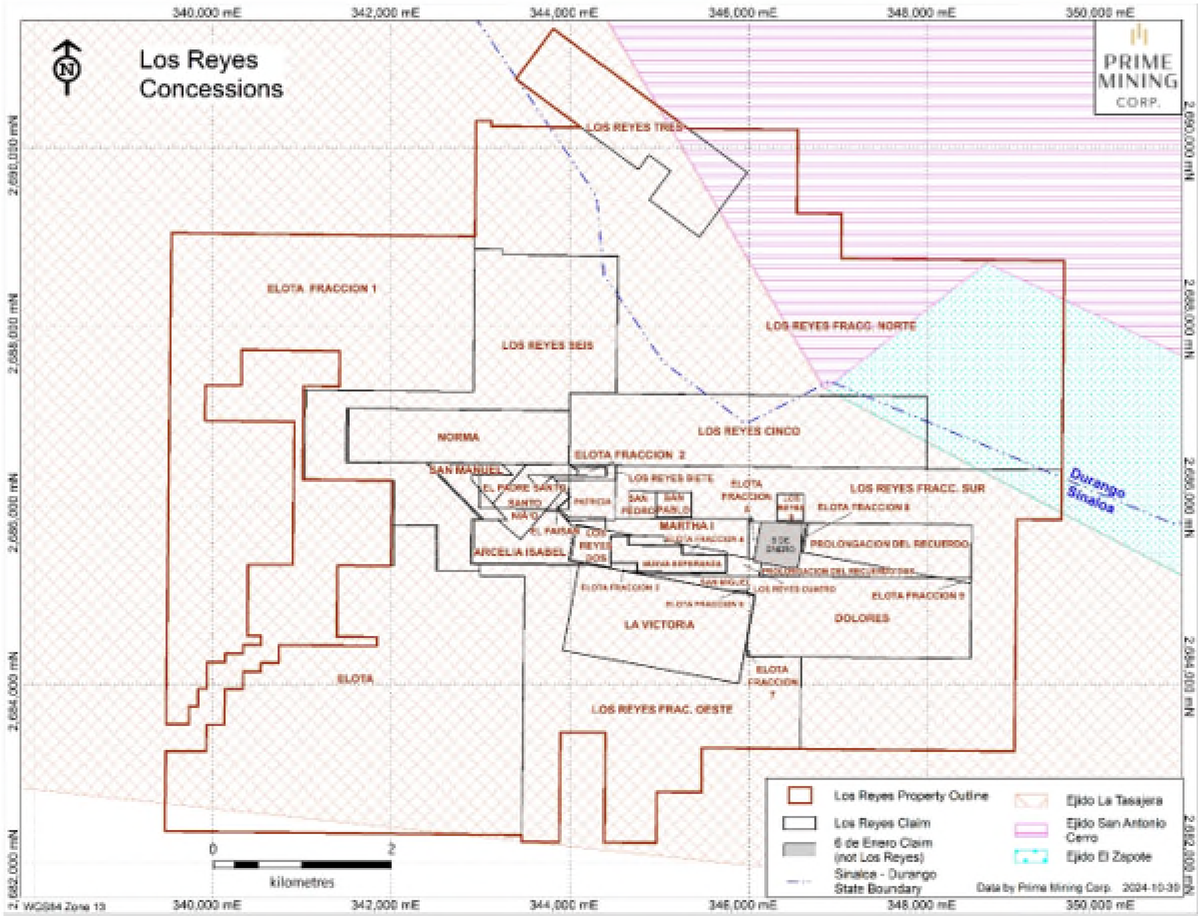
Figure 1-2 Los Reyes Property Location



1.2 Ownership and History

Prime acquired the Property by purchasing a Minera Alamos Inc. ("MAI") option agreement on their Vista Gold owned property in 2019. Prime owns 100% of the Property subject to various royalties and/or NSRs (as defined below). The Project is comprised of 37 contiguous mining concessions that have a combined area of 6,273 hectares (Figure 1-3).

Figure 1-3 Los Reyes Concessions



Several previous owners completed surface mapping, surface sampling, drilling, and various study work on the Property. It is believed that mining in the Project area dates back to the 18th century, if not earlier.

In addition to the Property claim group, Prime applied for a 7,500 hectare claim group known as "El Rey" (see Figure 1-4) in March 2021. This claim has not yet been granted.

1.3 Geology and Mineral Resource Estimate

The Property is within the Sierra Madre Occidental ("SMO") mountain range of the North American Cordillera that extends for hundreds of kilometres from central to northern México in the Basin and Range province (Rossotti, Ferrari, López-Martinez, & Rosas-Elguere, 2002). The SMO is a large continuous sequence of volcanics from late Cretaceous to middle Tertiary in age (McDowell & McIntosh, 2012). Numerous gold and silver deposits exist within the SMO.

Near the Property, the volcanic sequence unconformably overlies a late Cretaceous-aged batholith. This overlying volcanic package is subdivided into Lower and Upper sequences that are separated by an angular unconformity. The Lower Sequence spans from late Cretaceous-early Tertiary, is approximately 1 km thick, and is predominantly composed of intermediate (andesitic) volcanics and more felsic units that are mostly dacitic to rhyolitic in composition. The upper sequence is deposited unconformably on the lower sequence and is composed of ash-flow and ash-fall tuffs that are rhyolitic to dacitic in composition. This sequence is over 1 km thick in high elevation areas.

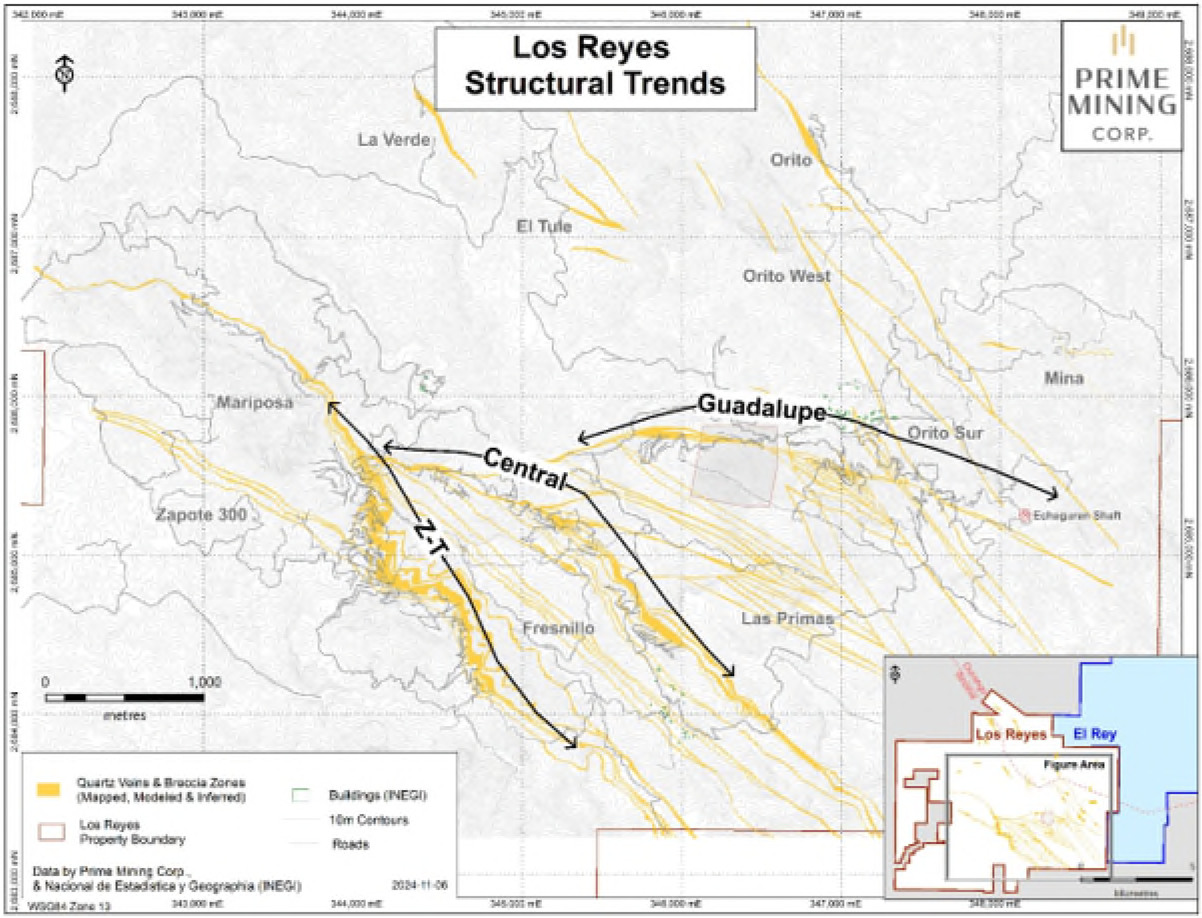
The mineralized zone is characterized by a low-sulphidation epithermal system containing silica veins, stockwork veins, and breccias. The gold and silver mineralization predominantly occurs along three northwest and west-northwest oriented silicified structural corridors (Figure 1-4). These primary mineralized structural corridors are named after the mineralized areas that they host, and are as follows:

1. The Mariposa-Zapote-Tahonitas trend (the “Z-T Trend”).
2. The central San Miguel-Noche Buena trend (the “Central Trend”).
3. The Guadalupe trend (the “Guadalupe Trend”).

Two subsidiary mineralized structures have been identified between the main mineralized structures: Las Primas, located between the Guadalupe and Central trends, and Fresnillo, located between the Z-T and Central trends.

Several other mineralized trends have been recognized including the Orito trends, which intersect the Guadalupe trend, and the Mina showing which may be on a splay proximal to the Orito trend.

Figure 1-4 Los Reyes Structural Corridors



Historical work by previous owners included soil and rock grab sampling, ground geophysics and both RC and diamond drilling. During 2019-2020, the Company completed a comprehensive trenching and roadcut sampling program. From late 2020 to the drill cutoff date of July 17, 2024, the Company completed over 191,000 metres of drilling along the primary structural corridors and several subsidiary trends, totalling more than 126,000 samples (excluding blanks, duplicates, and standards). Geological mapping at various scales has been ongoing since 2020, covering nearly the entire property and revealing dozens of previously unknown mineral showings.

Trench and roadcut sampling beginning in September 2019 through November 2020 collected systematic and continuous samples across mineralized vein systems, or along roadcut outcrop exposures that totaled over 5,000 metres. The Company has continued to collect rock samples which include adit, chip, float and grab samples as part of the geological mapping program.

Drilling in 2021 focused on confirming a few key historic drill holes, testing down dip extensions at each area and testing new and historic prospects. Drill access was hampered by poor road conditions during the first year of drilling. Prime drilled 156 holes in 2021 totalling 30,347 metres.

Drilling in 2022 continued expanding the deposit extensions both along strike and down dip as well as drill testing other showings. Improvements to the road infrastructure provided increased access, particularly to the Guadalupe East and Tahonitas deposits. In 2022, 266 drill holes were completed totaling 74,811 metres.

Drilling in 2023 and 2024 has continued expanding the deposit extensions both along strike and down dip as well as drill testing other showings. Improvements to the road infrastructure continued and allowed increased access, particularly to Las Primas and Fresnillo deposits. In 2023, 184 drill holes were completed totaling 58,896 metres. In 2024 up to the drill cutoff for this resource estimate, July 17, 2024, a total of 82 drill holes were completed totaling 30,645 metres.

The Los Reyes resource model was prepared by the Company under the supervision of Sims Resources LLC (Independent QP). Geologic and estimation domains were constructed using Leapfrog Geo v.2023.2.3, including input from geochemical analyses completed in ioGAS v.8.2. Geostatistical evaluations and Exploratory Data Analysis ("EDA"), including topcut selection, declustering, variography, and Sequential Gaussian Simulation ("SGS") were completed using X10-Geo v.1.4.18.22 and Snowden Supervisor v.9.0. Resource estimation was prepared using Leapfrog EDGE v.2023.2.3.

Gold and silver grades were interpolated into 5x5x5 m and 2.5x2.5x2.5 m block models using inverse distance cubed ("ID3") estimation techniques. Search ellipse orientation and radii were selected based on variogram models for gold ("Au") and silver ("Ag") in each estimation domain, with variable search orientation applied according to the nearest vein midpoint surface in the quartz vein and breccia model. Blocks were classified under the categories of "Indicated" and "Inferred" mineral resources, in accordance with the 2014 Canadian Institute of Mining, Metallurgy and Petroleum Standards for Mineral Resources and Mineral Reserves, Definitions and Guidelines, May 2014 (the "CIM Definition Standards"). The "Measured" resource category was not used because no modern mining has been undertaken at the Project and it is therefore not possible to reconcile the models against production or tightly spaced data such as grade control drilling.

The economic pit-constrained resource estimate was completed by Snowden Optiro. Mineral resources ("Mineral Resources") were reported below the most recent light detection and ranging ("LiDAR") topographic surface and are contained within economically constrained pit shells generated using the Hochbaum Pseudoflow algorithm implemented in Datamine's Studio NPVS or underground stope shapes generated using Datamine's Mineable Shape Optimizer ("MSO"). Open pit Mineral Resources are reported estimated using a 0.17 g/t Au-only cutoff grade, and underground Mineral Resources are reported from stopes which meet or exceed an NSR value of US$80.81/tonne. The Mineral Resources are classified as Indicated or Inferred based on drill spacing and geological continuity. Two processing methodologies were assumed: a mill to process the higher-grade blocks, and a heap leach.

See Table 1-1 for the 2024 MRE.

Table 1-1 Mineral Resource Estimate[1,2,3, 4]

Mining Method and Process	Class	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
Open Pit – Mill	Indicated	24,657	1.13	899	35.7	28,261
	Inferred	7,211	0.89	207	42.8	9,916
Underground – Mill	Indicated	4,132	3.02	402	152.4	20,243
	Inferred	4,055	2.10	273	78.6	10,247
Total Mill	**Indicated**	**28,789**	**1.41**	**1,301**	**52.4**	**48,504**
	Inferred	**11,266**	**1.33**	**480**	**55.7**	**20,163**
Open Pit - Heap Leach	Indicated	20,254	0.29	190	8.4	5,492
	Inferred	5,944	0.30	58	7.3	1,398
Total	**Indicated**	**49,042**	**0.95**	**1,491**	**34.2**	**53,995**
	Inferred	**17,210**	**0.97**	**538**	**39.0**	**21,561**

Notes:

1. Open Pit Resource estimates are based on economically constrained open pits generated using the Hochbaum Pseudoflow algorithm in Datamine's Studio NPVS and the following optimization parameters (all dollar values are in US dollars):
    - $1,950/ounce gold price and $25.24/ounce silver price.
    - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
    - Heap leach recoveries of 73% and 25% for gold and silver, respectively.
    - Pit slopes by area ranging from 42-47 degrees overall slope angle.
    - 5% ore loss and 5% dilution factor applied to the 5 x 5 x 5m open pit resource block models.
    - Mining costs of $2.00 per tonne of waste mined and $2.50 per tonne of ore mined.
    - Milling costs of $16.81 per tonne processed.
    - Heap Leach costs of $5.53 per tonne processed.
    - G&A cost of $2.00 per tonne of material processed.
    - 3% royalty costs and 1% selling costs were also applied.
    - A 0.17 g/t gold only cutoff was applied to ex-pit processed material (which is above the heap-leaching NSR cutoff).
2. Underground Resource estimates are based on economically constrained stopes generated using Datamine's Mineable Shape Optimizer (MSO) algorithm and the following optimization parameters (all dollar values are in US dollars):
    - $1,950/ounce gold price and $25.24/ounce silver price.
    - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
    - Mechanized cut and fill mining with a $60.00 per tonne cost.
    - Diluted to a minimum 4m stope width with a 98% mining recovery.
    - G&A cost of $4.00 per tonne of material processed.
    - Milling costs of $16.81 per tonne processed.
    - 3% royalty costs and 1% selling costs were also applied.
3. Where mentioned, "residual open pits" assumes that any underground stopes are backfilled with zero grade material at two-thirds of the original rock density. Economic-constrained open pits are then estimated with this mined-out, backfilled material in the open pit block selective mining unit ("SMU") model and assuming the resource parameters above.
4. Mineral Resources are not Mineral Reserves (as that term is defined in the CIM Definition Standards) and do not have demonstrated economic viability.

1.4 Mineral Resource Estimate Sensitivities

1.4.1 *Underground Sensitivity*

The Project is also amenable to a more substantial underground mining approach. In the following sensitivity table, the Project is assumed to be mined by underground methods, backfilled, and then economically-constrained residual open pits are estimated at a 0.17 g/t Au only cutoff.

Table 1-2 Sensitivity: Underground Mining Prioritized Scenario

Mining Method	Class	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
Underground	Indicated	8,231	2.68	709	103.2	27,306
	Inferred	8,979	2.14	617	81.4	23,492
Open Pit (Residual)	Indicated	19,166	0.56	345	16.0	9,842
	Inferred	3,483	0.50	56	15.4	1,721
Total	Indicated	27,397	1.20	1,053	42.2	37,148
	Inferred	12,462	1.68	673	62.9	25,212

Notes:

1. This and any other sensitivities presented are in lieu of, and not in addition to the 2024 MRE inventories.
2. Open Pit Resource estimates are based on economically constrained open pits generated using the Hochbaum Pseudoflow algorithm in Datamine's Studio NPVS and the following optimization parameters (all dollar values are in US dollars):
   - $1,950/ounce gold price and $25.24/ounce silver price.
   - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
   - Heap leach recoveries of 73% and 25% for gold and silver, respectively.
   - Pit slopes by area ranging from 42-47 degrees overall slope angle.
   - 5% ore loss and 5% dilution factor applied to the 5 x 5 x 5m open pit resource block models.
   - Mining costs of $2.00 per tonne of waste mined and $2.50 per tonne of ore mined.
   - Milling costs of $16.81 per tonne processed.
   - Heap Leach costs of $5.53 per tonne processed.
   - G&A cost of $2.00 per tonne of material processed.
   - 3% royalty costs and 1% selling costs were also applied.
   - A 0.17 g/t gold only cutoff was applied to ex-pit processed material (which is above the heap-leaching NSR cutoff).
3. Underground Resource estimates are based on economically constrained stopes generated using Datamine's Mineable Shape Optimizer (MSO) algorithm and the following optimization parameters (all dollar values are in US dollars):
   - $1,950/ounce gold price and $25.24/ounce silver price.
   - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
   - Mechanized cut and fill mining with a $60.00 per tonne cost.
   - Diluted to a minimum 4m stope width with a 98% mining recovery.
   - G&A cost of $4.00 per tonne of material processed.
   - Milling costs of $16.81 per tonne processed.
   - 3% royalty costs and 1% selling costs were also applied.
4. Where mentioned, "residual open pits" assumes that any underground stopes are backfilled with zero grade material at two-thirds of the original rock density. Economic-constrained open pits are then estimated with this

mined-out, backfilled material in the open pit block selective mining unit ("SMU") model and assuming the resource parameters above.

5. Mineral Resources are not Mineral Reserves (as that term is defined in the CIM Definition Standards) and do not have demonstrated economic viability.

1.4.2 *Mill Only Cut-off Grade Sensitivity*

The following table illustrates the mill only open pit and underground economic inventories using an open-pit Au only cutoff grade of 0.17 g/t (Mineral Resource cutoff for reference) and a higher-grade cutoff of 0.75 g/t (Au only).

Table 1-3 Sensitivity: Mill Only at Various Cutoff Grades

	Classification	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
0.17 g/t Au only cutoff (reference)	Indicated	28,789	1.41	1,301	52.4	48,504
	Inferred	11,266	1.33	480	55.7	20,163
0.75 g/t Au only cutoff	Indicated	16,499	2.10	1,112	70.4	37,354
	Inferred	6,800	1.91	418	69.8	15,262

Notes:

1. This and any other sensitivities presented are in lieu of, and not in addition to the 2024 MRE inventories.
2. Open Pit Resource estimates are based on economically constrained open pits generated using the Hochbaum Pseudoflow algorithm in Datamine's Studio NPVS and the following optimization parameters (all dollar values are in US dollars):
    - $1,950/ounce gold price and $25.24/ounce silver price.
    - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
    - Heap leach recoveries of 73% and 25% for gold and silver, respectively.
    - Pit slopes by area ranging from 42-47 degrees overall slope angle.
    - 5% ore loss and 5% dilution factor applied to the 5 x 5 x 5m open pit resource block models.
    - Mining costs of $2.00 per tonne of waste mined and $2.50 per tonne of ore mined.
    - Milling costs of $16.81 per tonne processed.
    - Heap Leach costs of $5.53 per tonne processed.
    - G&A cost of $2.00 per tonne of material processed.
    - 3% royalty costs and 1% selling costs were also applied.
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    - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
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5. Mineral Resources are not Mineral Reserves (as that term is defined in the CIM Definition Standards) and do not have demonstrated economic viability.

1.5 Mineral Processing and Metallurgical Testing

Preliminary mineral processing and metallurgical testing was completed between 1998 and 2012 by previous owners, and more recently by Prime.

Leach testing was completed on composite samples with parameters such as cyanide concentration, pulp density and grind size to determine preliminary recovery parameters and to support recoveries used for this resource estimate.

Preliminary gravity separation and flotation testing has been performed to assist with future flow sheet optimization design.

Based on the metallurgical test work results, the following processing design parameters were recommended by Kappes, Cassiday & Associates ("KCA"):

- Heap Parameters:
  - Three-stage crushing to 80% passing 6.3 mm for heap leach material.
  - 90-day leach cycle.
  - Average gold recovery of 73% and silver recovery of 25%.
- Mill Parameters:
  - Target grind size of 80% passing 0.037 mm (400 mesh).
  - Gravity concentration with agitated leach on gravity tails.
  - Overall mill recoveries of 95.6% for gold and 81% for silver.

In general, the various deposits at the Project show amenability to cyanide leaching for the recovery of gold and silver values, with improved recoveries with fine crushing/grinding. Further details, including reagent consumptions, are provided in Chapter 13.

1.6 Environmental Studies and Social Considerations

The environmental conditions of the Project area were documented in an environmental study carried out by Consultores Interdisciplinarios en Medio Ambiente, S.C ("CIMA") in 2022. The study analyzed, characterized, and described the current conditions of the area of interest to help identify future changes that could be the product of the activities carried out by the Company, and to facilitate permitting. The report covered an area of 21,079 hectares, which extends beyond the limits of the Project claim area.

The Project concession area does not fall within a designated protected natural area ("Áreas Naturales Protegidas"), area of importance for conservation of birds (as recognized by "Sección

Mexicana del Consejo Internacional para la Preservación de las Aves”), and no priority terrestrial regions (“regiones terrestres prioritarias – RTP") are located within the Project area. The authors of the Technical Report note disturbance in the area due to prior mining activities, as well as agricultural and livestock impact.

CIMA found that Prime has strictly complied with the applicable laws and standards and has received no sanctions from the regulatory entities since the beginning of operations. The Project area does not overlap with, and is not proximal to, any protected wilderness areas.

In 2021, CIMA carried out a socioeconomic baseline study. The Project area is divided into the Ejidos La Tasajera (88%), San Antonio del Cerro (5%) and Zapote (7%). The ejido acts as a legal entity and is made up of land for production, common or collective use and human settlements.

The resource estimate is completely contained within the Ejido La Tasajera, and a 15-year (renewable for an additional 15-year period) agreement was signed in 2020 for the benefit of the inhabitants and the Company in order to guarantee access and exploration work, while providing a structure to compensate landowners for any disturbance. This agreement includes terms for Project construction and operations. The surface rights agreement for eventual Project use was doubled to 1800 hectares in a subsequent agreement with Ejido La Tasajera in 2023.

Prime works closely with the ejidos in regard to development, access improvements, water supply, potential employment and other considerations.

1.7 Conclusions and Recommendations

Based on the highly prospective geology, size and continuity of the mineralized structural corridors identified to date, including surface and drilling results by both Prime and others, Property mineralization may be more extensive than currently reported.

The Project contains Indicated and Inferred Mineral Resources that are associated with well-defined mineralized trends and models. All deposits are generally open along strike and at depth. Prime believes that the Project has the potential for the delineation of additional Mineral Resources within the three main trends and Generative Targets, and that further additional exploration is warranted on new high-priority targets identified from detailed mapping and surface sampling within the Property.

The exploration program should include a phased approach of drilling along the extensions (along strike and at depth) of the known deposits (resource drilling) along with drilling other identified high-priority targets (discovery drilling) as well as other key objectives as listed below:

- Continue detailed field mapping and sampling, rock and soil geochemistry along currently defined and possible new structural corridors.

- Completion of the budgeted 2024 drilling program, consisting of Mineral Resource expansion and generative exploration, totalling 50,000 metres.
- Drilling in 2025 and beyond will be subject to the Company's overall project development strategy. A minimum of 20,000 metres is recommended.
- Almost three-quarters of the updated MRE is at the Indicated level of confidence, which is sufficient for inclusion in a PFS (as defined below) and potential conversion to Mineral Reserves. Prior to commencement of a PEA (as defined below), exploration should focus on adding resource extensions at the Inferred level of confidence.
- Project engineering and advancement: depending upon the results of subsequent drilling and modelling work, market conditions and investor expectations, Prime should begin to consider further Project study and analysis leading to development of a PEA. This would further considerations around processing methodologies, mining methods (open pit vs. underground), infrastructure, initial capital considerations, operating costs, and overall economic returns of the Project.

2. INTRODUCTION

2.1 Issuer and Purpose

The Company has contracted John Sims, CPG (as defined below) to prepare the Technical Report for the Project located in the states of Sinaloa and Durango, México. Mr. Sims visited the Property in November 2022. Caleb Cook, P.Eng., also visited the Property in January 2024.

Prime is using this Technical Report to support disclosure of an updated MRE at the Project. The Technical Report conforms to NI 43-101. The effective date of this MRE is October 15, 2024, following a drilling cutoff of July 17, 2024. There were no material changes to the MRE between this date and the publication of this accompanying NI 43-101 Technical Report. Drilling and interpretation continue at the Property.

2.2 Authors and Site Inspection

This Technical Report has been prepared in conjunction with, and on behalf of, the Company, by John Sims, Certified Professional Geologist ("CPG") and President of Sims Resources LLC, Damian Gregory, P.Eng. of Snowden Optiro, Chantal Jolette, P.Geo and President of Qualitica Consulting Inc., and Caleb D. Cook, P.Eng. with KCA (collectively, the "Qualified Persons"). The Qualified Persons are Independent QPs per NI 43-101 definitions.

Mr. Sims is a graduate of the University of Montana with a B.A.Sc. in Geology and has over 35 years of mining industry experience. He is a member in good standing of the American Institute of Professional Geologists, AIPG Certification number CPG-10924. His experience with respect to Mineral Resources and Mineral Reserves includes working as a resource exploration geologist in Chile, Honduras, México, Tanzania, and USA; exploration project manager in Nicaragua; mine site project manager and geologist at underground and open pit mines in western USA, Central and South America; 20 years of resource modelling and Mineral Reserve optimization experience for deposits in Argentina, Australia, Chile, Bolivia, Ecuador, Ghana, Mauritania, México, Russia, Tanzania and USA. He has 19 years of experience as a site and corporate Qualified Person (as that term is defined in NI 43-101) which includes positions as a Senior Project Mine Geologist, then Director of Technical Services for Coeur d'Alene Mines Corporation, and as Director, VP and SVP of Technical Services for Kinross Gold Corporation. He has project managed multi-disciplinary teams that required close interaction with mining engineers for Mineral Reserve estimation, as well as consideration of recovery methods, project infrastructure, costs and economics including PEA, PFS and Feasibility studies.

Mr. Sims visited the Property from November 11 to November 16, 2022. The visit included field checks for access, historical and active drill pads and geology at various outcrops/gossans at the Property. Mr. Sims inspected core and sample cutting and logging areas; discussed geology and mineralization; reviewed geological interpretations and Mineral Resource modeling procedures with Prime's technical staff. All sections in this Technical Report have been prepared under the supervision of Mr. Sims.

Damian Gregory is a senior mining professional with over 20 years of engineering and operational experience in the mining industry. Mr. Gregory is an expert in strategic mine planning, Mineral Resource and Mineral Reserve evaluation, PEAs, PFS and Feasibility Studies for both open pit and underground deposits. He is a registered Professional Engineer ("P.Eng.") in Ontario, Canada with broad consulting experience covering variety of commodities from around the world. Damian is a co-author of several papers related to mine planning and optimization. Mr. Gregory did not visit the Project site.

Chantal Jolette, P.Geo is President and Principal Geologist with Qualitica Consulting Inc., Ms Jolette has 20 of relevant analytical quality control experience in production and exploration environments, and in multiple commodity spaces. She has reviewed the quality assurance and quality control procedures, as well as the results of the control samples for the 2021-2022 drilling at the Project and prepared Section 11 – Sample Preparation, Analyses, and Security. Ms. Jolette has not visited the Project site.

Caleb D. Cook, P.E. is Project Manager at KCA. A 2010 graduate from the University of Nevada, Reno, he holds a BS in Chemical Engineering. Mr. Cook is a licensed P.Eng. in the state of Nevada and has been with KCA for more than 8 years where he has worked as a Support Engineer and Project Manager on mining projects all over the world. Mr. Cook visited the site in January, 2024. During the site visit, Mr. Cook met with project personnel, reviewed drill core, discussed metallurgical test work and planned testing and visited proposed processing facilities locations including crushing/milling sites, heap leach sites and tailings facilities sites.

A summary of the Independent QPs is provided in Table 2-1.

Table 2-1 Independent Qualified Persons

Qualified Person	Position	Employer	Date of Last Site Vist (if applicable)	Professional Designation	Responsibility
John Sims	President	Sims Resources LLC	November, 2022	CPG	Independent Qualified Person for Technical Report
Damian Gregory	Principal Consultant	Snowden Optiro	Not Applicable	P.Eng	Economically constrained Resource estimate (Section 14.3.11)
Chantal Jolette	President and Principal Geologist	Qualitica Consulting, Inc.	Not Applicable	P.Geo	Quality Assurance / Quality Control review (Sections 11 and 12)
Caleb Cook	Project Manager	Kappes, Cassiday & Associates	January, 2024	P.E.	Mineral Processing & Metallurgical Testing (Section 13)

2.3 Sources of Information

The sources of information and data contained in the report or used in its preparation include: documentation listed in Section 3 – Reliance on Other Experts and Section 27 – References, excerpts or summaries from documents authored by other consultants and figures and tables developed by the Company, and verified by Mr. Sims. Mr. Sims reviewed all relevant information provided by the Company required for this Technical Report.

Mr. Sims also reviewed other sources of information including the Company's internal reports and has supervised the preparation of this report based on his Property visit and the work performed on the Property to date. Mr. Sims believes that exploration completed by both Prime and select work by previous Property owners as cited in this Technical Report and listed in Section 27 – References is accurate and representative of the Property and has been completed to acceptable standards.

2.4 Units of Measure and Abbreviations

With respect to abbreviations and units of measure, unless otherwise stated, this Technical Report uses:

- Bulk weight is presented in metric tonnes ("tonnes"; 1,000 kg or 2,204.6 lbs.)
- Geographic coordinates are projected in the Universal Transverse Mercator ("UTM") system relative to Zone 13 of the World Geodetic System 1984 ("WGS84")
- Currency in Canadian dollars ($CAD), unless otherwise specified (e.g., U.S. dollars, $US; Euro dollars, €)
- Grams per tonne ("g/t" or "gpt")
- Gold ("Au")
- Hectares ("ha")
- Kilometres ("km")
- Ounces ("oz"), thousands of ounces ("koz") and millions of ounces ("Moz")
- Metres ("m")
- Millimetres ("mm")
- Net Smelter Return ("NSR")
- Parts per million ("ppm")
- Pre-Feasibility Study ("PFS")
- Preliminary Economic Assessment ("PEA")
- Percent ("%")

2.5 Effective Date

The effective date of this MRE is October 15, 2024, following a drilling cutoff of July 17, 2024. There were no material changes to the estimate between this date and the publication of this accompanying NI 43-101 Technical Report. Drilling and interpretation continue at Project.

3. RELIANCE ON OTHER EXPERTS

In preparation of this Technical Report, the Independent QP relied on:

- A title opinion provided by Prime, authored by Juan Carlos de Teresa of Bello Gallardo Bonequi y Garcia, SC ('BGBG') which is summarized in sub-sections 4.2 and 4.3 of Section 4 – Property Description, Location and Tenure herein.
- Information regarding permitting and environmental status of the Project that was provided by Prime and is summarized in sub-section 4.6 of Section 4 – Property Description, Location and Tenure. Much of this summary is from a baseline environmental assessment consulting report by CIMA titled 'Linea Base Ambiental "Los Reyes"', 2022.

4. PROPERTY DESCRIPTION, LOCATION AND TENURE

4.1 Description and Location

The Property is located in the Guadalupe de Los Reyes mining district in the western foothills of the SMO mountain range, Sinaloa and Durango states, México (Figure 4-1). The Property is north of the coastal city of Mazatlán, approximately 110 km by air and 200 km by paved road. The Property is within the municipality of Cosalá (population 17,012, INEGI 2000) and the closest city to the Property is Cosalá (population 7,888, INEGI 2020), which is located 30 km to the northwest of the Property. Enroute to the Property from Cosalá are the villages of Palo Verde and La Tasajera. The village of Guadalupe de los Reyes is on the Property and was a site for Spanish colonial mining (Figure 4-2). The general geographic coordinates of the Property are N-24°17´ and W-106°32´ (UTM Zone 13 North 0344250E, 2686400N). Coordinates are in WGS 84.

Figure 4-1 General Location Map

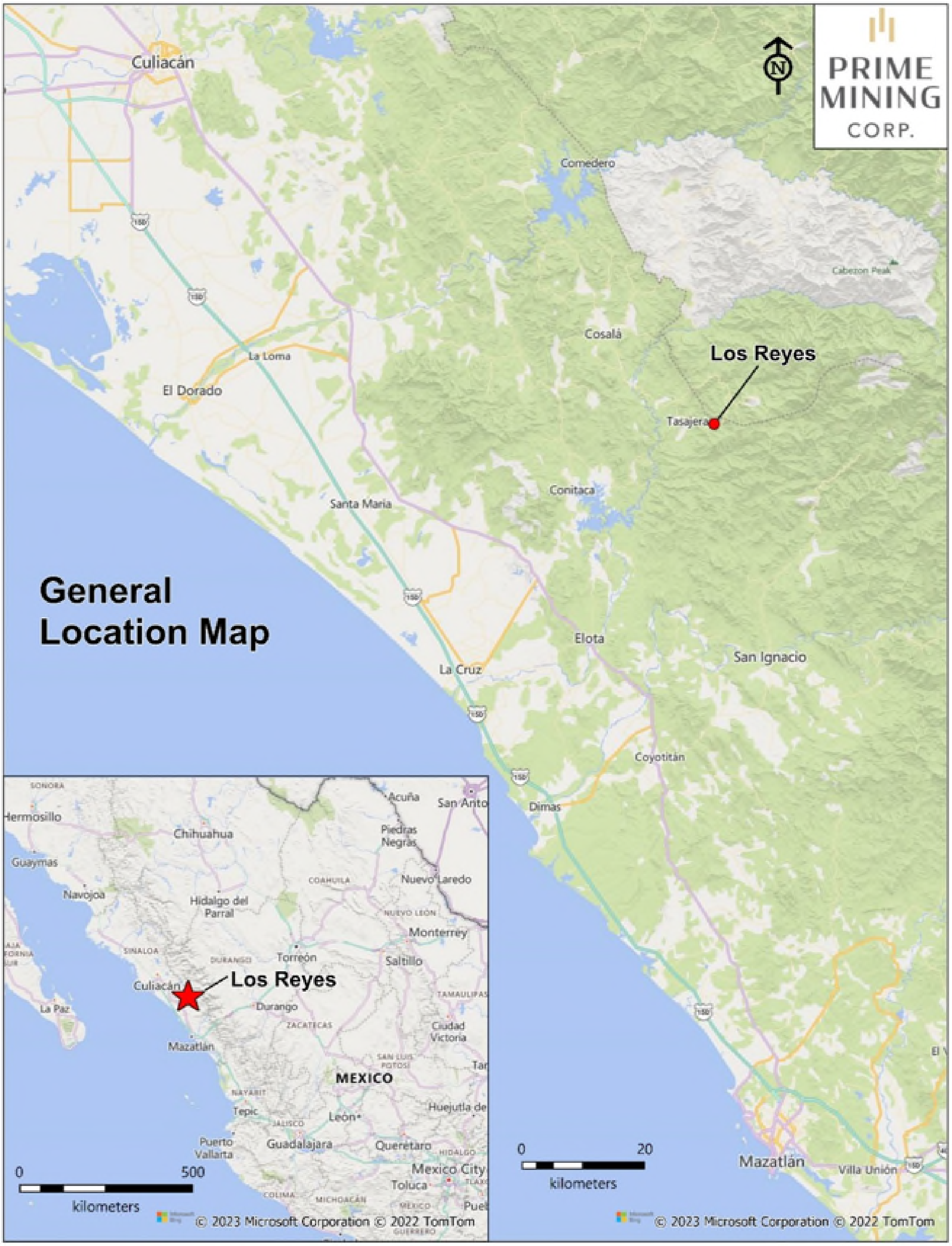
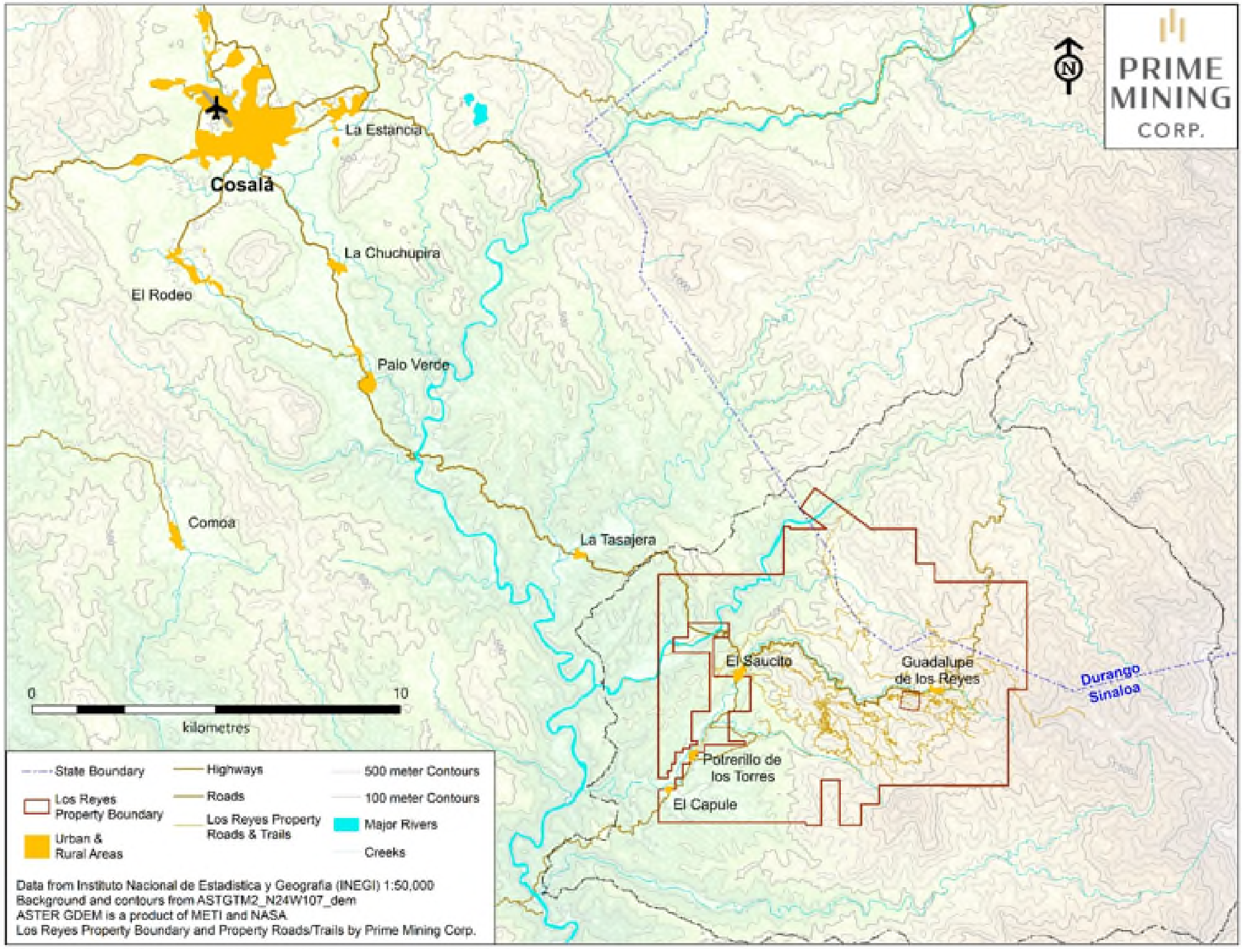


Figure 4-2 Property Location Map



4.2 Los Reyes Property Concessions and Area

The Property is composed of 37 contiguous concessions that have an area of 6,302.7 hectares; however, due to overlap between some of the concessions, the actual area is 6,273 hectares**.** Figure 4-3 shows the concessions and their associated overlap.

Bello Gallardo Bonequi y García, S.C., located in Mexico City, which is a law firm in México, was commissioned in late 2024 to provide a title opinion and related matters that are associated with the mining concessions of the Property. This title opinion was completed on November 7, 2024 and stated that the Property was in good standing.

Prime's subsidiary, Minera Amari, S.A. de C.V. has a negotiated surface rights agreement for 1,800 hectares of land use with the local community, Ejido La Tasajera, located in Cosalá, Sinaloa, México. These payments are in good standing, and are progressive, based on time and project status. See Section 4.4 below for further details.

4.3 Mineral Tenure, Option Agreements, Royalties and Encumbrances

Prime holds the unencumbered rights to 100% of the Los Reyes mining concessions, free of any liens, charges or third-party claims or rights, and subject only to royalties, some of which include a buyout option. Outlined below is the history of the Property claim ownership, including the ultimate transfer of the rights to Prime in 2019.

Portions of the claim block have been owned by several entities over time. As a result, there are several royalty agreements in place. The entities that hold or held agreements are listed below:

- Minera Alamos Inc. (MAI), a company incorporated under the laws of the Province of Ontario;
- Minera Alamos De Sonora S.A. De C.V. ("MAI México"), a company incorporated under the laws of the United Mexican States;
- ePower Metals Inc. (name changed to Prime Mining Corp. on August 28, 2019), which is a company incorporated under the laws of the Province of British Columbia;
- Vista Gold Corp. ("Vista Gold") is a corporation existing under the laws of the Province of British Columbia;
- Minera Gold Stake, S.A. de C.V. ("MGS"), a corporation existing under the laws of the United Mexican States;
- Minera Gold Stake Holdings Corp. ("MGS Canada"), a corporation existing under the laws of British Columbia; and
- Granges Inc. ("Granges"), a corporation existing under the laws of British Columbia.

4.3.1 *Previous Ownership Agreements*

Vista Gold Agreement

Vista Gold, MGS Canada and Granges together own 100% of the outstanding common shares of MGS. MGS acquired a 100% interest in portions of the Zapote zone on August 1, 2003, from Sr. Enrique Gaitán Maumejean. The final payment of the purchase option, which also included acquisition of a data package associated with the project, was completed in 2009. In January 2008, MGS further consolidated the remaining mining concessions, subsequently known as the Guadalupe de los Reyes project (Los Reyes project), except for the 6 de Enero claim, which is 23.7 hectares in size. Following this consolidation, and the acquisition of ten new claims, including fractionals, MGS's land position included 37 contiguous concessions. The consolidation of the mineral rights was completed through agreements with Grandcru Resources Corporation (Grandcru), Goldcorp Inc., and the San Miguel Group.

In addition to securing the mineral tenure, MGS also negotiated access agreements to the lands held by Ejido La Tasajera. These agreements provided access the Property.

Minera Alamos Option Agreement

MAI and its wholly owned Mexican subsidiary, MAI México, entered into an option agreement dated October 23, 2017 with Vista Gold, MGS, MGS Canada and Granges. This option agreement granted to MAI an option to acquire 100% of the issued and outstanding common shares of MGS, and therefore own the Los Reyes mining concessions.

This option agreement, subject to a 49% back-in right (a "Back-In Right") on underground resources, required the payment of $US6 million, payable in four instalments of $US1.5 million each. The first instalment stipulated payment at the time of execution of the agreement, with the following two instalment payments being made on the 12th month and 24th month of execution of the agreement. Payment of the last instalment, termed the purchase price payment, was to be made on or before the end of the option period. In the event that MAI announced a positive decision to take the Los Reyes project into construction, MAI agreed to make this final payment within 30 days following the date of such announcement. The date of the announcement would then be the closing date. In addition to these cash payment requirements, MAI agreed for the duration of the option agreement to pay for storage of core in Hermosillo and to pay for 100% of the maintenance costs to keep the mining concession in good standing.

In order for the Alamos group of companies (MAI and MAI México) to comply with Mexican law, MGS and MAI México entered into an exploration agreement to conduct exploration work on the mining concessions, to cover the costs of the core storage facility in Hermosillo, and to fulfill all of the obligations with the Ejido La Tasajera. An Ejido is communal land used for agriculture in which the community members have usufruct rights rather than ownership rights to the land. Obligations to the Ejido La Tasajera and other landowners in the Property area include obtaining a temporary occupancy agreement to obtain access to the Property along with other potential required agreements.

4.3.2 *Prime Mining Corp. Purchase Agreement Terms*

Effective June 25, 2019 (the "Assumption Date"), MAI and MAI México transferred all rights of the Los Reyes project, through an option agreement, to Prime (formerly ePower Metals Inc.). To meet the contractual obligations of this option agreement, Prime agreed to the following conditions:

- Payment of $US1.5 million to MAI as reimbursement for the instalment payment made by MAI to Vista Gold on April 23, 2019 (which represented the second option payment under the October 23, 2017 agreement).
- Assume MAI's remaining option payments of $US3 million in favour of Vista Gold: $US1.5 million due on October 23, 2019 and $US1.5 million due on the earlier of October 23, 2021 or a production decision.
- Issuance of 9,450,000 post-consolidation common shares of Prime and 3,350,000 common share purchase warrants of Prime to MAI, entitling MAI to acquire further

post-consolidation common shares at a price of $0.50 per share for a period of 24 months. Prime completed this transaction, as stated in its August 28, 2019, news release.

Effective on the Assumption Date, Prime took over all obligations and liabilities of MAI and MAI México with respect to the option agreement between Vista Gold and MAI.

On June 12, 2020, the Company amended the Los Reyes Amended Option Agreement for the Los Reyes Project with Vista Gold. The amended Los Reyes Amended Option Agreement provides for the cancellation of all ongoing NSRs and Back-In Rights held by Vista Gold, in consideration for accelerating the final $US1,500,000 option payment owing to Vista Gold (the "Option Payment") and paying (1) $US1,100,000 no later than six months from the acquisition date; and (2) $US1,000,000 no later than 12 months from the acquisition date.

According to the terms of the amended agreement, once the Company made the Option Payment, Vista Gold would no longer retain a capped NSR on production from open-pit mining or a perpetual NSR on production from underground mining. In addition, Vista Gold would no longer have the Back-in Rights to assume a 49% non-carried interest in any underground mining project developed at the Property. If the Company failed to make the $US1,100,000 and $US1,000,000 payments, Vista Gold would have the right to reinstate its NSRs and Back-in Rights.

In summary, to acquire the Property, Prime:

- Paid $US1,500,000 to MAI, to reimburse MAI for the cost of an option payment required to be made to Vista Gold in April 2019.
- Assumed MAI's remaining Option Payments of $US3,000,000 in favour of Vista Gold of which $US1,500,000 was paid in October 2019 and $US1,500,000 was paid in July 2020.
- Issued to MAI 9,450,000 common shares and 3,350,000 common share purchase warrants entitling MAI to acquire further common whares at a price $0.50 per share for a period of 24 months.
- Paid to Vista Gold $US1,100,000 in January 2021 and a further $US1,000,000 in July 2021, which together satisfied the conditions of the Option Payment within the required timeframe, thereby removing the NSRs and Back-In Rights previously held by Vista Gold.

As of July 20, 2020, the Company filed a deed in México with the Public Registry of Property and Commerce to record the transfer of the 37 Los Reyes mining concessions. Registration of these concessions with the Mines General Directorate's Mining Public Registry was completed in November 2024.

4.3.3 *Summary of Los Reyes Property Concessions and Royalties*

A summary of the royalty agreements, the requirements and associated encumbrances by mining concession, as currently understood by Prime based on documentation from Vista Gold, are included in Tables 4-1 and 4-2. Table 4-1 lists the mining concessions that comprise the claim block and lists the associated royalty percentages, while Table 4-2 describes the terms of the royalties shown in Table 4-1. Prime continues to review the various royalties listed to confirm their status and validity. Note that due to slight overlap of the 37 individual Los Reyes concessions, the total area is shown as 6,302.7 hectares. The actual surface area of the Los Reyes claim block is 6,273 hectares. The Property dispositions are shown on Figure 4-3.

Table 4-1 Mineral Tenure, Royalty Agreement Summary by Mining Concession within the Property

Concession Name	Title Number	Surface Area (Ha)	Expiration Date	Location	Royalty % (and Table 4.2 ref.)	
					With repurchase option	Without repurchase option
Los Reyes Dos	214131	17.4	9-Aug-51	Cosalá, Sinaloa		4%: NSRs 1 and 4
Los Reyes Tres	214302	197.0	5-Sep-51	Tamazula, Durango		4%: NSRs 1 and 4
Los Reyes Cuatro	217757	11.2	12-Aug-52	Cosalá, Sinaloa		4%: NSRs 1 and 4
Los Reyes Cinco	216632	320.0	16-May-52	Cosalá, Sinaloa		4%: NSRs 1 and 4
Los Reyes Seis	225122	427.7	21-Jul-55	Cosalá, Sinaloa		1%: NSR 4
Los Reyes Siete	225123	4.8	21-Jul-55	Cosalá, Sinaloa		1%: NSR 4
Los Reyes 8	226037	9.0	14-Nov-55	Cosalá, Sinaloa		4%: NSRs 1 and 4
Los Reyes Fracc. Oeste	210703	476.9	17-Nov-49	Cosalá, Sinaloa		4%: NSRs 1 and 4
Los Reyes Fracc. Sur	212758	589.1	7-Oct-49	Cosalá, Sinaloa		4%: NSRs 1 and 4
Los Reyes Fracc. Norte	212757	1334.5	7-Oct-49	Cosalá, Sinaloa		4%: NSRs 1 and 4
Norma	177858	150.0	28-Apr-36	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
Nueva Esperanza	184912	33.0	5-Dec-39	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
San Miguel	185761	11.8	13-Dec-39	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
San Manuel	188187	55.8	21-Nov-40	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5

Concession Name	Title Number	Surface Area (Ha)	Expiration Date	Location	Royalty % (and Table 4.2 ref.)	
					With repurchase option	Without repurchase option
El Padre Santo	196148	50.0	15-Jul-43	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
El Faisán	211471	2.6	30-May-50	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
Santo Niño	211513	44.1	30-May-50	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
San Pablo	212752	11.2	21-Nov-50	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
San Pedro	212753	9.0	21-Nov-50	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
Patricia	212775	26.2	30-Jan-51	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
Martha I	213234	46.7	9-Apr-51	Cosalá, Sinaloa	2%: NSR 3	1%: NSR 5
Elota	237661	947.7	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Elota Fracción 1	237662	905.6	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Elota Fracción 2	237663	3.3	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Elota Fracción 3	237664	2.7	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Elota Fracción 4	237665	8.1	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Elota Fracción 5	237666	4.2	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Elota Fracción 6	237667	0.5	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Elota Fracción 7	237668	0.2	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Elota Fracción 8	237669	0.7	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Elota Fracción 9	237670	1.0	19-Apr-61	Cosalá, Sinaloa Tamazula, Durango	NIL	NIL
Diez De Mayo	223401	0.2	10-Dec-54	Cosalá, Sinaloa	2%: NSR 2	2-3%: NSR 6
Prolongación Del Recuerdo	210497	91.5	7-Oct-49	Cosalá, Sinaloa	2%: NSR 2	2-3%: NSR 6
Prolongación Del Recuerdo Dos	209397	26.7	8-Apr-49	Cosalá, Sinaloa	2%: NSR 2	2-3%: NSR 6
Arcelia Isabel	193499	60.4	18-Dec-41	Cosalá, Sinaloa	2%: NSR 2	2-3%: NSR 6

Concession Name	Title Number	Surface Area (Ha)	Expiration Date	Location	Royalty % (and Table 4.2 ref.)	
					With repurchase option	Without repurchase option
Dolores	180909	222.0	5-Aug-37	Cosalá, Sinaloa	2%: NSR 2	2-3%: NSR 6
La Victoria	210803	199.9	29-Nov-49	Cosalá, Sinaloa	2%: NSR 2	2-3%: NSR 6
TOTAL SURFACE AREA		**6,302.7**				

Table 4-2 Royalty Agreement Definitions

NSR 1: A 3% NSR to be obtained as a result of producing and selling gold, silver and other ores covering the mining concessions: “Los Reyes Dos”, title 214131; “Los Reyes Tres”, title 214302; “Los Reyes Cuatro”, title 217757; “Los Reyes Cinco”, title 216632; “Los Reyes 8”, title 226037; “Los Reyes Fracc. Oeste”,title 210703; “Los Reyes Fracc. Sur”, title 212758; and “Los Reyes Fracc. Norte”, title 212757, in favor of Corporación Turística San Luis, S.A. de C.V. or its designee.

NSR 2: (Re-purchase option) Enrigue Gaitan's 2% NSR (Minera Tatemas S.A. de C.V.) can be re-purchased for $US 1 million before July 31, 2053. The Gaitan NSR came from Vista Gold's acquisition of the Gaitan claims Jan 3, 2003 for US$1.4 million plus 2% NSR.

NSR 3: (Re-purchase option) San Miguel Group’s (SMG) 2% NSR can be re-purchased for $US 1 million at any time. The SMG NSR is owed to Genssler Investment Partnership, LLP, Doug Foote, and Synergy Group Limited (San Miguel Group). GrandCru acquired the San Miguel Group claims in 2004 for $650,000 plus the 2% NSR.

NSR 4: A 1% NSR to be obtained as a result of producing and selling gold, silver and other ores covering the mining concessions “Los Reyes Dos”, title 214131; “Los Reyes Tres”, title 214302; “Los Reyes Cuatro”, title 217757; “Los Reyes Cinco”, title 216632; “Los Reyes Seis”, title 225122, “Los Reyes Siete”, title 225123; “Los Reyes 8”, title 226037; “Los Reyes Fracc. Oeste”, title 210703; “Los Reyes Fracc. Sur”, title 212758; and “Los Reyes Fracc. Norte”, title 212757, in favor of Desarrollos Mineros San Luis, S.A. de C.V. or its designee.

NSR 5: A 1% NSR to be obtained as a result of producing and selling gold, silver and other ores covering the mining concessions “Norma”, title 177858; “Nueva Esperanza”, title 184912; “San Miguel”, title 185761; “San Manuel”, title 188187; “El Padre Santo”, title 196148; “El Faisán”, title 211471; “Santo Niño”, title 211513; “San Pablo”, title 212752; “San Pedro”, title 212753; “Patricia”, title 212775; and “Martha I”, title 213234, in favor of Desarrollos Mineros San Luis, S.A. de C.V. or its designee.

NSR 6: A royalty between 2% and 3%, based on the prevailing gold price as indicated below, on the NSR from producing and selling gold, silver from the lots covering the mining concessions: “Prolongación del Recuerdo”, title 210497; “Prolongación del Recuerdo Dos”, title 209397;

"Arcelia Isabel", title 193499; "Dolores", title 180909; and "La Victoria", title 210803, in favor of Desarrollos Mineros San Luis, S.A. de C.V. or its designee. For gold prices $US499 per Troy ounce or less, the royalty is 2.00% and for gold prices $US500 or more, it is 3.00%.

Figure 4-3 Property Concessions Map

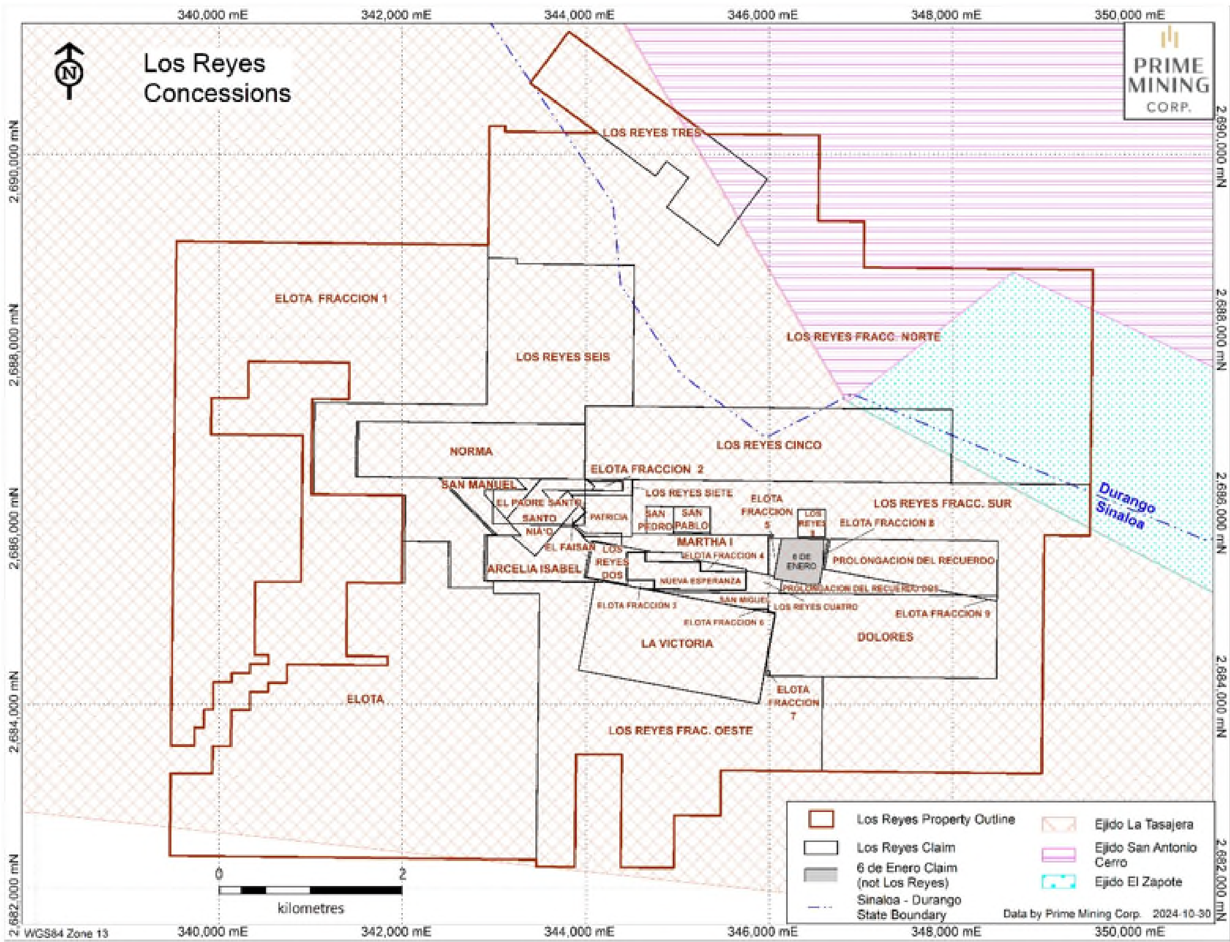
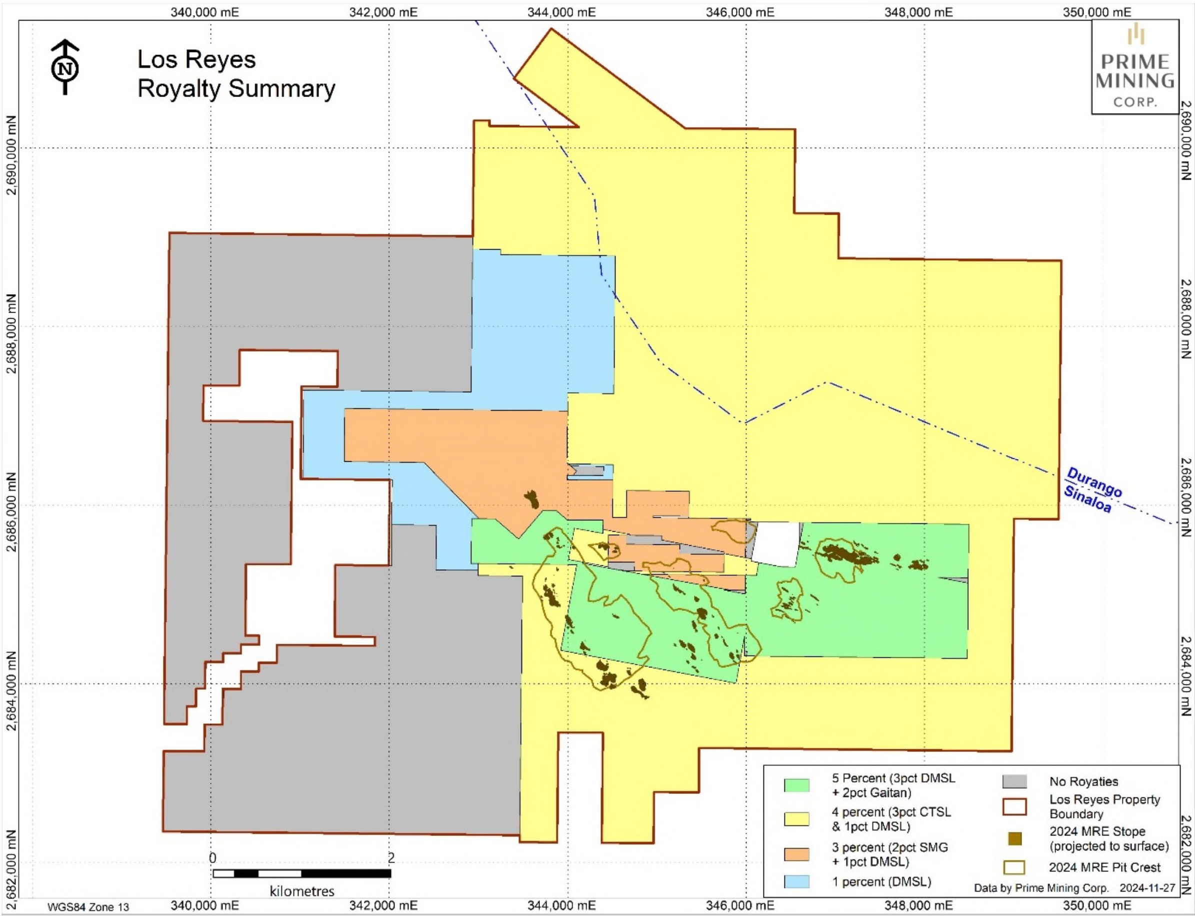


Figure 4-4 Property Royalties by Concession Map



4.4 Surface Use and Disturbance Agreement

On March 3, 2020, Prime announced in a news release that it had signed a long-term agreement (the "Agreement") with the representatives of the Ejido Tasajera for surface use and compensation for disturbance of the Project area. The Agreement has an initial term of 15 years and can be extended for an additional 15-year period, and includes access and land use for exploration, engineering, construction, commissioning, and commercial operation. Upon execution of this agreement, Prime made an initial payment of US$38,300 to Ejido Tasajera. In 2023, this Agreement area doubled from 900 to 1,800 hectares.

The commercial terms of the Agreement are divided into three stages of activities: exploration, construction, and commercial production. The main conditions of the Agreement include:

- For an initial period of three years while conducting exploration, Prime agreed to pay an upfront fee of MXP$700,000 (US$38,300), as noted above, that includes the exploration work completed over the preceding six months and a three-year prepayment of three MXP$200,000 annual payments.

- Prime has the right to extend the exploration period for up to two additional years by making an annual payment of $US20,000 in year four (2023, paid) and $US30,000 in year five (2024).
- Prime has the right to initiate construction of a mine at any time. If construction begins prior to the fifth year, the annual payment is increased to $US30,000.
- Upon commencement of commercial production, the annual payment increases to $US200,000, paid in semi-annual installments of $US100,000. The payments are subject to customary indexing for inflation.
- Payments due to the Ejido Tasajera during commercial production are subject to adjustments based on Unidad de Medida de Actualizacion, the official Mexican index for the adjustment of government pensions, social security payments, taxes, etc.
- During commercial production, Prime will also make, collectively, a $US15,000 annual "apoyo" or gift distributed to the local families of Ejido Tasajera.
- During the dry season months, Prime will arrange to haul water to the Tasajera village if requested.
- Prime also intends to maximize employment of qualified local and Ejido Tasajera residents in its activities with individuals having the necessary skill levels and capability.
- The Agreement is fully transferable without further approval of the Ejido Tasajera.

In addition to the Agreement, an arrangement has also been completed that establishes specific, non-material payments to local individuals whose traditional land use within the Ejido becomes affected by Prime's exploration, construction, and production activities.

4.5 Environmental Liabilities

Existing environmental liabilities on the property are limited and include mine adits, roads, small waste rock piles and one cyanidation vat, which operated in the 1950s, near the village of Guadalupe de Los Reyes (Borrastero, López, & Stevens, 2003; López 2009). No acid mine drainage from the existing adits or underground mine has previously been reported.

4.6 Permitting Requirements

It is understood that environmental permitting will involve environmental impact assessment, obtaining permission to utilize natural resources, and change of land use permit. Approval of these permits is a prerequisite for obtaining a construction permit, which is the final permit that must be approved prior to commencement of mining activities.

The primary law legislating environmental protection in México is the Ley General del Equilibrio Ecológico y la Protección al Ambiente ("LGEEPA"). This environmental law is administered by the Secretaría de Medio Ambiente y Recursos Naturales ("SEMARNAT"), which is a branch of the federal government. SEMARNAT is also responsible for issuing land-use change permits for properties such as the Property that involve alteration of forested areas. SEMARNAT representatives in each state administer and address environmental impact issues as they are familiar with local issues and concerns.

The Procuraduría Federal de Protección al Ambiente (“PROFEPA”) is the agency responsible for enforcing SEMARNAT regulations. PROFEPA’s main activities are to deal with complaints, conduct inspections, and in general verify compliance with all federal environmental laws and regulations. It imposes penalties for violations of environmental laws and regulations, and monitors compliance with any preventive and mitigating measures issued by it. PROFEPA also conducts environmental audits.

Water use and infrastructure, water quality, and the right to discharge process water (collectively referred to as water rights) related to the Property would be handled by National Water Commission (Comisión Nacional del Agua) (“CONAGUA”). Land use permits are handled by local agencies in charge of the zoning and registration of land ownership.

Permitting is ongoing for exploration on the Property. Environmental permitting is supported by ongoing water quality monitoring, and baseline studies.

4.7 Baseline Environmental Studies

In order to support future efforts for project permitting, Prime has been engaged with CIMA, a leading Mexican environmental firm. In 2022, CIMA completed a baseline study (Linea Base Ambiental – “Los Reyes”) for the Project area.

The objective of this study was to analyze, characterize and describe the physical, environmental, and biological conditions of the environmental system where the Project is located. Another additional objective resulting from this study was to identify the most relevant physical-environmental attributes at the Property.

The Los Reyes concession area does not fall within a designated protected Áreas Naturales Protegidas, area of importance for conservation of birds (as recognized by “Sección Mexicana del Consejo Internacional para la Preservación de las Aves”), and no priority terrestrial regions (“regiones terrestres prioritarias – RTP") are located within the Los Reyes area.

The authors of the Technical Report note the disturbance of the area due to previous mining activities, as well as agricultural and livestock impact.

4.8 Other Significant Factors and Risks

The authors are unaware of significant factors or risks that may materially restrict Prime from its right and ability to perform work on the Property.

5. ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY

5.1 Topography, Elevation, and Vegetation

The Property is located within the SMO mountain range that trends north-northwest along the western coast of México. The topography varies from steep mountain terrain in the east to river valley in the west. Elevations range from 230 to 1,400 metres above sea level.

The vegetation includes tropical bushes and shrubs within the river valleys and evergreens at higher elevations within the mountainous regions. The majority of the land surrounding the villages is developed for agriculture.

5.2 Property Access and Proximity to Population Centers

The Property is approximately 110 km by air and 200 km by road from the coastal city of Mazatlán, Sinaloa. The Property is within the municipality of Cosalá (population 17,012), 30 km southeast of the city of Cosalá (population 7,888, INEGI 2020) by an all-weather road. The village of Guadalupe de Los Reyes is on the Property and was the site of Spanish colonial mining (Figure 5-1).

5.3 Climate

According to the Köppen-Geiger Climate Classification, this region is classified as Aw - Tropical Wet and Dry (De Jesus, A., Brena-Naarnjo, J.A., Pedrozo-Acuna, A., & Yamanaka, V.H.A., 2016). This region's weather is characterized by distinct wet and dry seasons, with most of the precipitation occurring in the high-sun ('summer') season (Britannica, 2020). Annual temperatures range from 16°C to 29°C. Precipitation reaches a peak in July, with 212.6 mm of rainfall in 2019 (World Weather online, 2020, paras. 2-3). This can cause flooding along the river that can limit access from the Property to Cosalá (López, 2009). To improve access to the Property, widening and upgrading the road, as well as reinforcing the river crossings, will be necessary (Turner and Hunter, 2020).

The Property is accessible year-round. Recent improvements to the area's infrastructure, such as the high bridge over the Las Habitas River, have enhanced accessibility.

5.4 Infrastructure

Cosalá is proximal to four international airports. Mazatlán International Airport is located approximately 2.5 hours from Cosalá and has regular flights to and from many North America centres. The other three airports are: Culiacán International Airport, also located approximately 2.5 hours from Cosalá; Mochis International Airport, located approximately 5 hours from Cosalá;

and General Guadalupe Victoria International Airport, also known as the Durango International Airport, located approximately 6 hours from Cosalá.

Cosalá has a regional airport, Aeropuerto de Cosalá, located northwest from the city centre. The road from Cosalá through Guadalupe de Los Reyes is the only maintained land access to the southeastern mountains in this part of the country.

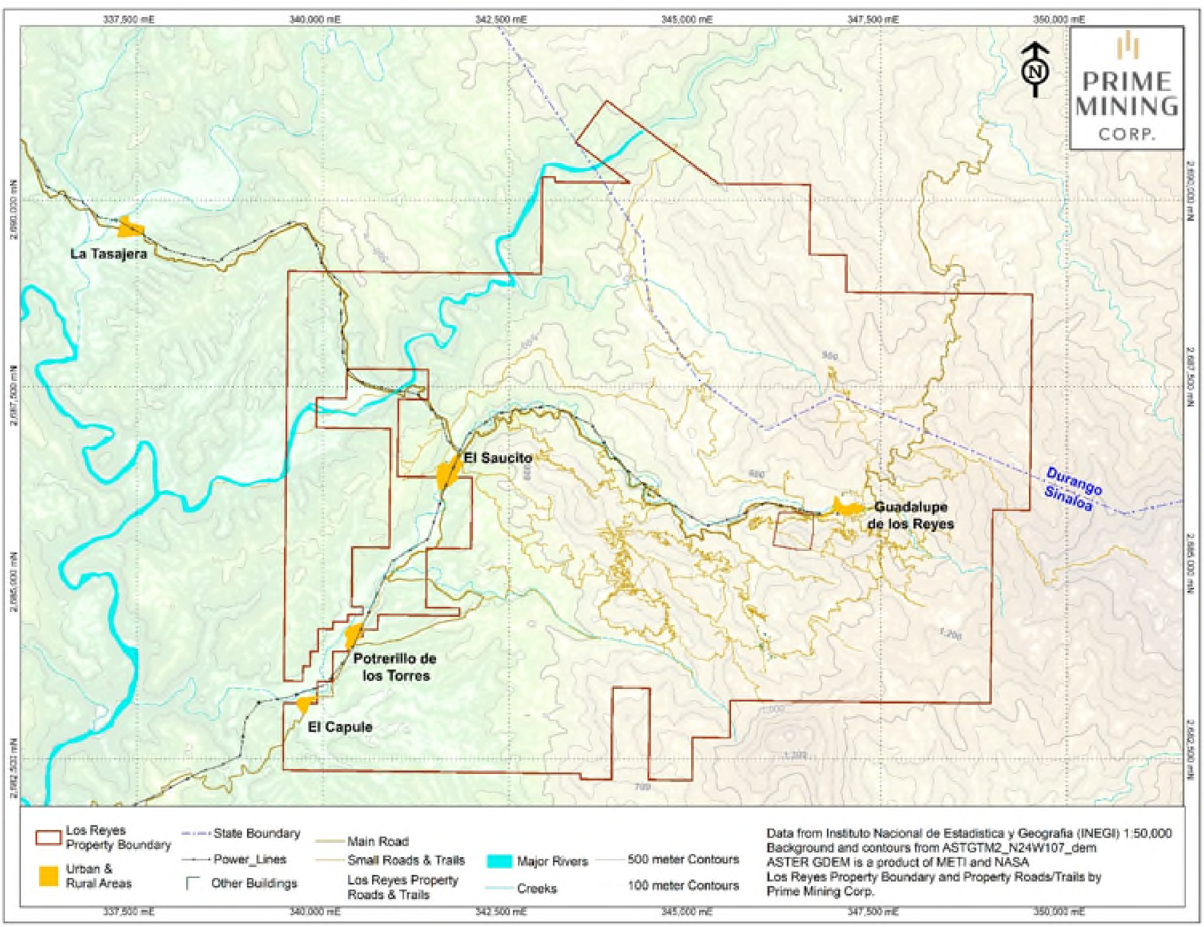
Local facilities include a hospital and health clinics; schools; banks; retail stores; hotels; restaurants; and tourism companies (sport utility vehicles).

The surrounding communities can provide labor, but a skilled workforce would have to be sourced from larger cities such as Mazatlán, Culiacán, and Durango, or imported from other countries. However, there is mining and minerals processing industry in and around Cosalá.

Local grid power is available throughout the area villages. Water is available seasonally from the Ejido. Additional water sources would need to be developed to support mining operations.

The surface rights and agreements with the Ejido are sufficient for mining operations.

Figure 5-1 Infrastructure Map



6. HISTORY

The original data from NCM (as defined below), Vista Gold, and Great Panther Silver Limited ("Great Panther") is currently in the Prime office in Vancouver, Canada. All of this data has been checked, compared and verified with the Prime digital files. Meridian Gold ("Meridian") data is incomplete with only the reverse circulation ("RC") drill holes on the Zapote deposit completed, and these were the only drill holes from Meridian used in the Resource estimate. All the Vista Gold and Great Panther drill collars have been located and resurveyed by Prime's contracted surveyor. Twenty-seven NCM drill collars have been surveyed by Prime's contracted surveyor and another approximately 35 NCM drill collars have been visually verified and handheld GPS coordinates collected. All NCM drill holes were collared on drill roads as shown on NCM maps and these locations compare very well with Prime's LiDAR topography, indicating that the NCM drill collars are probably within 10 metres of their original coordinates.

6.1 Prior Ownership and Ownership Changes on the Property

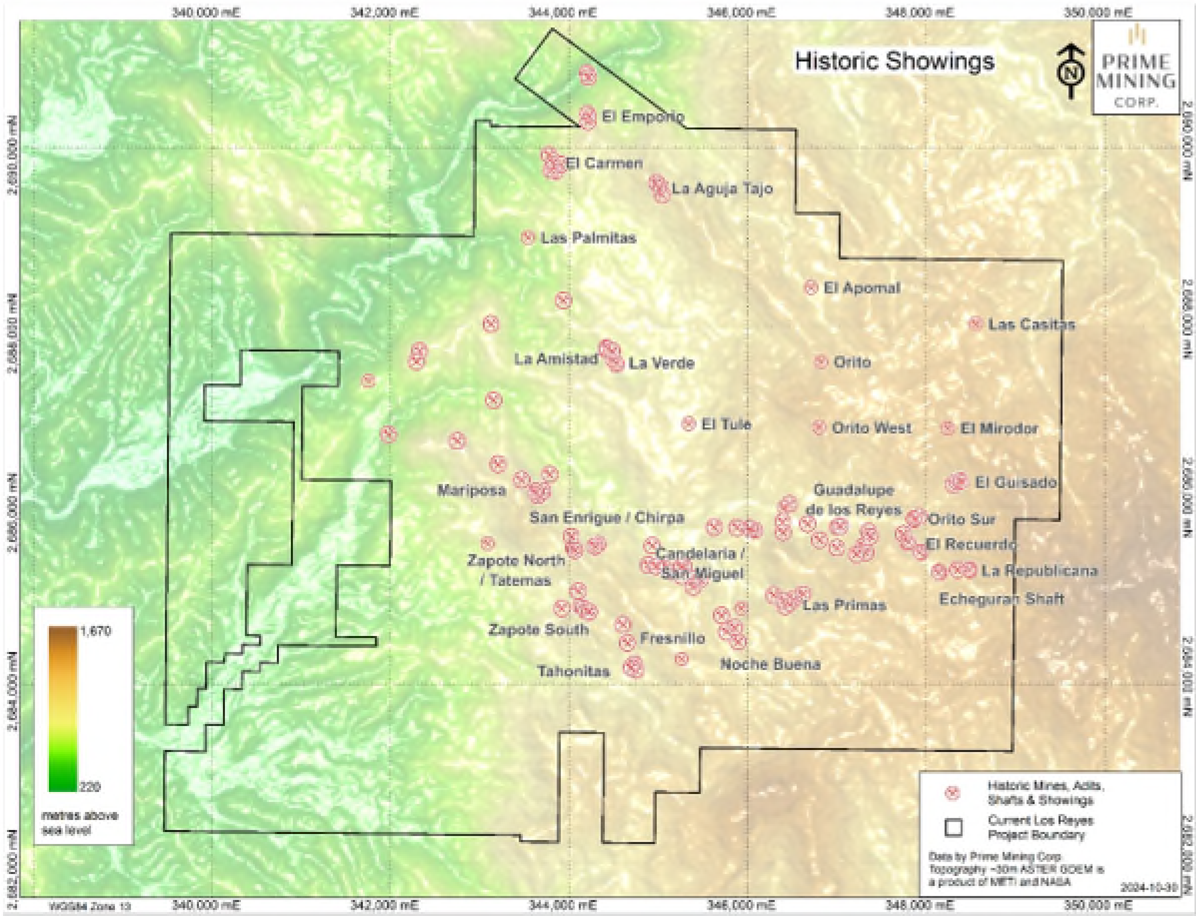
Since the discovery of gold and silver on the Property in approximately 1772, there have been several changes in ownership. The current ownership of the concessions that make up the Property are reviewed in detail in Section 4 – Property Description, Location and Tenure.

6.2 Exploration Type, Amount, Quantity and Results

6.2.1 *Property Overview*

Several mineralized areas have been identified, including: Mariposa; Zapote North; Zapote South; Tahonitas; San Miguel West (previously La Chiripa and San Enrique); San Miguel East; Fresnillo; Guadalupe West; Guadalupe East (previously Laija); Las Primas; Noche Buena; El Apomal; Orito; Las Casitas; Mina 20/21 and El Mirador. Figure 6-1 shows the location of all the known historical mines, adits, shafts and showings over topography. Previous technical reports mention two additional areas: Tatemas and Candelaria (Borrastero, López, & Stevens, 2003; López, 2009). It was concluded during this study that Tatemas was an open stope in the northern extent of Zapote North, while Candelaria was in the current extents of San Miguel East.

Figure 6-1 Los Reyes Historical Showings



6.2.2 *Historical Surface Exploration*

In the last three decades, several companies completed surface mapping, sampling (soil and rock), and geophysics exploration campaigns. These companies included Luismin (Gold Corp's Mexican subsidiary), NCM, Vista Gold, and Great Panther. A summary of the historical surface exploration is provided in Table 6-1.

Table 6-1 Summary of Exploration (1992 to 2019)

Company Name	Year	Surface Sampling and/or Exploration Method (Sample total)	Mineralized Areas
Luismin	1990-2000	Unknown	Orito, La Palmita, El Mirador, Las Casitas, El Apomal
NCM	1992-2000	Soil (4,640 samples) Rock (1,448 samples) Very Low Frequency Electromagnetics and Ground Magnetics	Guadalupe, Zapote, San Miguel, Noche Buena, Tahonitas, Orito, Mariposa
Vista Gold	2011-2012	Rock (271 samples)	Guadalupe, Zapote, San Miguel, Noche Buena
Great Panther	2014	Rock (275 samples)	Zapote, San Miguel, Las Primas

6.2.3 *Historical Drilling*

Historical drilling was conducted throughout the Property from 1992 to 2015 and is summarized by company in Table 6-2. Figure 6-2 shows historical drill hole locations within the Property.

Table 6-2 Drilling Summary by Year and Company

Company		**NCM**					**Meridian**	**Vista**			**Great Panther**	**Total**
Year		***1993***	***1994***	***1996***	***1997***	**sub-total**	**2001**	***2011***	***2012***	**sub-total**	**2015**	
Guadalupe	drillholes			*48*	*31*	79		*10*	*8*	18	9	**106**
	metres			*6783.3*	*3765.2*	10548.5		*1470.1*	*1481.6*	2951.7	1493.6	**14993.8**
Zapote North & South	drillholes	*28*	*38*	*22*	*113*	201	7 *		*15*	15	11	**234**
	metres	*2336.6*	*3375.7*	*1991.3*	*8024.6*	15728.2	1082.0		*1886.5*	1886.5	1156.8	**19853.4**
San Miguel	drillholes				*34*	34	13 **		*11*	11	17	**75**
	metres				*3674.4*	3674.4	1243.5		*1852.8*	1852.8	2313.1	**9083.7**
Noche Buena	drillholes		*4*	*9*	*12*	25			*4*	4	4	**33**
	metres		*246.9*	*1016.7*	*1328.9*	2592.6			*729.0*	729.0	541.6	**3863.1**
Tahonitas	drillholes			*33*		33						**33**
	metres			*2258.0*		2258.0						**2258.0**
Orito	drillholes			*8*		8	3 **					**11**
	metres			*1140.1*		1140.1	374.9					**1515.0**
Mariposa	drillholes				*1*	1						**1**
	metres				*166.1*	166.1						**166.1**
Total	drillholes	*28*	*42*	*120*	*191*	381	23	*10*	*38*	48	41	**493**
	metres	*2336.6*	*3622.6*	*13189.4*	*16959.2*	36107.8	2700.4	*1470.1*	*5949.8*	7419.8	5505.1	**51733.1**

Notes:

1. Two of the seven Meridian drill holes have no assay or geological information.
2. There is no available data, which includes assay and geological information, for these drill holes.

Northern Crown Mines ("NCM")

NCM conducted RC drilling in 1993, 1994, 1996 and 1997. In 1993 drilling was contracted to Tonto Drilling Services Ltd. of Hermosillo, Sonora, México. In 1994 the contract changed to Dateline International, S.A. de C.V. of Hermosillo. In 1996 and 1997 drilling was contracted to Dateline International, S.A. de C.V. and Layne de México, S.A. de C.V., both based in Hermosillo. NCM Drilled 381 holes totaling 36,108 metres (see Table 6-2).

Most of the RC drilling was dry and used air for a medium to recover the drill chips but when ground water was encountered, a water recovery medium was occasionally used.

The processing and geological logging of the samples was conducted at the various drill sites by qualified geologists and geotechnicians who were either independent contractors or employed by NCM. The physical features and lithologic composition of each sample were recorded onsite, including alteration, mineralization, and any observable structural evidence. Any underground workings intersected by the drilling were also documented on the drill log forms.

Collar locations, originally spotted by chain and pacing, were later located with a handheld GPS. The RC drill holes were not surveyed for down hole deviation. Samples were picked up from the NCM field camp by the assay laboratory and transported to their facility in Hermosillo, Sonora, México (Allen and Thurston, 1997).

Meridian Gold

Meridian entered into an agreement with NCM in late 2000 and conducted an RC drilling program in 2001. Meridian contracted the drilling to Layne de México, of Hermosillo, México, and completed 23 RC drill holes on the Property (Table 6-2). The drill tested sites at Guadalupe East, San Miguel West, Zapote North and Zapote South. Meridian collected samples from approximately 15 m above the mineralized/altered zone (hanging wall) and generally to the end of the hole. Bonder Clegg picked up samples at the field camp site and transported them to their laboratory in Hermosillo. Only the drill holes in the Zapote south area have geological logs and sample assay data, which includes 313 intervals.

Vista Gold

During 2011 and 2012, Vista Gold completed 48 diamond drill core holes on the Property. Drill collar locations within Zapote, Noche Buena, Guadalupe, and San Miguel were placed along section lines that spanned 25 m to 100 m apart, depending upon the area.

The diamond core drilling program was conducted under the supervision of Minera Cascabel. Vista Gold core drilling in 2011 and 2012 utilized HQ core to depths of approximately 110-150 m (rarely as shallow as 50 m) switching to NTW size core and occasionally BTW size core around 130 m depending on conditions. Vista Gold drilled 7,420 m in 48 core holes. The drill contractor was Energold de México, S.A de C.V., of México City, México.

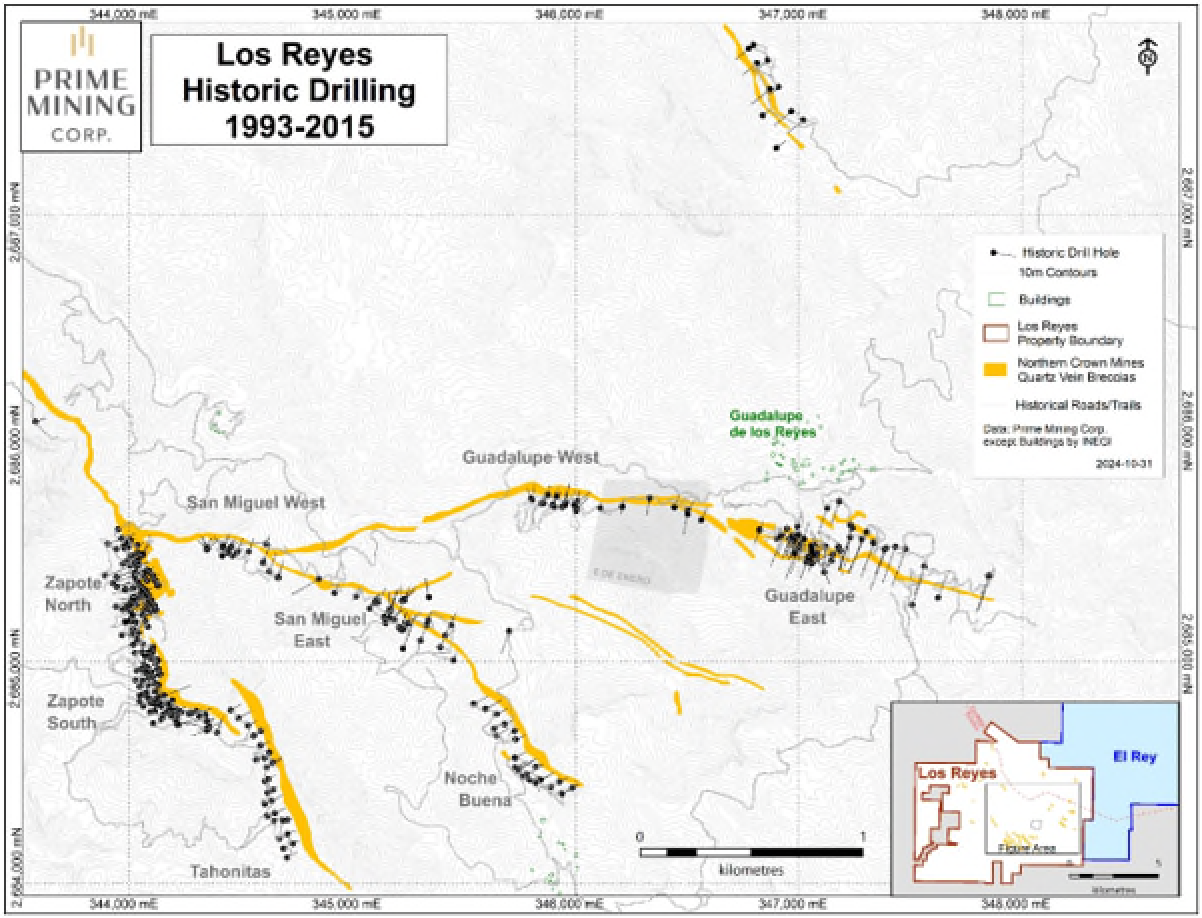
All collar locations were collected using a handheld GPS unit. Downhole surveys were completed on all drill holes. All the samples were kept in the secure area until picked up by ALS Chemex and delivered to Hermosillo for sample preparation and assay. Vista Gold submitted 5,396 split core samples. All remaining core, and pulps, are currently stored in one of Prime's warehouses in Cosalá, México.

Great Panther Silver Limited

In 2015, Great Panther drilled 41 confirmatory core holes for a total of 5,505 m. This includes 11 holes in the Zapote area, four holes in the Noche Buena area, 9 holes in the Guadalupe areas, and 17 holes in the San Miguel area. The drill program was supervised by Great Panther personnel. The drilling was carried out by Maza Diamond Drilling of Mazatlán, México using a track mounted HTM 2500 drill rig generating HQ or NQ core.

The objectives of the drill program were to test the continuity of the mineralized structures and the associated gold-silver mineralization with infill and confirmation holes, and to expand the mineralized zones with select step-out drill holes.

Figure 6-2 Los Reyes Historical Drilling



6.3 Historical Resource Estimates

Since 1998, numerous resource estimations have been conducted for portions of the Property by previous owners. The Mineral Resources that are reported in this section are historical in nature, have not been independently verified, are not current and should not be relied upon.

The historical Mineral Resources include: NCN 1998; Vista Gold 2003; 2005 GrandCru; 2009 Vista Gold; 2012 Vista Gold; 2016 Great Panther; Prime (Stantec), 2020; Prime (Sims), 2023. These historical resource estimations are superseded by this October 15, 2024 MRE.

6.3.1 *1998 NCM Historical Resource Estimate*

Pincock, Allen & Holt Ltd. (Pincock, Allen & Holt) was retained by NCM to prepare a technical report titled "Prefeasibility of the Zapote Deposit Guadalupe de Los Reyes Project, Sinaloa, Mexico", dated January 28, 1998. The MRE for the Zapote and San Miguel deposits were based on RC drilling programs carried out by NCM from 1994 to 1997. Table 6-3 shows the 1998 reported historical resource estimates and is reproduced from Table 1-1 of Pincock, Allen & Holt (1998).

Table 6-3 1998 NCM Historical Resource Estimate for San Miguel and Zapote

Geological Resource (unconstrained)	Base Case Zapote	Conceptual Study Zapote	Conceptual Study San Miguel	Total Base & Conceptual
	Indicated & Inferred	Inferred	Inferred	Indicated & Inferred
Cutoff Grade (g/t gold)	0.50		1.00	
Mineralized tonnes	5,852,000		1,120,000	6,972,000
Average grade gold (g/t)	1.35		3.79	1.74
Average grade silver (g/t)	8.7		91.0	21.9
Contained gold (ounces)	254,000		136,500	390,400
Contained silver (ounces)	1,637,000		3,277,000	4,915,000
In-Pit Resource	**Indicated**	**Inferred**	**Inferred**	**Indicated & Inferred**
Cutoff Grade (g/t gold)	0.50	0.50	1.00	
Mineralized tonnes	3,183,000	148,400	377,800	3,709,000
Average grade gold (g/t)	1.47	2.14	4.49	1.80
Average grade silver (g/t)	8.9	8.7	98.5	18.0
Contained gold (ounces)	150,500	10,300	54,600	215,400
Contained silver (ounces)	908,000	41,500	1,197,000	2,147,000

Notes:

This resource estimate is historical in nature and should not be relied upon, but it is considered relevant with respect to understanding the development of resources on the Los Reyes Property. Modelling methodology was not comprehensively presented in the 1998 Pincock, Allen & Holt Technical Report.

6.3.2 *2003 Vista Gold Historical Resource Estimate*

Pincock, Allen & Holt was retained by Vista Gold to prepare a technical report in accordance with NI 43-101 standards that is titled “Technical Report for the Guadalupe de Los Reyes Gold-Silver Project, State of Sinaloa, Western México”, dated July 17, 2003. The Guadalupe de Los Reyes MRE for the Zapote and other deposits within the Property area were based on RC drilling programs carried out by NCM from 1994 to 1997 and Vista Gold in 2003. Table 6-4 shows the 2003 reported historical resource estimates.

Table 6-4 2003 Vista Historical Resource Estimate

Deposit	Indicated (K Tonnes)	Gold (g/t)	Silver (g/t)	Inferred (K Tonnes)	Gold (g/t)	Silver (g/t)
Zapote	4,209	1.34	9.3	107	1.78	8.5
Tahonitas	404	1.41	48.4	290	1.54	52.0
Noche Buena	459	1.18	23.6	1,144	1.13	24.9
San Miguel – La Chiripa (now San Miguel East and West)	515	1.15	70.8	173	1.80	60.3
Guadalupe – Laija (now Guadalupe East)	751	1.71	53.2	2,106	2.59	93.4
Guadalupe – West	9	0.59	19.1	20	0.66	15.5
TOTAL	**6,347**	**1.36**	**23.0**	**3,840**	**2.01**	**65.6**

Notes:

Resource has been adjusted to reflect material removal from historical underground workings and is reported within Optioned Claims @ 0.5 g/t gold. This MRE is historical in nature and should not be relied upon, but it is considered relevant with respect to understanding the development of resources on the Los Reyes Property.

Pincock, Allen & Holt utilized mineralization envelopes or zones built from the database to create solid zones which were estimated by ordinary kriging ("OK"). Derived historical mining solids were removed from the resource.

The 2003 resource assessment was superseded by an MRE presented in the 2009 technical report, as addressed in the following subsection.

6.3.3 *2005 Grandcru Historical Resource Estimate*

Pincock, Allen & Holt was retained by Grandcru Resources Corporation ("Grandcru") to prepare a technical report in accordance with the requirements of NI 43-101 that is titled "Technical Report Los Reyes, Gold-Silver Project, State of Sinaloa, Western México", dated April 11, 2005. This report stated that the Los Reyes MREs included in the report were based on RC drilling programs carried out by NCM from 1994 to 1997 (López & Stevens, 2005). Table 6-5 shows the historical resource estimate presented in this study.

Table 6-5 2005 Grandcru Historical Resource Estimate

Deposit	Indicated (K Tonnes)	Gold (g/t)	Silver (g/t)	Inferred (K Tonnes)	Gold (g/t)	Silver (g/t)
Zapote	1,520	1.45	7.4	68.00	1.60	6.4
Tahonitas	7	0.76	42.7	0.50	0.56	30.6
San Miguel – Chiripa (now San Miguel East and West)	1,568	2.19	54.6	491.00	2.58	55.3
Guadalupe – West	619	1.28	25.3	477.00	1.57	27.8
TOTAL	**3,714**	**1.73**	**30.4**	**1,036**	**2.05**	**39.4**

Notes:

Resource has been adjusted to reflect material removal from historical underground workings and is reported within Optioned Claims @ 0.5 g/t gold. This MRE is historical in nature and should not be relied upon, but it is considered relevant with respect to understanding the development of resources on the Property.

Pincock, Allen & Holt utilized mineralization envelopes or zones built from the database to create solid zones which were estimated by OK. Derived historical mining solids were removed from the resource.

The 2005 resource assessment was superseded by a resource estimate presented in the 2009 Technical Report, as addressed in the following subsection.

6.3.4 *2009 Vista Gold Historical Resource Estimate*

In 2009, Pincock, Allen & Holt was retained by Vista Gold to prepare a Technical Report in accordance with the requirement of NI 43-101 that is titled “Technical Report for the Guadalupe de Los Reyes Gold-Silver Project, Sinaloa, México”, dated August 12, 2009. The Guadalupe resource estimates for the Zapote and other deposits in the Property area were based on reverse circulation drilling programs completed by NCM between 1994 and 1997 (López, 2009). Table 6-6 shows the 2009 historical resource estimate that is a copy of Table 17-6 of López, 2009.

Table 6-6 2009 Vista Gold Historical Resource Estimate

Deposit	Indicated (K Tonnes)	Gold (g/t)	Silver (g/t)	Inferred (K Tonnes)	Gold (g/t)	Silver (g/t)
Zapote	5,723	1.37	8.8	180	1.71	7.7
Tahonitas	404	1.41	48.4	297	1.54	52.0
Noche Buena	459	1.18	23.6	1,144	1.13	24.9
San Miguel – Chiripa (now San Miguel East and West)	2,083	1.93	58.6	664	2.38	56.6
Guadalupe – Laija (now Guadalupe East)	751	1.71	53.2	2,106	2.59	93.4
Guadalupe West	628	1.27	25.2	497	1.53	27.3
TOTAL	**10,048**	**1.50**	**25.7**	**4,888**	**2.02**	**60.0**

Notes:

Resource has been adjusted to reflect material removal from historical underground workings and is reported within Optioned Claims @ 0.5 g/t gold. This MRE is historical in nature and should not be relied upon, but it is considered relevant with respect to understanding the development of resources on the Property.

Pincock, Allen & Holt utilised mineralisation envelopes or zones built from the database of holes drilled throughout the area to create solid zones which were estimated by OK in the GEMCOM software. Derived historical mining solids were removed from the resource.

The 2009 resource assessment was superseded by a MRE presented in the 2013 technical report, as addressed in the following subsection.

6.3.5 *2012 Vista Gold Historical Resource Estimate*

In 2012, Tetra Tech was commissioned by Vista Gold to prepare a technical report in accordance with the requirements of NI 43-101 titled "NI 43-101 Technical Report Resource of Guadalupe de los Reyes Gold Silver Project", dated November 29, 2012. This technical report included resource estimates for the Zapote, Noche Buena, San Miguel-Chiripa (now San Miguel East and West), and Guadalupe areas. The historical MREs shown in Table 6-7 are based on the estimates presented in Tables 14-3 and 14-4 of the 2012 Vista Gold Technical Report (Bryan and Spiller, 2012) and Tables 14-3 and 14-4 of the Vista Gold PEA that was released the following year (Bryan, Lips, Scharnhorst, and Spiller, 2014). MAI reproduced these resource estimates in Table 14-5 and 14-6 of the technical report titled "NI 43-101 Updated Technical Report Guadalupe de los Reyes Gold/Silver Project Sinaloa, México", that has an amended and reissued date of April 16, 2018.

Table 6-7 2012 Vista Historical Resource Estimate

Deposit	Indicated (K Tonnes)	Gold (g/t)	Silver (g/t)	Inferred (K Tonnes)	Gold (g/t)	Silver (g/t)
Zapote	3,905	1.65	16.5	1,127	1.25	11.8
Noche Buena	937	1.32	16.5	480	1.13	17.8
San Miguel – Chiripa (now San Miguel East and West)	459	3.19	77.4	583	2.21	64.8
Guadalupe	1,541	1.74	52.5	1,054	1.52	50.8
TOTAL	**6,843**	**1.73**	**28.7**	***3,244**	**1.49**	**34.9**

Notes:

Resource has been adjusted to reflect material removal from historical underground workings and is reported within Optioned Claims @ 0.5 g/t gold. * = total for this column is different from what was presented in the 2012 technical report due to summation difference. This MRE is historical in nature and should not be relied upon, but it is considered relevant with respect to understanding the development of resources on the Property.

Tetra Tech utilized mineralization envelopes or zones built from the database of holes drilled in the area to create solid zones that were estimated by OK in the GEMCOM software. Derived historical mining solids were removed from the resource.

6.3.6 *2016 Great Panther Historical Resource Estimate*

Great Panther commissioned SRK Consulting (Canada) Inc. ("SRK") to prepare a technical report in accordance with the requirements of NI 43-101 titled "Independent Technical Report for the Guadalupe de Los Reyes Gold-Silver Project, Sinaloa, México", dated February 16, 2016. Table 6-8 shows the historical MREs.

Table 6-8 2016 Great Panther Historical Resource Estimates

Open Pit Resource						
Deposit	**Indicated (K Tonnes)**	**Gold (g/t)**	**Silver (g/t)**	**Inferred (K Tonnes)**	**Gold (g/t)**	**Silver (g/t)**
Zapote	706	2.28	15	43	2.48	24
TOTAL	**706**	**2.28**	**15**	**43**	**2.48**	**24**
Underground Resource						
Deposit	**Indicated (K Tonnes)**	**Gold (g/t)**	**Silver (g/t)**	**Inferred (K Tonnes)**	**Gold (g/t)**	**Silver (g/t)**
Zapote	215	4.14	16.0	20	3.58	23.0
Noche Buena	172	4.31	57.0	115	5.76	48.0
San Miguel – Main	99	3.21	140.0	102	3.14	173.0
San Miguel – North	52	6.25	91.0	19	4.46	54.0
TOTAL	**538**	**4.23**	**59.17**	**256**	**4.45**	**96.30**

Notes:

Open pit Mineral Resources are reported at a cutoff grade of $US40 and underground Mineral Resources are reported at a cutoff grade of $US110. Cutoff grades are based on a price of $US1,150 per ounce of gold, $US18.50 per ounce of silver and recoveries of 96% for gold and 53 percent for silver. Mineral Resources are reported in relation to a conceptual pit shell.

SRK utilized mineralization envelopes built from the database of holes drilled throughout the area to create solid zones that were estimated by OK in the GEMCOM software. Derived historical mining solids were removed from the resource.

6.3.7 *2020 Resource*

In April 2020, Prime completed an initial NI 43-101 resource (Stantec; Turner and Hunter, 2020) and technical report thereon.

Two 3D geologic resource models, named TZSM and GUAD, were developed for delineated portions of the Property. The TZSM model encompasses the Zapote and Tahonitas deposits, as well as the San Miguel and Noche Buena deposits. The GUAD model includes the Guadalupe deposits. The MREs calculated in this study were restricted to pit-constrained surface resources. The pits were built using a constant 45° pit slope and block revenue minus block cost was used as a driver to determine the overall size of the Lerchs-Grossmann pits. Furthermore, pit economics used in the development of the economically constrained pits assumed Heap Leach processing.

The MREs were at the base case cutoff of 0.22 g/t gold, as well as cutoff sensitivities at 0.50 g/t gold, 0.70 g/t gold, 0.90 g/t gold, and 1.00 g/t gold. The assigned resource classification is currently constrained by a pit floor elevation determined visually from the down dip extent of blocks estimated in the first pass (Inferred) and by the maximum search distance of each estimation pass. Table 6-9 summarizes the 2020 Mineral Resource.

Table 6-9 Los Reyes Mineral Resource Estimate (Turner and Hunter, 2020)

Au Cutoff	Category	Tonnes ('000)	Average Gold Grade (g/t)	Contained Gold (ounces '000)	Average Silver Grade (g/t)	Contained Silver (ounces '000)
0.22 g/t cutoff total	Measured (M)	8,527	1.24	341	28.98	7,946
	Indicated (I)	11,225	0.81	293	23.99	8,658
	Inferred	7,094	0.78	179	29.95	6,831
0.50 g/t cutoff total	Measured (M)	5,294	1.8	306	37.62	6,403
	Indicated (I)	6,528	1.15	240	31.01	6,509
	Inferred	3,956	1.13	144	42.9	5,456
0.70 g/t cutoff total	Measured (M)	4,094	2.15	283	42.46	5,589
	Indicated (I)	4,603	1.38	204	35.48	5,251
	Inferred	2,603	1.44	120	54.36	4,549
0.90 g/t cutoff total	Measured (M)	3,323	2.47	264	46.57	4,975
	Indicated (I)	3,423	1.58	174	39.46	4,342
	Inferred	1,859	1.71	102	64.23	3,839
1.00 g/t cutoff total	Measured (M)	3,019	2.62	254	48.42	4,700
	Indicated (I)	2,895	1.7	158	41.85	3,895
	Inferred	1,685	1.78	97	67.22	3,642

Notes:

1. Three year rolling gold price of $US1,329 / Troy ounce and silver price of $US16 / Troy ounce used.
2. Cutoff grade of 0.22 g/t gold applied, unless otherwise stated.
3. Total mining and processing cost of $US6.70 / tonne applied.
4. No NSR charges were applied in calculation of cutoff or mining costs.
5. In-place tonnages constrained to the LG pit solids using combined gold and silver revenue.
6. The author, an Independent QP, has not done sufficient work to classify the estimate discussed below as current Mineral Resources or Mineral Reserves and is treating the estimate as historical in nature and not current Mineral Resources or Mineral Reserves. This historical estimate is presented only for the purpose of describing the extent of gold and silver mineralization and to outline the exploration potential.
7. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability.

6.3.8 *2023 Resource*

In May 2023, Prime completed an NI 43-101 resource update (Sims, 2023) and technical report thereon.

The Los Reyes resource model was prepared by Prime under the supervision of Sims Resources LLC (John Sims, Independent QP). Geologic and estimation domains were constructed using Leapfrog Geo v.2022.1.1, including input from geochemical analyses completed in ioGAS v.8.0. Geostatistical evaluations and EDA, including topcut selection, declustering, variography, and SGS were completed using X10-Geo v.1.4.18.22 and Snowden Supervisor v.8.15. Resource estimation was prepared using Leapfrog EDGE v.2022.1.1.

Gold and silver grades were interpolated into 5x5x5 m block models using ID3 estimation techniques. Search ellipse orientation and radii were selected based on variogram models for each Au and Ag estimation domain, with variable search orientation applied according to the nearest vein midpoint surface in the quartz vein and breccia model. Blocks were classified under the categories of Indicated and Inferred, in accordance with CIM Definition Standards. The Measured resource category was not used in either model because no modern mining has been undertaken at Los Reyes and it is therefore not possible to reconcile the models against production or tightly spaced data such as grade control drilling.

The economic pit-constrained resource estimate was completed by Snowden Optiro. The estimate was prepared using Datamine Studio NPVS, a strategic mine planning software package that generates pit shells based on the economic input parameters, and the Hochbaum Pseudoflow algorithm. The estimate considers blocks of Indicated and Inferred assurance categories only. The selected pit was computed using the NSR cutoff, which was subsequently filtered to include blocks with grades above the 0.22 gpt gold-only cutoff (or other gold cutoff sensitivities using the same methodology). Two processing methodologies were assumed: a mill to process the higher-grade blocks, and a heap leach. Only open pit mining was considered for extraction.

See Table 6-10 for the 2023 MRE.

Table 6-10 2023 Mineral Resource Estimate (0.22 gpt Au Cutoff Grade)

Process Stream	Assurance Category	Ore Tonnes (millions)	Average Gold Grade (gpt)	Contained Gold (k ozs)	Average Silver Grade (gpt)	Contained Silver (k ozs)
Mill	Measured (M)					
	Indicated (I)	16.6	1.66	888	60.2	32,182
	M+I	*16.6*	*1.66*	*888*	*60.2*	*32,182*
	Inferred	10.8	1.18	411	47.2	16,390
Heap Leach	Measured (M)					
	Indicated (I)	10.5	0.37	125	9.1	3,081
	M+I	*10.5*	*0.37*	*125*	*9.1*	*3,081*
	Inferred	7.3	0.37	86	8.3	1,944
TOTAL	Measured (M)					
	Indicated (I)	27.2	1.16	1,013	40.4	35,263
	M+I	***27.2***	***1.16***	***1,013***	***40.4***	***35,263***
	Inferred	**18.1**	**0.85**	**497**	**31.5**	**18,334**

Notes:

The reported MRE above considers contained Au and Ag ounces, reported from within economically constrained pits using the following optimization parameters:

1. $US1700/ounce gold price and $US22/ounce silver price.
2. Mill recoveries of 93% and 83% for gold and silver, respectively.
3. Heap leach recoveries of 73% and 25% for gold and silver, respectively.
4. 45-degree pit slopes, with an assumed 5% ore loss and 5% dilution factor applied.
5. Mining costs of $US2.00 / tonne of waste mined and $US2.50/ tonne of ore mined.

6. Milling costs of $US15 / tonne processed and heap leaching costs of $US4 / tonne processed.
7. G&A of $US1.60 / tonne processed.
8. 3% royalty costs and 1% selling costs were also applied.
9. Mineral Resources that are not Mineral Reserves do not have demonstrated economic viability.

6.4 Historical Production on the Property

Historical production, estimated from several reports and memorandums, is approximately 1 million ounces of gold and 60 million ounces of silver from 2.7 million tonnes. The main historical mines were the Estaca and Descubridora mines and ancillary veins at Guadalupe de Los Reyes, La Candaleria mine (San Miguel East), Tatemas and La Chiripa mines (Zapote North and San Miguel West), and Pachuca and Zapote mines (Zapote South). Small operations in more recent times include the Gaitan mine (Zapote South) and Mariposa mine. There are numerous exploration adits and shafts that tested a variety of mineralized veins, some of which may have produced limited ore, but the history on these is sparse. Figure 6-1 shows the locations of the recognized mines, adits and shafts and Table 6-10 shows the estimated historical production.

Table 6-11 Historical Production at the Property

Main Areas Mined	Years Mined	Production Mined (tonnes)	Estimated Au Grade (g/t)	Estimated Au Ounces	Estimated Ag Grade (g/t)	Estimated Ag Ounces
Guadalupe De Los Reyes	1772 - 1871	1,500,000	12	578,713	900	43,403,445
Guadalupe De Los Reyes	1871-1938	875,000	8.8	247,464	521	14,650,972
La Candalaria	1930s	100,000	11	35,366	200	643,014
Tatamas/La Chiripa	1935-1944	170,000	12	65,587	250	273,281
Zapote South/Pachuca	1930s	NA	NA	NA	NA	NA
Zapote South/Gaitan	1988-1989	31,500	6	5,975	NA	NA
Mariposa	1980s	10,000	5	1,672	NA	NA
Total Estimate		**2,686,500**		**934,776**		**58,970,712**

7. GEOLOGICAL SETTING AND MINERALIZATION

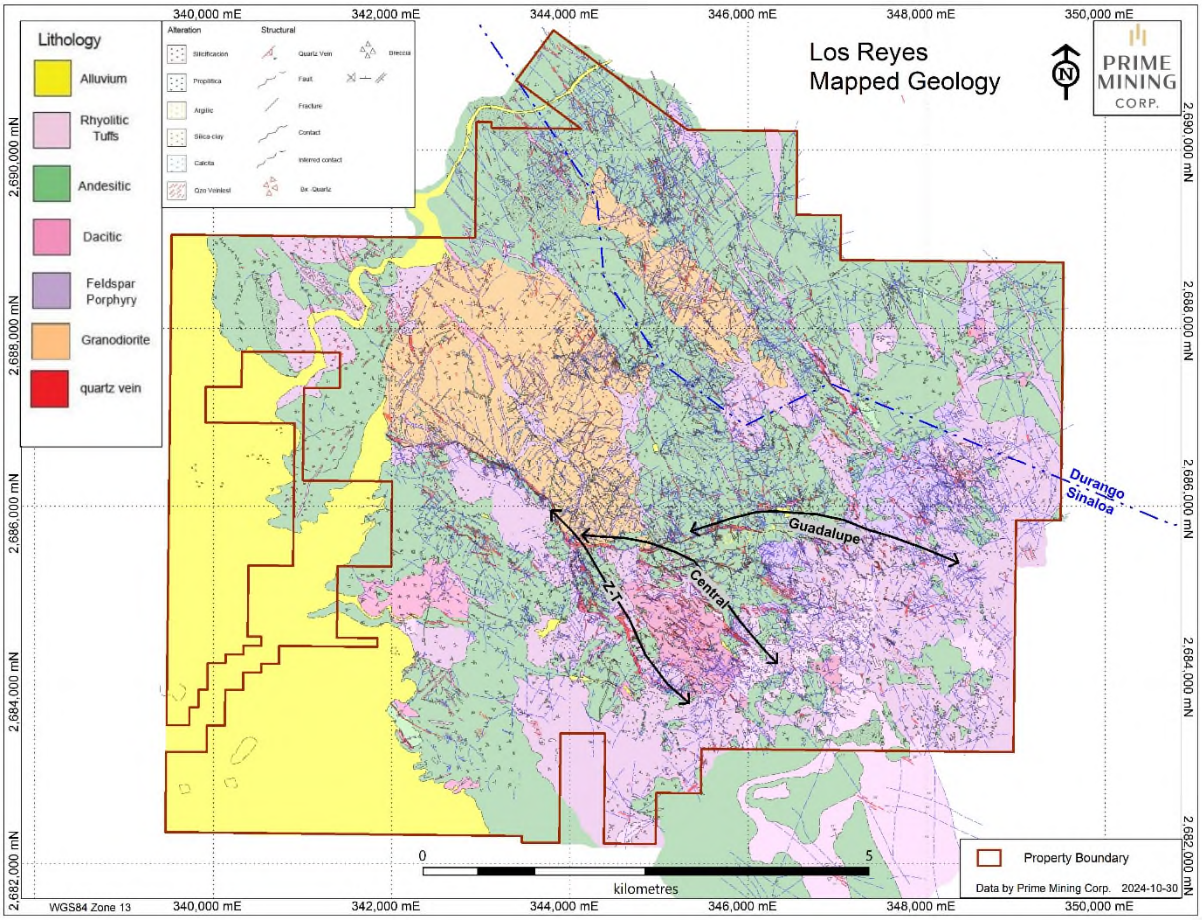
7.1 Regional and Property Geology

The Property is within the SMO mountain range of the North American Cordillera that extends for hundreds of kilometres from central to northern México in the Basin and Range province (Rossotti, Ferrari, López-Martinez, & Rosas-Elguere, 2002). The SMO is a large continuous sequence of volcanics from late Cretaceous to middle Tertiary in age (McDowell & McIntosh, 2012).

Near the Property, the volcanic sequence unconformably overlies a late Cretaceous- aged batholith. This overlying volcanic package is subdivided into Lower and Upper sequences that are separated by an angular unconformity. The Lower sequence spans from late Cretaceous-early Tertiary, is approximately 1 km thick, and is predominantly composed of intermediate (andesite) volcanics and more felsic units that are mostly dacitic to rhyolitic in composition. Intercalated sandstone and volcanic conglomerates of the Lower volcanic sequence are not significant on the property but do increase north of the Property towards Cosalá. The Upper Volcanic sequence which is deposited unconformably on the Lower sequence is composed of ash-flow and ash-fall tuffs that are rhyolitic to dacitic in composition. This sequence is over 1 km thick in higher elevation areas to the east (López & Ramirez, 2019; Turner and Hunter, 2020). Figure 7-1 shows Prime's significant detailed mapping of the Property since 2020. Within the Property the Upper sequence is found to be generally gently dipping and caps higher hilltops and ridges within and surrounding the district.

Several generations of felsic dykes cut the Lower Volcanic sequence. They include probable feeders for the rhyolitic to dacitic volcanic rocks in the upper part of the Lower sequence and some that are strongly flow-banded may be associated with the Upper Volcanic sequence eruptions. Gold and silver bearing quartz veins are commonly associated with the earlier rhyolitic to dacitic dykes suggesting that the mineralization is temporally associated with the culmination of Lower Volcanic sequence volcanism (Allen et al., 2001).

Figure 7-1 Los Reyes Property Geology



7.2 Mineralization

Gold and silver mineralization occur predominantly along three northwest to west-northwest oriented silicified structural corridors that form a horsetail-like structural complex that ultimately all merge together towards the west (Figure 1-4). These mineralized structural corridors are named after the mineralized areas that they host, which include: 1) the Mariposa- Zapote-Tahonitas (Z-T) trend; 2) San Miguel-Noche Buena (Central) trend; and 3) the Guadalupe (Guadalupe) trend. These main mineralized areas are described below and summarized in Table 7-1 (modified from López, 2009; Turner and Hunter, 2020). Several subsidiary mineralized structures have been identified between the main mineralized structures (Las Primas & Fresnillo). Gold and Silver values are associated with different pulses of quartz exploiting the same structure. Types of quartz are white, grey or greenish in colour, displaying classic low sulphidation epithermal textures such as saccharoidal, drussy, crustiform, colloform and crystalline textures.

7.2.1 *Mariposa-Zapote-Tahonitas (Z-T) Trend*

The Mariposa-Zapote-Tahonitas (Z-T) structure strikes to the north-northwest and dips at approximately 50° to the southwest. This trend shows evidence of previous workings, such as stopes, trenches, and adits.

Mariposa is the northernmost portion of the Z-T mineralized trend and has a length of approximately 1100m. The structure at Mariposa is at the contact between andesite and granodiorite with the rhyolitic stock. This structure is exposed on surface intermittently along the road that provides access to the historical mine workings (López, 2009). Mineralization is associated with hydrothermal breccias ((Turner and Hunter, (2020)); Table 7-1).

Zapote, which is divided into the North and South, is drill tested and is approximately 1.6 km in length and widths vary from 7 m to 66 m (Table 7-1). The hanging wall mineralization of Zapote is gradual and consists of quartz veining, brecciation, moderate silicification and argillization. Mineralization along the footwall is variable and consists of weak silicification and propylitic alteration. Mineralization within the main zone is strongly associated with silicified breccia and contains quartz, calcite, and adularia veins (López, 2009; Turner and Hunter, 2020).

Tahonitas, which is southernmost along the mineralized trend, is over 950 m in length. The widths vary from 15 m to 45 m. The mineralized structure at Tahonitas dips between 45° and 60° to the southwest (López, 2009). Tahonitas is hosted at the contact between rhyolite dikes and andesites of the Lower Volcanic Sequence.

7.2.2 *San Miguel-Noche Buena (Central) Trend*

The San Miguel West, San Miguel East and Noche Buena areas occur along a regional northwest – southeast striking structure called the Central trend that moderately dips between 50° and 70° to the southwest. The San Miguel West and East areas have a combined length of approximately 1,450 m and widths vary from 9 m to 75 m. This trend also shows evidence of previous workings, such as stopes, trenches, and adits. The host rocks in the area are andesites of the Lower Volcanic sequence that were subsequently intruded by an argillic altered feldspar-hornblende-biotite porphyry dike. The mineralized zone is associated with the brecciated zones proximal to the dike, as well as along the structure (López, 2009; Turner and Hunter, 2020).

The Noche Buena zone is the southernmost extension of the Central trend and is hosted in a system of sub-parallel quartz veins and veinlets. This zone has an approximate length of 800 m and widths vary from 12 m to 55 m (Turner and Hunter, 2020).

7.2.3 *Guadalupe Trend*

The Guadalupe trend, which bifurcates to the east from the San Miguel West deposit, is subdivided into the Guadalupe East and Guadalupe West deposits (see Figure 10-11). The trend, which has an east-west orientation, is strongly silicified and contains zones of silica stockworks. Guadalupe East and Guadalupe West have a cumulative length of 2,500 m and a true width that varies from 4 m to 68 m. The area was previously mined, with significant underground working that extend laterally by approximately 1.5 km and vertically to 400 m. The host rocks to mineralization are intermediate volcanics (in Guadalupe West this is andesitic flows and tuffs, while in Guadalupe East it is predominantly feldspathic porphyry) of the Lower Volcanic sequence.

In Guadalupe East the main structure contains a steeply south dipping to vertical vein called Estaca which has seen historical mining. North dipping antithetic structures in the hanging wall of the Estaca vein are present within a 500 m long block bounded by 2 northwest structures. This block was historically called Laija and more recently Prime has described it as a “flower structure”. East of Laija there are north dipping antithetic structures in the footwall of the Estaca vein; the larger antithetic veins were called San Manual and San Nicolas and these also reported historical mining.

7.2.4 *Additional Mineralized Areas*

Two mineralized areas: Fresnillo and Las Primas occur along subordinate subparallel structures to these main structures described above. Fresnillo is located between the Z-T and Central structures and the host rocks to mineralization are rhyolitic and dacitic rocks. In Las Primas, which is east of the Central structure and south of the Guadalupe structure, the host rocks are andesites of the Lower Volcanic sequence that were subsequently intruded by a feldspathic porphyry and rhyolite/dacite intrusives.

Additional mineralized areas are also identified to the north and northeast of the main area of mineralization. These mineralized areas include Palmitas, La Verde, Las Agujas, Orito, and Mina. Table 7-1 is a summary of mineralized areas and their characteristics. Table 7-1 is modified from Turner and Hunter, 2020.

Table 7-1 Summary of Mineralized Areas

Mineralized Area	Characteristics
Mariposa	Structure: Z-T Trend; Strike: From 320° in the southeast to 280° in the northwest; Dip: ~50° SW; Length: 1,100 m Structure Width (estimated): 15m to >40m; Mineralization Style: Silicified host rock, border breccias, stockwork and veins; Lithological Contacts: Breccias along faults proximal to andesite to rhyolitic intrusive bodies, border breccias, and veins.
Zapote (North & South)	Structure: Z-T Trend; Strike: 290° to 350° in the south, 280° to 360° in the north; Dip: 48-56º W; Length: 1,600 m; Width (true): varies from 7 m to 66 m; Mineralization Style: Silicified host rock, border breccias, stockwork and veins; Contacts: Sharp footwall contact and faulted stockwork and breccias to the hanging wall.

Mineralized Area	Characteristics
Tahonitas	Structure: Z-T Trend; Strike: 315° in the NW to 350 in the S°; Dip: 45º to 60º SW; Length: 950 m; Width (true): varies from 15m to 45m; Mineralization Style: Silicified host rock and veins border breccias, stockwork and veins; Contacts: Sharp footwall, some veining to the hanging wall.
San Miguel West	Structure: Central Trend; Strike: 275°; Dip: 70º SW; Length: 600 m; Width (true): varies from 9 m to 75 m; Mineralization Style: Silicified host rock, stockwork breccias and veins; Contacts: Sharp both walls
San Miguel East	Structure: Central Trend; Strike: 295°; Dip: 70º SW; Length: 850 m; Width (true): varies from 9 m to 75 m; Mineralization Style: Silicified host rock, stockwork breccias and veins; Contacts: Sharp both walls
Noche Buena	Structure: Central Trend; Strike: 320° to 335°; Dip: 50º to 60º SW; Length: 800 m; Width (true): varies from 12 m to 55m; Mineralization Style: Silicified host rock, breccias and veins; Contacts: stockwork footwall and stockwork to the hanging wall.
Las Primas	Structure: between Central and Guadalupe Trends Strike: 310° Dip: 65° - 80°SW to 80° NE; Length: 480 m (drill defined); Width (true): 1 m to 10 m based on drilling to date; Mineralization Style: a number of parallel to divergent structures across a 450 m width with stockwork Silicified host rock and breccias, stockwork veins; Contacts: Breccia to stockwork zone with quartz veining.
Fresnillo	Structure: between Z-T and Central Trends; Strike: 315-340°; Dip: 65º-70º SW; Length: 750 m (drill defined); Width (true): 1 m to 10 m based on drilling to date; Mineralization Style: Dacite host rock, breccias and veins(estimated): unknown; Contacts: Breccia zone with quartz veining.
Guadalupe East	Structure: Guadalupe Trend; Strike: 290° to 300°; Dip: 70º to 90º SW; Length: 1,500 m (drill defined); Width (true): varies from 4 m to 68 m; The widest area of mineralization is called Laija, it has a strike length of 500m and is characterized by a trans-tensional flower structure in which multiple NE-dipping veins emanate from the SW-dipping Estaca vein, which is hypothesized to be the principal controlling structure in Guadalupe East. Mineralization Style: Silicified host rock and breccias, stockwork veins; Contacts: Sharp in veins within breccia zone.
Guadalupe West	Structure: Guadalupe Trend; Strike: 270° to 280°; Dip: 65º to 80º SW; Length: 500 m (drill defined); Width (true): varies from 4 m to 55 m; Mineralization Style: Silicified host rock and breccias, stockwork veins; Contacts: Sharp in veins within breccia zone.
Orito	Structure: Orito Trend; Strike: 330°; Dip: 66º- 85º NE; Length: 3,000 m; Width (estimated): 1 m to 10 m based on the width of brecciated zones; Contacts: Breccia zone with quartz veining and iron oxide alteration, kaolinization.
Gavilanes	Structure: Outcroppings (structure not defined); Strike: 270° ; Dip: 63°-70° S; Length: 500 m; Width (estimated): from 1 m to 8 m based on mapping; Contacts: Breccias in hanging wall of Rhy Dk.

Mineralized Area	**Characteristics**
La Verde/ El Tule	Structure: Fault Zone; Strike: 330° Dip: ~60° SW; Length: 1000 m Structure Width (estimated): 1-10 metres based on mapping ; Mineralization Style: border breccias, stockwork and veins; Lithological Contacts: Breccias along faults proximal to andesite to rhyolitic intrusive bodies or granodiorite contact border breccias, and veins
Catanos/ Republicana	Structure: San Manuel Vein Trend part of Guadalupe Trend; Strike: 270° to 300°; Dip: 55º to 70º NE; Length: 1,500 m (cumulative); Width: varies from 4 m to 10 m; Mineralization Style: Silicified host rock and breccias, stockwork veins; Contacts: Sharp in veins. NE trend cut the E-W system.
Las Palmitas (El Carmen Mines)	Structure: Fault Zone; Strike: 310°; Dip: NE; Length: 350m; Width (estimated): unknown; Contacts: Quartz vein associated to Rhy Dk.
Las Agujas	Structure: Orito Trend; Strike: 330°; Dip: 60-75° NE; Length: part of the Orito trend (3000m); Width (estimated): 1-3 m; Contacts: Quartz vein associated to Rhy Dk.
Mina	Structure: on strike with Orito Trend; Strike: 340-355°; Dip: 70-85° NE; Length: (unknown); Width (estimated): unknown; Mineralization Style: border breccias, stockwork and veins; Contacts: Breccias along faults proximal to rhyolitic intrusive bodies.

8. DEPOSIT TYPES

The mineralized zones are characterized by a low-sulphidation epithermal system containing silica veins, stockworks, and breccias. These zones are generally formed in felsic subaerial complexes in extensional strike slip structural settings. Low sulphidation gold deposits are associated with magmas where ore deposition occurs several kilometres above the intrusion, and display certain alteration assemblages (Cooke & Simmons, 2000). The intrusions are likely the result of tectonic activity, such as plate subduction and extension. Deep hydrothermal fluid flow systems comprised of meteoric water, as well as near surface systems such as hot springs, are the sites of mineralization. Mineral deposition takes place as the fluids undergo cooling by fluid mixing, boiling and decompression (Cooke & Simmons, 2000).

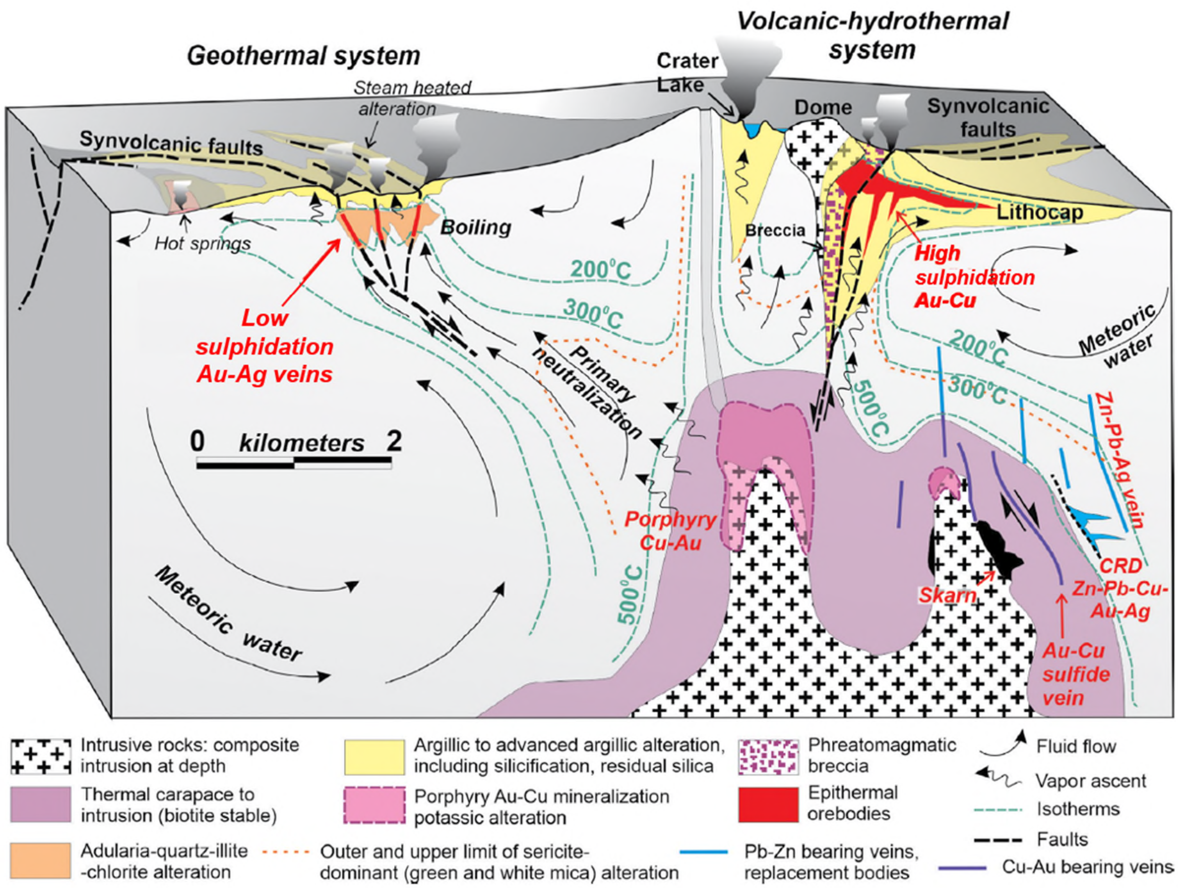
Distinguishing characteristics of low-sulphidation epithermal deposits are shown in Table 8-1 (Cooke & Simmons, 2000). A schematic cross-section diagram of a low-sulphidation epithermal system is shown in Figure 8-1 (Rhys et al, 2020).

Table 8-1 Characteristics of Low-Sulphidation Epithermal Deposits

Characteristics	Descriptions
Size of largest deposit	~90 t gold in Florida Canyon
Age	Oilgocene, Miocene
Ore Bodies	Veins, stockwork, disseminations
Vein Textures	Brecciates, crustiform, colloform, lattice
Tectonic setting	Magmatic arc with transtensional faults or Basin and Range faults
District setting	Volcanic centres localized by crustal fractures
Igneous association	Calc-alkaline, subduction related or bimodal, mantle derived
Igneous composition	Mafic-intermediate, intermediate-felsic
Host rocks	Calcareous and siliceous sedimentary rocks, metasedimentary rocks, & volcanic rocks
Depth of formation	Shallow, 0 to 2 km
Mineralization	Discordant ± strata bound; sinters are stratiform
Alteration types	Phyllic, argillic and opaline silica near surface
Open-space filling minerals	Quartz, adularia, bladed calcite, fluorite, pyrite-marcasite, sulfides
Ore minerals	Pyrite/marcasite, sulfosalts, base metal sulfides, electrum
Residence of gold	Free, inclusions and solid solution in pyrite-marcasite, sulfosalts
Landscape geochemistry	Along fracture zone near magmatic centre
Geochemical signature	Gold, silver, arsenic, antimony, mercury, selenium, barite, manganese, ± base metals
Iron mobility	Introduced, generally weak
Gold – Silver ratio	Low, variable, up to 2
Base metal content	Low or variable, 100 ppm to 3%
Formation temperature	~250°C to 100°C

Characteristics	Descriptions
Ore fluid chemistry	Low to moderate salinity, low CO_2, H_2S
pH of ore fluid	Near neutral
Gold transport	Bisulfide complex
Source of H_2O	Meteoric, ± magmatic
Source of CO_2	Igneous or carbonate rocks
Source of H_2S	Magmatic, sedimentary rocks
Depositional mechanisms	Boiling and mixing, ± sulphidation, ± oxidation

Figure 8-1 Schematic of Epithermal Deposits (adapted from; Rhys et al., 2020)



9. EXPLORATION

Exploration activities have been undertaken by Prime and the previous owners of the Property.

9.1 Grids and Surveys

The Coordinate System used is WGS84 UTM Zone 13 North. The Project's control points are tied into control points of INEGI, the National Institute of Statistics and Geography, an autonomous agency of the Mexican Government. In March 2021 accompanying a helicopter supported geophysical survey, LiDAR digital elevation data was collected by Pioneer Exploration Consultants Ltd., along 1,050 line-kilometres, with 50 metre line spacing over most of the Property, resulting in 20 - 50 centimetre resolution data. Actual elevations occurring in the survey block ranged from 325 to 1475 masl. In April 2022 and May 2024, a contractor (Unmanned Aerial Services Incorporated) performed LiDAR surveys with an Elios 3 drone, a handheld and remote controlled small, tracked unit to the extent possible of +45 adits, shafts, and underground workings within the main area of interest at the Project. This data was tied into control points and the data added to the geological and resource model as historically mined voids.

9.2 Geological Mapping Program

Prime personnel undertook geological mapping in late 2020 and have continued to date, the mapping now covers more than 60 square kilometres. Regional geological mapping (1:5,000 scale) is working towards covering the complete claim group and this has been complimented with detailed geological mapping (1:2,000 scale) over areas previously identified as containing mineralization and new areas identified during the regional mapping.

High-potential areas identified through mapping are:

Tahonitas (southeast) - This area is at the southernmost end of the Z-T Trend. Mapping has defined the extension of the structure more than 800 m further to the southeast than where drill defined. The structure contains faulting, quartz breccias, quartz veins and veinlets with strike similar to the main Z-T Trend.

Las Primas - Mapping has better defined the prospect with a rhyolitic dike with two quartz veins inside the dike and quartz stockwork zone on the border of dike in contact with the volcanic andesite rock.

Fresnillo - This area is between the Z-T and Central Trends. Mapping defined structures as quartz breccias, quartz veins and veinlets with strike similar to Zapote and Noche Buena, the difference is the structures/mineralization are hosted in a dacite intrusive. Surface sampling returned elevated gold and silver values.

300 Trend (Zapote West) - Mapping west of Mariposa identified a structural system with quartz/breccia veins/veinlets trending 300 degrees, with a strike length of more than 500 metres. It is located on the west side and joins into the Z-T trend at Zapote South. Surface sampling while mapping returned elevated gold and silver values up to 0.811 g/t Au.

Orito trend - Mapping defined 2-3 regional structural systems NW40-50SE, with zones of quartz breccia, quartz vein-veinlets and stockwork, evidence mineralization similar to those encountered in other areas. This area appears to be higher in elevation, but further exploration is required.

On the north-central part of the Project, north of San Miguel East and Guadalupe East, there are structures demonstrating evidence of mineralization, such as quartz breccias quartz vein-veinlets with strike similar to the Orito trend and others associated to rhyolitic dikes with strike E-W. Further exploration is required on these structures.

9.3 Rock and Soil Sample Programs

In late 2019, Prime personnel began exploration by systematically trenching and sampling road-cuts over approximately 5,000 metres. The program focused on sampling across outcrops along known mineralized structures. This program was designed to obtain continuous surface grades in select areas that, when combined with historical drill hole data, assisted to advance the geological model. Prime has continued to collect rock samples which include adit, channel, chip, float and grab samples as part of the geological mapping program. Table 9-1 shows the total number of rock samples taken and the number of samples ≥ 0.2 g/t Au and ≥ 20.0 g/t Ag. All trench and roadcut samples were 1.5 metres in length. Adit samples varied from 0.5m to 2.0m. QA/QC (as defined below) samples include standards, blanks, and check assays on selected mineralized samples and the shoulders to mineralized zones. Figure 9-1 shows the locations of the trench, road-cut and adit samples and Figure 9-2 shows the locations and range of Au concentrations of the mapping samples.

In addition, 4,251 soil samples were collected by Prime along with 157 duplicates, Figure 9-3 shows the locations. A geochemical study was undertaken by Heberlein Consulting at the request of Prime in November 2021 to review historical soil samples along with Prime rock and soil samples in the main area at the Property. This study of historical and new soil and rock geochemistry successfully identified the known mineralized structures and identified potential targets for further investigation, including the Fresnillo and Las Primas targets (Heberlein, 2021).

In addition to engaging external consultants, Prime continuously evaluates geochemical data internally to refine exploration targeting in the Los Reyes district. Data collected to date shows a strong spatial correlation between Au and Ag, As, and Sb in the Z-T and Central Zones, with As and Sb anomalism observed at lateral distances up to 100m from Au-Ag mineralization. A systematic increase in Cu, Pb, and Zn with increasing depth typical of many low sulphidation epithermal Au-Ag deposits has not yet been confirmed in the Z-T and Central zones; this is likely due to the relative lack of deep drilling in these target areas. However, mineralization at Guadalupe East does show a tight spatial correlation between Au, Ag, and Cu, in addition to displaying similar broad As and Sb anomalism to the Z-T and Central Zones. The presence of elevated Cu, along with generally higher Ag/Au ratios at Guadalupe East, may suggest that mineralization in this zone formed at higher temperatures than in the Z-T and Central zones. All zones of potentially economic Au-Ag mineralization discovered to date show evidence of K addition and corresponding Na-Ca depletion within and immediately adjacent to precious metals mineralization. This is consistent with the presence of adularia in many areas of high-grade Au-Ag mineralization and the observed alteration of feldspars to illite and sercite in the surrounding wallrock.

9.4 Geophysics

An airborne magnetic-radiometric survey was completed in March 2021 and interpreted by Campbell and Walker Geophysics Ltd. A total of 1,056 line-kilometres of combined magnetics, gamma-ray spectrometry and VLF-EM were successfully acquired and processed. A series of transformations and derivatives applied to the magnetics highlighted the structural fabric of the Property. Northwest- to west-northwest-striking magnetic linears or trends correlate in large part to the known mineralized structures. Additional linears and/or inferred structures are apparent southwest from the Zapote - Tahonitas trend, and may cut through, extending further northwest; one such feature is provisionally termed the ‘Zapote 300’ trend. A number of pronounced Th/K ratio ‘low anomalies’ are mapped by the radiometrics; three of these correlate very well to the known mineralization. Three other Th/K lows appear to coincide with established target zones, Orito, La Verde/ El Tule and Las Palmitas zones. Overall, the gamma-ray spectrometry mapped positive correlations to anomalous mineralization (Campbell, 2021). The VLF-EM results highlighted several prominent shear zones, with associated offsets, breaks. Power transmission lines cutting across/through the survey area presented issues, but overall, the VLF-EM provided some benefit and confirmation of regional structural trends.

Table 9-1 Rock Sampling Program

<table>
<tr><th>Sample Type</th><th>Sample Count</th><th>>= 0.2 g/t Au</th><th>>= 20.0 g/t Ag</th></tr>
<tr><td>Trenching</td><td>2894</td><td>827</td><td>408</td></tr>
<tr><td>Roadcut</td><td>2083</td><td>522</td><td>240</td></tr>
<tr><td>Adit</td><td>585</td><td>174</td><td>105</td></tr>
<tr><td>Chip/channel</td><td>2749</td><td rowspan="4">276</td><td rowspan="4">120</td></tr>
<tr><td>Grab</td><td>41</td></tr>
<tr><td>Float</td><td>19</td></tr>
<tr><td>Undefined</td><td>3</td></tr>
<tr><td>QA/QC</td><td>790</td><td>N/A</td><td>N/A</td></tr>
<tr><td>Totals</td><td>9164</td><td>1799</td><td>873</td></tr>
</table>

Figure 9-1 Los Reyes Trench, Roadcut & Adit Sampling

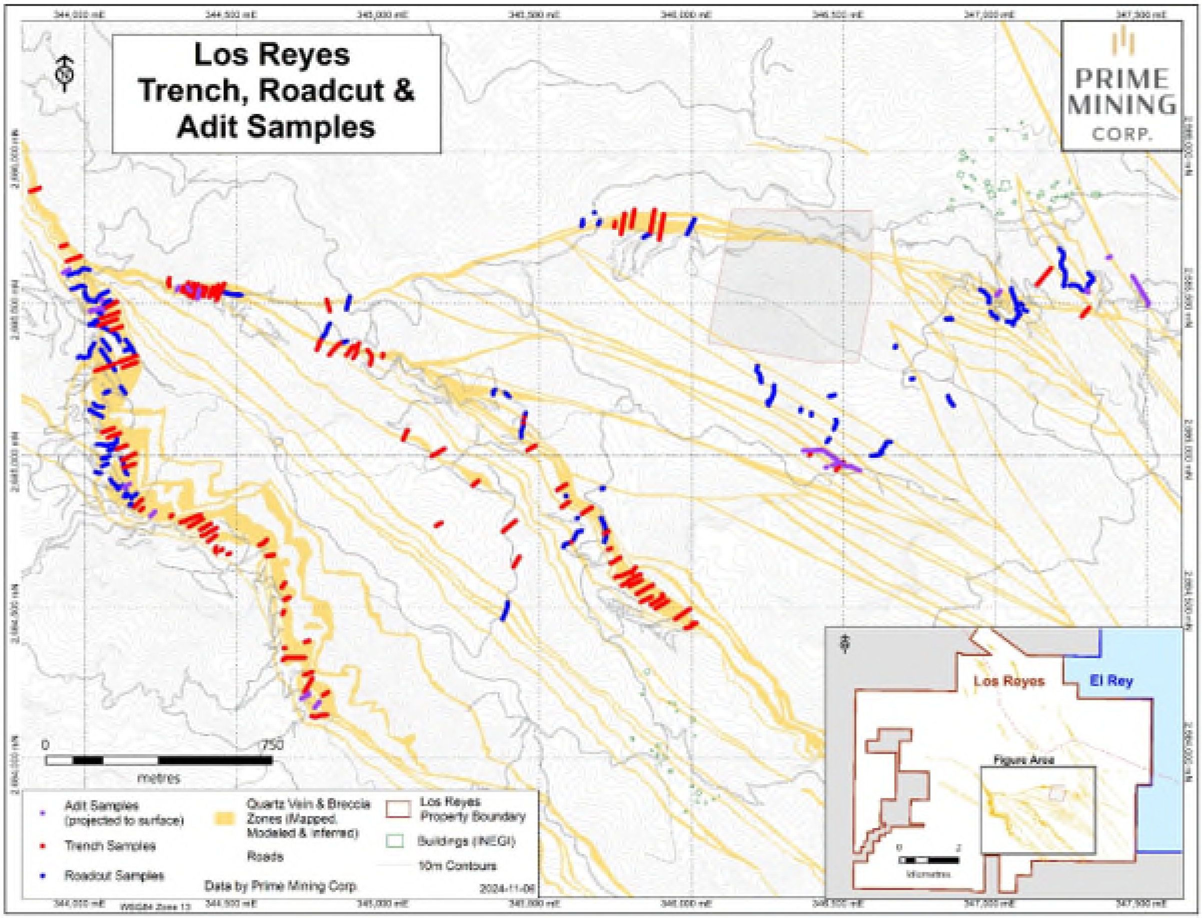


Figure 9-2 Los Reyes Mapping Samples Locations

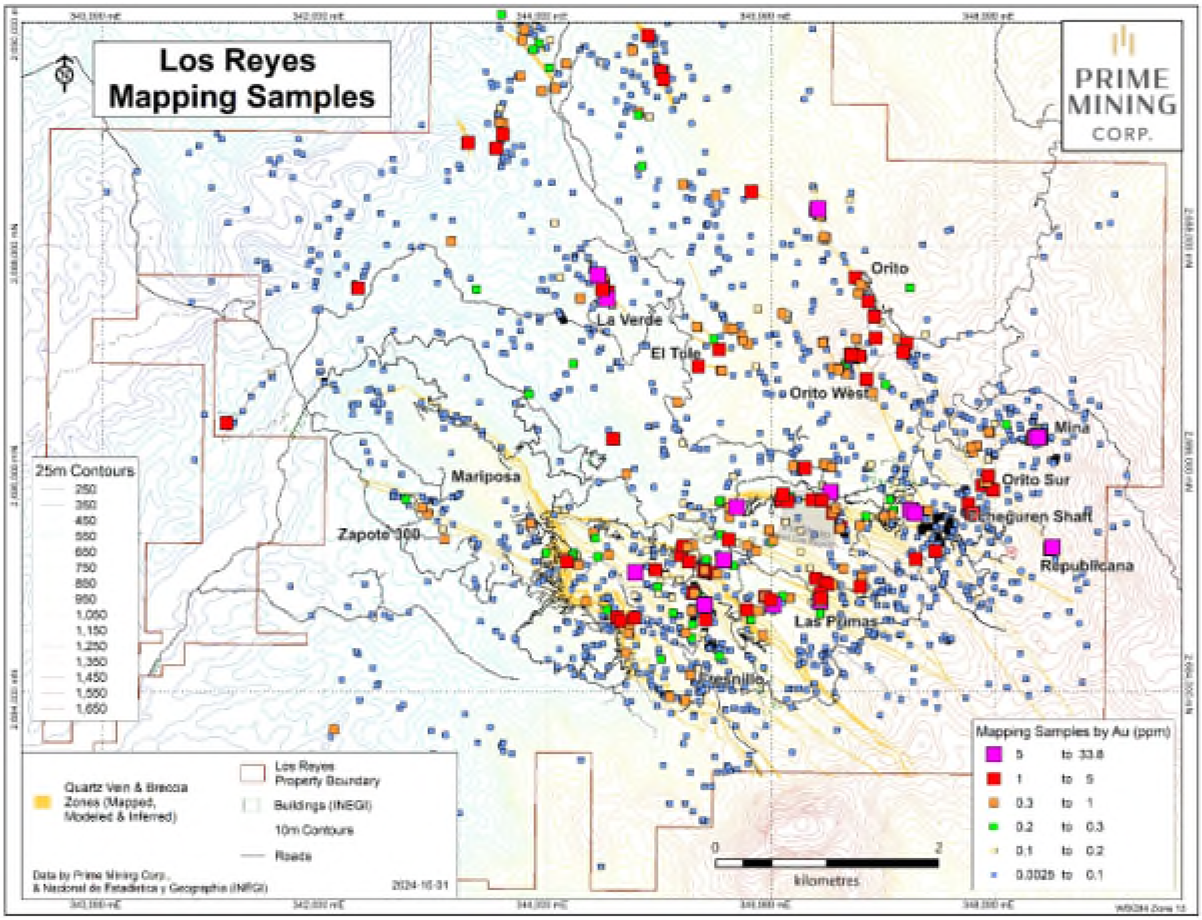
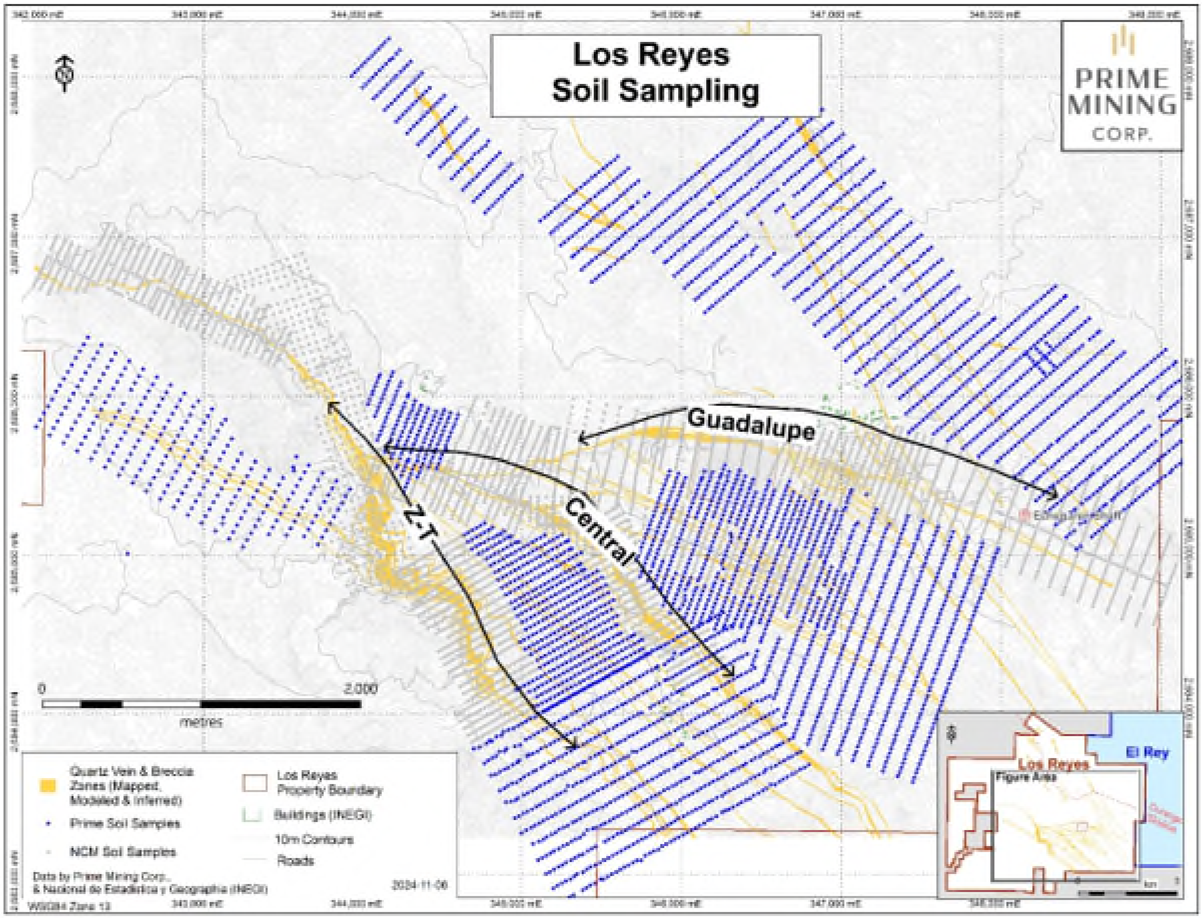


Figure 9-3 Los Reyes Soil Sampling



9.5 Spectral Mineralogy and Magnetic Susceptibility

Prime employs a TerraSpec Halo mineral identifier, an instrument developed by ASD, to systematically collect mineralogical data from drill core and surface samples across the Property. The instrument measures the visual, near-infrared, and short-wave infrared ("VIS-NIR-SWIR") regions (350-2500 nanometres) and is used to assist in exploration vectoring by identifying minerals associated with hydrothermal alteration. Spectral data are collected from cleaned, dry drill core at regular intervals, typically at 3 to 6 metre increments in non-mineralized host rock and at 0.7 to 1.5 metre increments in intervals showing visible alteration or quartz veining. The raw spectral data are then processed using The Spectral Geologist software, developed by CSIRO for analysis of VIS-NIR-SWIR data, to determine principal alteration minerals and to calculate additional scalars such as illite crystallinity and kaolinite crystallinity. The December 31, 2022, TerraSpec dataset includes analyses from 44 drillholes and 1,056 surface samples.

Spectral data collected to date suggests that the Property is characterized by an alteration zonation pattern typical of many low-sulphidation epithermal Au-Ag deposits (Hedenquist, et. al., 2000). Quartz-adularia-sericite(muscovite) alteration is observed within hydrothermal upflow zones and is often present at lateral distances up to 10-30 metres from ore-grade Au-Ag mineralization. Illite alteration is dominant at intermediate distances (generally 30-75 metres), typically with increasing illite crystallinity and a transition to more muscovitic compositions as the ore zones are approached. Distal alteration is typically characterized by a transition from illites to smectites with increasing distance from mineralization, and chlorite-epidote is dominant at distances greater than 100 metres from the ore zone. While near-paleosurface expressions of hydrothermal alteration such as sinter and opaline silica are generally absent at the Property, kaolinite is occasionally observed at high elevations and may reflect the remnants of steam-heated alteration associated with the Los Reyes system.

Magnetic susceptibility measurements are also collected from cleaned, dry drill core on the same intervals as the TerraSpec Halo data, using a KT-10 handheld magnetic susceptibility metre developed by Terraplus Inc, and Georadis S.R.O. Andesites and andesitic tuffs across the Property are generally weakly magnetic, and magnetite destruction associated with hydrothermal alteration can therefore be an important vector for mineralization in these host rocks. Magnetic susceptibility data collected to date suggests that de-magnetization in andesitic host rocks can be observed at lateral distances up to 20-30 metres from mineralized structures.

9.6 Remote Sensing

Remote Spectral Geology is the measurement and analysis-interpretation of spectral satellite data to identify different rock types and surface materials, their mineralogy, and their mineralization-alteration signatures. Prime engaged an external consultant to generate a set of spectral images to reflect the local geology, showing variations in rock types, mineral associations, mineral zoning/vectoring. Results to date have confirmed the regional geological trends and alteration. This work is ongoing and further processing of spectral data is required.

10. DRILLING

10.1 Introduction

The Project has been drilled by several operators since 1993. Please refer to Section 6 – History for a review of the historical work, specifically, Section 6.2, for a review of the drilling done prior to Prime taking ownership of the project.

From late 2020 to the 2024 MRE cut-off of July 17, 2024, Prime has drilled 199,452.76 metres in 688 completed drill holes. Total drill samples submitted are 126,381 plus approximately 8,000 samples to check quality control and quality assurance ("QA/QC") representing approximately 182,363.84 metres of drilled rock. Some holes were not sampled or assayed in their entirety, particularly holes that were drilled from coincident collars that were fully assayed or areas with sufficient sampling of wall rock.

Of the total number of Prime drill holes, 654 (191,451.03 metres) were included in the MRE while the remainder were outside the resource block model extents. Table 10-1 summarizes the Prime drilling and the drill hole locations are shown by year in Figure 10-1 to 10-4. The two drill holes started in 2020 are included in the figure showing the 2021 drill holes.

Table 10-1 Summary of Prime Drilling

Company		Prime Mining Corp.				
Year		2021 [1]	2022	2023	2024 [4]	Sub-total
Guadalupe	Core drill holes	37	89	24	11	161
	Core metres	10,169.3	33,419.5	8053.3	3911.0	55,553.0
	RC drill holes	5	16	0	0	21
	RC metres	1127.35	3553.26	0	0	4680.6
	Total drill holes [2]	42	105	24	11	182
	Total metres	11,296.6	36,972.8	8053.3	3911.0	60,233.6
Z-T	Core drill holes	59	81	81	40	261
	Core metres	11,733.55	19,701.8	27,251.7	14,172.5	72,859.6
	RC drill holes	0	19	0	0	19
	RC metres	0	3652.37	0	0	3652.4
	Total drill holes	59	100	81	40	280
	Total metres	11,733.6	23,354.2	27,251.7	14,172.5	76,511.9
Central[3]	Total drill holes	31	44	29	6	110
	Total metres	6768.55	10,096.65	8750.6	1937.2	27,553.0
Other	Total drill holes	24	17	50	25	116
	Total metres	5301.98	4387.5	14,840.2	10,624.55	35,154.2
Total	**Total drill holes [2]**	**156**	**266**	**184**	**82**	**688**
	Total metres	**35,100.7**	**74,811.1**	**58,895.8**	**30,645.3**	**199,452.8**

Notes:

1. 2021: Two drill holes were started in December 2020, one of which was completed in 2020.
2. Total Drill Holes: Drill hole count and metres are counted in the year the drill hole was completed.
3. Central: Drilling in the Central areas and other areas were core drill holes only.
4. 2024: July 17th cutoff.

Figure 10-1 Los Reyes Prime Drilling 2021

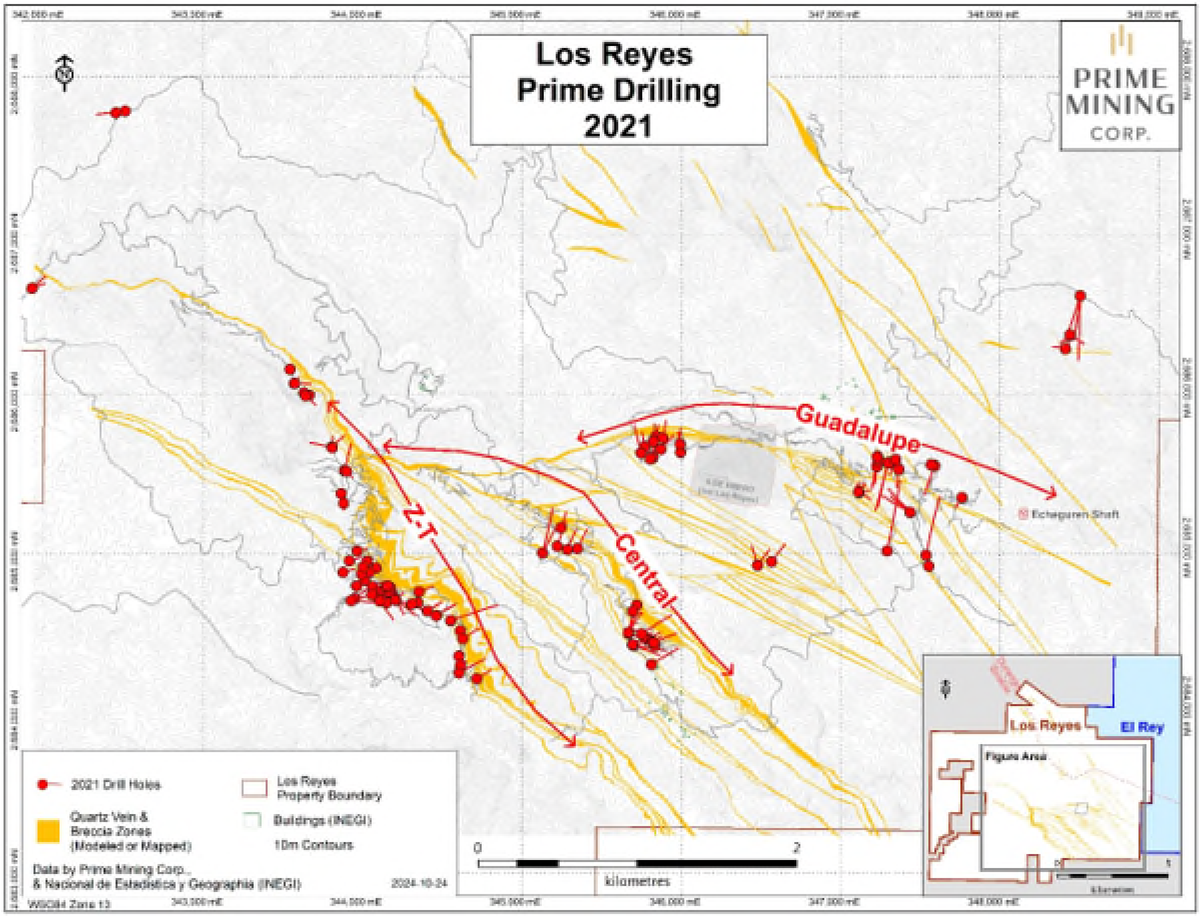


Figure 10-2 Los Reyes Prime Drilling 2022

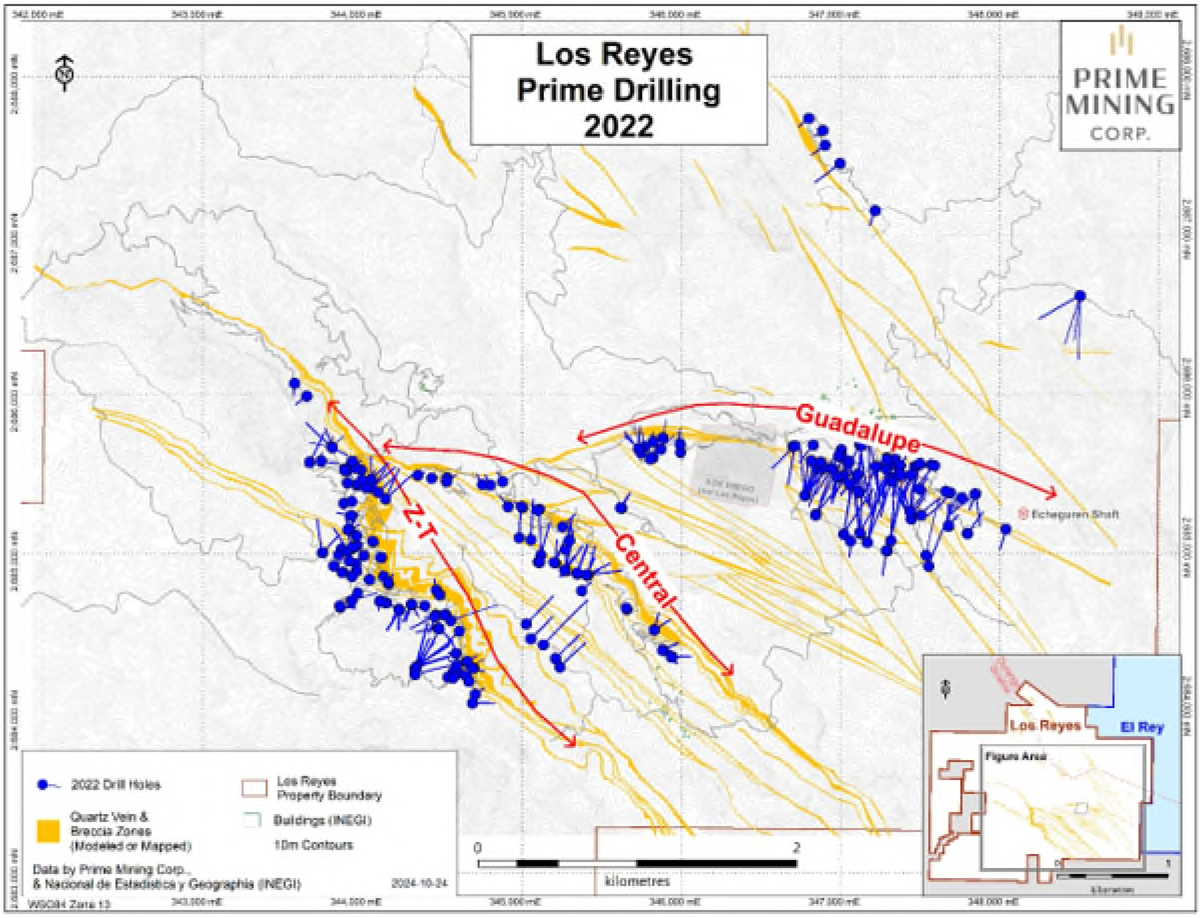


Figure 10-3 Los Reyes Prime Drilling 2023

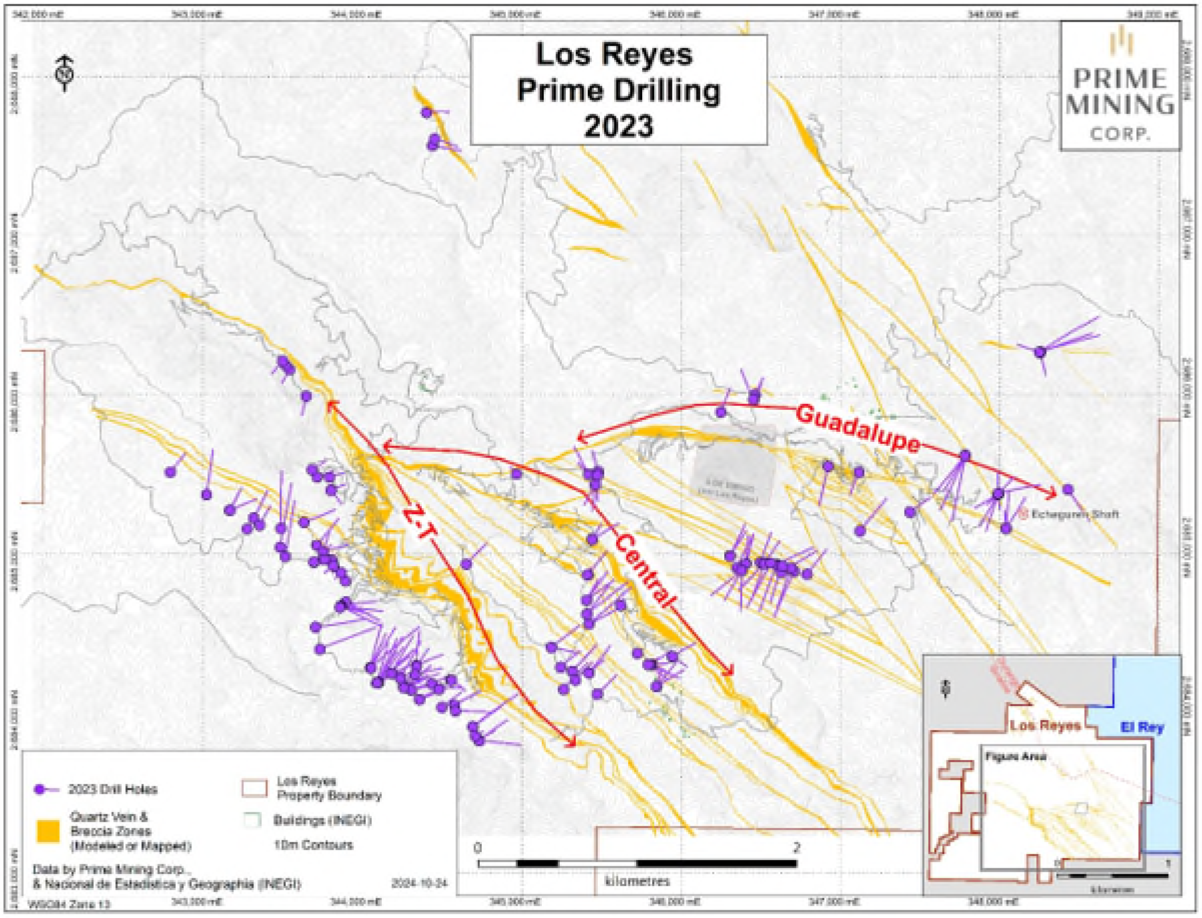
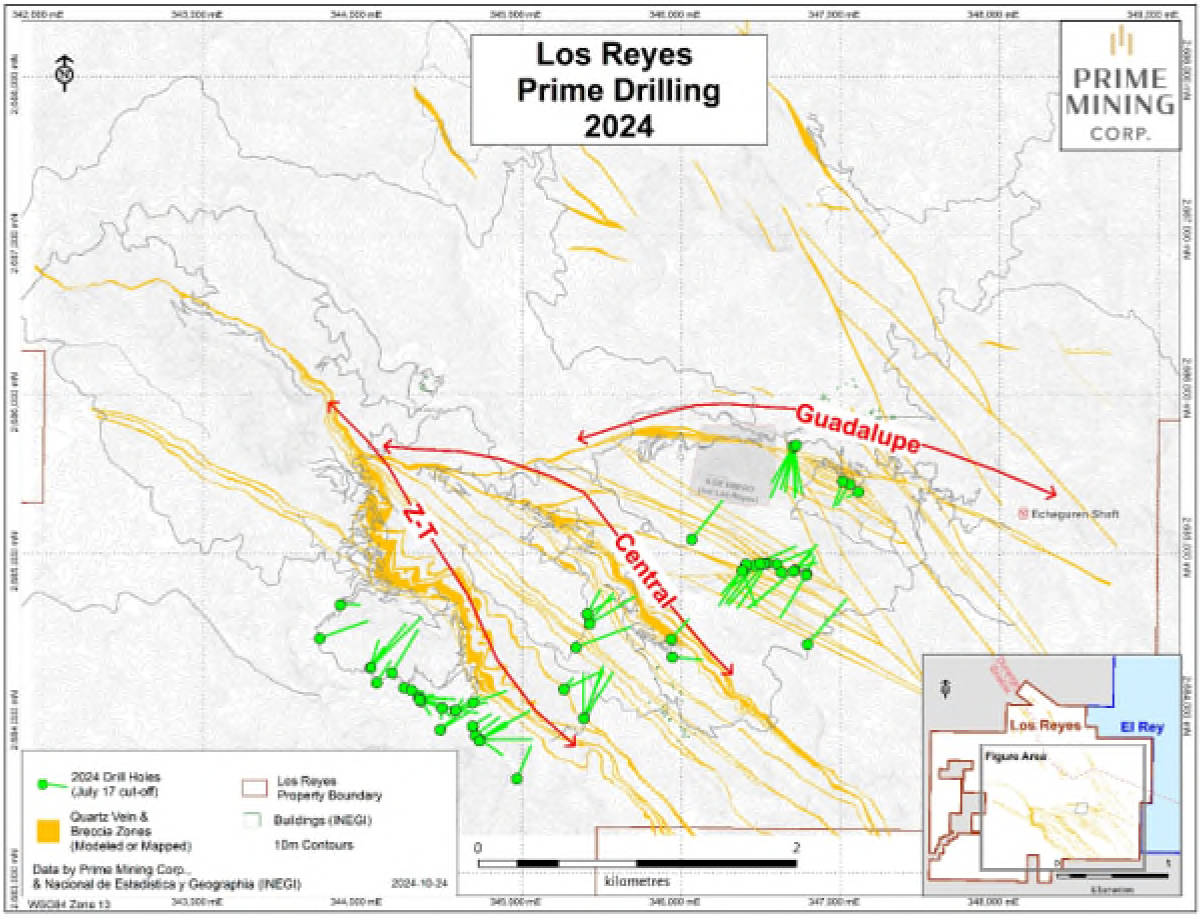


Figure 10-4 Los Reyes Prime Drilling 2024



Six hundred and forty-eight drill holes (191,119.8 metres) were core holes, all started as HQ size core and due to ground conditions forty-five drill holes were reduced to NQ size core. Forty of the drill holes (8,333.0 metres) were RC drill holes. Twenty-one RC drill holes were drilled in the Guadalupe area (4680.6 metres) and 19 RC drill holes were drilled in the Z-T area (3652.4 metres). Two drill holes (799.4 metres) were collared as RC holes, drilled to a predetermined depth and finished as HQ size core.

Drill holes are planned by Prime geologists and screened and prioritized on an ongoing basis, typically during a weekly planning session, for the highest potential in defining mineralization within each mineralized domain and the optimal distance from previous mineralized intervals. Drill holes have been drilled to confirm historical results, infill gaps in geological knowledge or mineralization continuity, and step-out along strike and down-dip from known mineralization to expand Inferred mineralization. Modelling of each zone of mineralization has been ongoing and is used to support new proposed drilling.

Drill holes are identified using an ID code utilizing the year the hole was started, a two to four letter area designation, and a sequential number. RC holes have an "R" suffix added to the drill hole name, and holes started as RC and completed with core collection have an "M" suffix.

10.2 Accuracy and Reliability of Results

The first 321 drill holes were sampled in their entirety submitting sawed half core to the assay laboratory to minimize sample bias. Starting in August 2022, core intervals were selectively submitted for assay analysis avoiding submitting unaltered rock and rock with no evidence of significant quartz veining that were previously sampled and submitted in close-by drill holes. To be conservative Prime has still submitted over 83% of all core meters drilled. In some circumstances, core recoveries within the mineralized corridors were poor due to faulting/shearing which could impact the accuracy of the results by either understating or overstating gold or silver values. Prime is working diligently with the drill companies to achieve sufficient recoveries within difficult zones and holes may be redrilled if recoveries are deemed insufficient. Sampling in zones of broken core is done by hand with the aim to avoid biasing the submitted sample and maintain a representative sample.

10.3 Drill Collar Alignment and Surveys

Alignment of the drill rigs is done using a Reflex TN14 Gyrocompass™, which takes approximately 10 minutes to complete its self-calibration following which a drill rig can be aligned to the correct planned azimuth and dip within minutes. The tool has a dip range of +/- 90° and Azimuth range of 0° to 360°, with no magnetic affectation.

Following completion of the drill hole and after site reclamation, the collar location is monumented by cementing a plastic tube into the drill hole with the drill hole name written in the cement. A Sokkia™ i-X600 total station is used to survey the location to a precision of two millimetres.

10.4 Down-Hole Surveys

Downhole surveys are done every 20 metres on the way down and from the bottom of the hole back to the collar with a DeviShot™, multishot survey tool, which provides high precision measurements of the azimuth and inclination. Certain hole conditions, such as large voids, rubbly fault zones, and strongly fractured rock, prohibit the use of the tool and in these situations, the next closest planned depth measurement is collected.

10.5 Orientated Core Measurements

Some core drill holes were selected for oriented core measurements to precisely measure the orientation of veins and structures encountered in the drill hole. A wireless Devicore BBT tool is used by a trained geologist to determine the orientation of the axis of the core using the Devicore BBT visual help system. The tool uses three high-accuracy accelerometres to measure inclination, orientation, gravity vector, and temperature. Once the alignment of the core is determined by the tool, a line is drawn on the core which marks the starting point for all geotech data collection. Orientated core measurements are used extensively in the modelling of the structures and veins.

10.6 Core Handling, Logging and Sampling Procedures

Drill core is placed directly into the core boxes by the driller's helper with any recovery gaps noted using a wooden block with the depths recorded. Orientated core is handled by a drill-site geologist trained in handling the instrument and marking of the core. Core boxes are prelabeled with the hole ID and box number. Wooden blocks are placed at the end of each drill rod run marked with the depth of the end of the interval. Each box is secured with a lid and remains at the drill rig under the supervision of the driller until the managing geologist makes his twice daily rounds to check on the rig and pick up the core boxes. The geologist ensures the boxes are correctly labelled with hole ID and box number and securely closed prior to loading them for transport to the logging facility. During 2021, the core logging facility was on the Property in the village of El Saucito. In 2022 and subsequent years, core logging was completed at the Company's office facility in Cosalá.

Once the core boxes are delivered to the core logging facility, they are laid out in sequence for a brief description of the core called a Quick Log. The Quick Log is included in the Daily Report which is disseminated to the Company's senior geologists and management. The core is then queued up for thorough logging, usually within a few days after completion of the hole.

When the core is ready for logging, the core boxes are laid out in sequence, cleaned and reassembled. Geotechnical information including core recovery, rock quality designation ("RQD"), fracture count, core strength, degree of natural breakage, and weathering is recorded digitally. Prior to mid-April, 2024, the data was recorded into Prime's custom-built Microsoft Access™ Capture software, called a Geoscience Database Manager ("GDM"). Each drill hole had its own Access™ Capture preloaded by the project manager with the drill hole location and set-up parameters. Beginning in mid-April, 2024, the Company used a customized version of MaxGeo's LogChief software to capture geotechnical and geological data, which is uploaded to MaxGeo's cloud-based DataShed5 database.

Each core box is labelled with the interval depths at top and bottom and metal tags showing the drill hole ID, box number and from / to intervals are stapled to one end of the box.

The core is then logged by geologists into the software recording a complete description of the rock including lithology, alteration, key mineralization, textures, veining, oxidation state, and colour. All structures are recorded by down-hole depth, type, alteration mineralogy, widths, and angle relative to the core axis. If the core orientation tool was used then additional measurements of the true dips of veining and structures are calculated, and more detailed descriptions of the faults, fractures and veins are recorded.

Once the core has been logged, the geologists mark the core for sampling. A saw line is marked along the axis of the core, rotating the core where necessary to ensure that significant structures are bisected by the cut, by drawing two closely spaced parallel lines, one red, the other blue, down the length of the core. The length of the sample is determined by the geologist based on the lithological characteristics. Prior to August 2022, maximum sample intervals were typically 1.5 metres in length. Subsequently, maximum intervals were typically 2.0 metres. Minimum sample intervals are typically 0.5 metres with rare exceptions. The longer length samples are well outside of expected mineralized zones, with shorter intervals closer to the expected mineralized zones. Within the anticipated mineralized zones, sample lengths are subject to their geological characteristics. Sample intervals are marked on the core and core box, with sample tags stapled to the box. Sample intervals are recorded into the software along with QA/QC samples. QA/QC measures include certified reference materials ("CRMs") inserted into the sample stream at preset intervals (every sample ending in 33 or 99) and barren rock (called blanks) within probable mineralized zones. Field duplicates were taken prior to November 2022 but ceased following the recommendation of an independent review of the Company's QA/QC practices and results (Jolette, 2022). In the review, it was noted that field duplicates can be useful at the beginning of a project to understand variability, but longer term is not necessary. Up to November 2022, field duplicates were collected at every 50th sample by cutting the half core sample into two quarter core samples and submitting the duplicate as the fifth sample below the original (original sample 00 and 50, duplicate sample as 05 and 55). The laboratory is instructed to prepare a pulp duplicate (also known as an assay duplicate) for every sample ending in 75 and a prep duplicate (also known as a core duplicate) for every sample ending in 25.

Prior to the core being cut and sampled it is photographed using a high-resolution digital camera set up on a stand. Both wet and dry photos were taken prior to August 2022 but subsequently after reviewing industry best practice only wet digital photos are taken. Photos include the drill hole ID, core box number, interval from and to, with a measuring tape for scale. A colour palette was introduced in 2024. Sample intervals and tags are visible in the photos.

At the core cutting and sampling stage, a technician is instructed whether the drill hole is to be sampled entirely or if only selected intervals will be submitted. Core is cut using a diamond disk saw utilizing a stream of water to cool and clean the saw blade. The core is sawed in half between the lines drawn by the geologist; the half core with the red line is returned to the core box and the half core marked with the blue line is submitted for assay. For friable, incompetent or rubbly core, the technician samples half the core based on markers set by the geologist. Each sample is collected and bagged in pre-labelled poly-ore bags with half the sample tag inserted. The technician checks that the core box sample tag and poly-ore bag sample tag numbers match. After each sample, the saw tray is washed, and the sample bag is closed. After sampling, the core boxes are moved to the Company's secure, long-term storage facility.

10.7 RC Chips Handling, Logging and Sampling Procedures

The RC drilling provides rock chips up to 3.0 centimetres in size and pulverized rock material. Drill runs are 1.525 metres in length (5.0 feet) which makes up each sample. A full run recovers an average of 27.3 kilograms of rock. Rock cuttings are collected straight from the cyclone in a bucket which is then separated into two parts using a splitter. One half is discarded, and the second half is split again, collecting each half in a pre-labeled micropore sample bag containing a portion of the sample tag. A retained portion of the sample tag records the hole ID, from and to interval, geologist and or sampler's name, and the date. One sample is retained at the Company's secure storage facility and the other submitted for analysis. Representative samples of RC chips and dry, fine material from each run are placed in pre-marked chip trays, one for coarse chips and one for fine material, labelled with the drill hole ID and each sample interval. Chip trays are digitally photographed.

Logging of the RC chips is done at the drill site by a geologist using a sampling of the chips collected from the entire drill run. Chips are washed and a binocular microscope is used to identify the lithology and any other rock characteristics discernable such as alteration, textures, general colour, percentage of key minerals, estimated quartz vein content and characteristics, oxidation characteristics and any specific comments. This information, collected for each run, is recorded on a paper form, and transferred to the Capture software after the hole is completed.

QA/QC measures are the same for the RC samples as for the core samples.

10.8 Density/Specific Gravity Measurements

Field measurements of the density of the rock are made by cutting a whole core puck about two centimetres in thickness, measuring the diameter and length (averaging five measurements of each), and weighing the puck on a high precision scale as fresh core and again after two hours in a drying oven, then after another one hour in the oven, repeating until the sample weight is constant. The density is then calculated by dividing the final dry weight by $\pi r2*l$, where π is the mathematical constant pi, r2 is the radius (average half diameter) squared, and l is the average length of the puck. The Company collected 4,776 density measurements on core pucks from ore zones and a variety of country rock. Of these, 509 were submitted to Bureau Veritas ("BV") for specific gravity ("SG") determination by waxed core, water immersion method. In addition, 81 of the core pucks were submitted to ALS for SG determination by waxed core, water immersion method. Comparison between the three measurement methods shows that the caliper field measurements generally reproduce the lab-reported values well, but are 1% lower, on average, compared to the BV wax immersion measurements, and 5% lower, on average, compared to the ALS wet density measurements.

Density measurements were filtered by lithology and alteration. See Chapter 14 for a further discussion of the results.

10.9 Data Handling

Prior to migrating to the MaxGeo data collection system, the Company used a custom-built Microsoft Access™ Capture software program that contains most of the pertinent information recorded from the drill coordinates and set up parameters through to the photography and sampling intervals. The project manager reviewed the data before handing off a copy via Microsoft SharePoint™ to the data manager who imported each Capture into a Microsoft SQL Server™ database. The data was reviewed, and collar, survey and lithology files were exported and checked for integrity prior to being disseminated to the geological team. Assay results were received from the laboratory and uploaded into SQL Server™ using the Access™ GDM. The software paired the assay data with the sample data and sorted the QA/QC data for quick review.

The MaxGeo software system uses a customized version of their LogChief software which collects essentially the same information as the Capture software. This data is validated by the project manager then uploaded to MaxGeo's Cloud-based DataShed5. The data manager reviews the data and disseminates a simplified version of the data to the geological team. Assay results are merged into the sampling data using the DataShed5 export and Microsoft Excel™ and Microsoft Access™.

Assay data is checked, and composite intervals are calculated. Assay data is then disseminated to the Company's senior geologists for review and interpretation including determination of estimated true widths ("ETW") of mineralized intervals.

Mineralized intervals and/or the immediate shoulders are selected for check assay at a different laboratory on about 5% of the samples. Check assays were done on both rejects and pulps prior to September 2022 and subsequently only pulps following the recommendation of an independent review of the Company's QA/QC practices and results (Jolette, 2022).

10.10 Results and Interpretation

10.10.1 *Z-T Trend*

Prior to Prime's drilling campaigns, three deposits were recognized within the main structure along the Z-T trend: Zapote North, Zapote South and Tahonitas to the south. Prime drilling proved that low grade mineralization is more or less continuous along the structure punctuated with generally south plunging higher grade mineralized shoots and apparent north plunging or near vertical higher-grade shoots that may be related to northeast/southwest crosscutting structures. Gold and silver mineralization is generally contained within quartz veins and breccia zones. These mineralized zones anastomose within the structure and there are also mineralized veins parallel to the structure and vein splays, particularly at shallower elevations in the southern part of the deposit. The Z-T structure remains open along strike to the SSE and NNW.

Prime has drilled 280 holes into the Z-T trend, not including Mariposa, totalling 76,511.9 metres. Of these, 19 were RC holes (3,652.4 metres) and 261 were core holes (72,859.6 metres).

Historical drilling focused on shallow tests along the strike of the structure. Prime's drilling focused mostly on step-outs down dip as well as step-outs along strike. An example of Prime's drill results from Z-T are shown in Tables 10-2 to 10-4 sorted by historical deposit area, from north to south and listed by collar location from north to south. The locations of these selected holes are shown labeled in Figure 10-5 along with the projected trace of other drill holes. Representative cross sections are in Figures 10-6 to 10-8 and their location is shown on Figure 10-5.

Table 10-2 Z-T Drill Results Summary (Zapote North)

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
22ZAP-56	186.7	189.0	2.4	1.7	4.80	17.0	562.0
22ZAP-56	235.5	243.0	7.5	5.3	0.20	7.0	511.0
22ZAP-56	247.5	252.0	4.5	3.7	0.20	5.0	501.0
21ZAP-31	51.5	60.5	9.0	6.4	0.50	6.0	694.0
21ZAP-31	65.8	68.5	2.7	1.9	0.20	4.0	686.0
21ZAP-31	112.5	114.0	1.5	1.1	0.30	8.0	654.0
21ZAP-31	132.0	133.5	1.5	1.1	0.20	8.0	640.0
21ZAP-31	136.5	144.7	8.2	5.8	0.50	31.0	634.0
including	139.5	140.5	1.0	0.7	1.60	100.0	634.0
21ZAP-31	148.0	153.0	5.0	3.5	0.40	25.0	627.0
23ZAP-116	29.3	30.4	1.2	1.1	0.30	3.0	664.0
23ZAP-116	43.6	45.0	1.4	1.4	0.30	10.0	650.0
23ZAP-116	86.6	87.5	0.9	0.9	0.30	1.0	610.0
23ZAP-116	137.3	138.2	1.0	1.0	1.30	3.0	562.0
23ZAP-116	141.8	144.0	2.3	2.3	0.30	6.0	558.0
23ZAP-116	169.8	174.0	4.3	4.3	0.60	10.0	530.0
including	173.2	174.0	0.8	0.8	1.70	22.0	528.0
23ZAP-116	188.8	189.7	1.0	1.0	2.90	4.0	514.0
22SMW-01	0.0	18.0	18.0	11.6	0.70	19.0	729.0
including	4.5	6.0	1.5	1.0	2.00	23.0	736.0
22SMW-01	19.0	20.1	1.1	0.7	0.30	19.0	721.0
22SMW-01	21.0	22.5	1.5	0.9	2.30	42.0	720.0
22SMW-01	24.9	47.5	22.6	13.0	1.80	23.0	709.0
including	29.5	31.5	2.0	1.1	3.40	13.0	709.0
& including	35.5	38.5	3.0	1.7	3.10	24.0	709.0
& including	42.0	45.0	3.0	1.7	4.60	47.0	701.0
22SMW-01	52.0	55.0	3.0	1.9	0.50	14.0	697.0
22SMW-01	81.0	82.5	1.5	1.1	0.20	2.0	677.0
22SMW-01	143.0	144.5	1.5	1.5	0.40	9.0	633.0
23ZAP-121	72	73.4	1.4	1.3	0.50	9.0	643.0
23ZAP-121	76.9	81.3	4.4	4.2	0.60	10.0	638.0
including	76.9	78.5	1.6	1.5	1.10	15.0	639.0
23ZAP-121	86.7	87.5	0.9	0.8	0.40	6.0	630.0
23ZAP-121	89.9	90.9	1.1	1.0	1.60	11.0	627.0

Notes:

1. Elevations are at the midpoint of the interval, in metres above sea level (masl).

Table 10-3 Z-T Drill Results Summary (Zapote South)

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
22ZAP-78	134.3	136.0	1.7	1.6	2.20	10.0	455.0
22ZAP-78	174.0	175.5	1.5	1.2	0.20	1.0	423.0
22ZAP-78	259.5	274.5	15.0	10.6	0.50	7.0	347.0
including	261.0	262.5	1.5	1.1	2.50	6.0	353.0
22ZAP-78	279.0	280.5	1.5	1.1	0.20	7.0	337.0
22ZAP-78	282.0	282.9	0.9	0.6	0.20	9.0	335.0
22ZAP-78	285.0	299.5	14.5	10.3	1.30	33.0	327.0
including	296.5	298.0	1.5	1.1	7.90	99.0	321.0
22ZAP-78	338.5	340.0	1.5	1.1	0.40	1.0	288.0
23ZAP-96	165.0	168.0	3.0	2.9	3.00	29.0	509.0
23ZAP-96	255.3	256.0	0.8	0.7	0.20	0.0	505.0
22ZAP-82	197.0	198.5	1.5	1.3	0.30	4.0	463.0
22ZAP-82	203.0	218.0	15.0	13.0	1.30	22.0	452.0
including	211.1	212.0	0.9	0.8	13.00	48.0	452.0
22ZAP-82	219.5	221.0	1.5	1.3	0.30	9.0	444.0
22ZAP-82	222.5	227.0	4.5	3.9	0.30	19.0	440.0
22ZAP-82	228.5	234.2	5.7	4.9	0.40	15.0	434.0
22ZAP-82	238.1	254.0	16.0	13.8	3.60	20.0	421.0
including	245.0	247.2	2.2	1.9	22.20	41.0	421.0
22ZAP-82	254.7	267.2	12.5	10.8	0.40	15.0	408.0
22ZAP-82	274.0	276.7	2.7	2.3	0.30	18.0	396.0
22ZAP-83	87.0	88.5	1.5	1.4	0.20	4.0	547.0
22ZAP-83	99.0	100.5	1.5	1.4	0.20	5.0	535.0
22ZAP-83	111.0	112.5	1.5	1.4	0.70	5.0	524.0
22ZAP-83	128.5	130.0	1.5	1.4	0.50	7.0	508.0
22ZAP-83	133.0	134.5	1.5	1.4	0.20	13.0	504.0
22ZAP-83	136.0	148.0	12.0	10.9	0.50	14.0	502.0
22ZAP-83	152.5	154.0	1.5	1.4	0.40	17.0	491.0
22ZAP-83	154.8	156.0	1.2	1.1	0.30	17.0	489.0
22ZAP-83	158.0	178.5	20.5	18.6	0.90	18.0	478.0
including	162.5	164.0	1.5	1.4	3.30	18.0	482.0
23ZAP-99	307.0	309.0	2.0	1.4	0.30	5.0	402.0
23ZAP-99	311.9	313.0	1.1	0.8	0.30	12.0	399.0
23ZAP-99	314.5	326.5	12.0	8.5	1.00	23.0	393.0
including	319.0	322.0	3.0	2.1	1.80	41.0	393.0
23ZAP-99	329.5	330.8	1.3	0.9	0.30	7.0	385.0
23ZAP-99	333.0	334.5	1.5	1.1	0.30	17.0	382.0
23ZAP-99	337.0	338.5	1.5	1.1	0.20	4.0	379.0
23ZAP-99	340.0	341.5	1.5	1.1	0.20	8.0	377.0
23ZAP-99	347.0	347.9	0.9	0.6	1.20	8.0	372.0
23ZAP-99	350.5	352.0	1.5	1.1	0.30	13.0	369.0
23ZAP-99	358.0	359.5	1.5	1.1	0.20	6.0	363.0
23ZAP-99	381.3	385.5	4.2	3.0	0.80	23.0	344.0
including	384.0	385.5	1.5	1.1	1.60	24.0	342.0
23ZAP-99	387.5	389.7	2.3	1.6	0.50	26.0	340.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
23ZAP-99	391.8	392.8	1.1	0.7	0.30	2.0	337.0
23ZAP-95A	282.0	283.5	1.5	1.4	0.20	10.0	435.0
23ZAP-95A	288.0	292.4	4.4	4.3	0.40	15.0	429.0
23ZAP-95A	296.6	313.0	16.5	15.9	0.70	37.0	419.0
including	310.0	311.5	1.5	1.4	2.70	155.0	419.0
23ZAP-95A	314.5	316.0	1.5	1.4	0.30	13.0	411.0
21ZAP-27	222.0	223.5	1.5	1.2	0.50	24.0	468.0
21ZAP-27	226.5	230.5	4.0	3.2	0.50	29.0	463.0
21ZAP-27	235.5	240.0	4.5	3.6	0.50	11.0	456.0
21ZAP-32	229.0	249.0	20.0	11.5	0.50	23.0	484.0
21ZAP-32	264.3	292.5	28.3	18.2	1.10	32.0	448.0
including	273.9	274.6	0.7	0.4	8.50	52.0	452.0
& including	276.0	280.7	4.7	3.0	3.10	45.0	449.0
including	278.0	279.2	1.2	0.8	7.80	39.0	448.0
21ZAP-03	140.0	153.0	13.0	10.0	0.80	33.0	580.0
including	145.5	150.1	4.6	3.5	1.70	42.0	579.0
22ZAP-45	43.5	45.0	1.5	1.1	0.20	1.0	705.0
22ZAP-45	177.0	178.5	1.5	1.1	0.30	46.0	581.0
22ZAP-45	181.5	189.5	8.0	5.8	7.80	57.0	573.0
including	183.0	187.5	4.5	3.3	12.50	71.0	573.0
including	186.0	187.5	1.5	1.1	26.50	127.0	572.0
22ZAP-45	193.5	195.2	1.7	1.2	0.20	51.0	565.0
21ZAP-43	151.0	152.0	1.0	0.7	0.30	43.0	617.0
21ZAP-43	154.5	162.0	3.0	2.1	1.90	42.0	612.0
including	154.5	157.5	0.7	0.5	3.30	62.0	614.0
& including	158.4	159.0	7.5	5.3	4.10	73.0	612.0
21ZAP-43	165.0	167.2	2.2	1.5	0.20	8.0	605.0

Notes:

1. Elevations are at the midpoint of the interval, in metres above sea level (masl).

Table 10-4 Z-T Drill Results Summary (Tahonitas)

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
23TA-57	271.0	273.0	2.0	2.0	0.80	6.0	396.0
23TA-57	313.0	314.5	1.5	1.5	0.30	5.0	372.0
23TA-57	321.0	322.5	1.5	1.5	0.20	6.0	367.0
23TA-57	324.0	328.3	4.3	4.2	0.30	15.0	365.0
23TA-57	330.4	340.3	10.0	9.8	1.50	25.0	359.0
including	334.5	336.0	1.5	1.5	7.90	61.0	359.0
24TA-138	135.3	136.6	1.3	1.9	1.00	2.0	541.0
24TA-138	352.2	353.0	0.8	0.5	19.10	1.0	515.0
24TA-138	359.0	361.0	2.0	0.2	4.30	0.0	514.0
24TA-138	404.5	410.2	5.7	2.9	130.00	5.0	508.0
including	405.9	408.8	2.9	5.2	218.30	8.0	508.0
24TA-138	413.9	420.3	6.4	2.9	49.20	4.0	507.0
including	413.9	417.7	3.8	4.8	56.80	6.0	507.0
22TA-32	247.5	249.0	1.5	0.8	0.90	109.0	550.0
22TA-32	252.0	253.5	1.5	0.8	2.70	333.0	545.0
22TA-32	258.0	270.0	12.0	6.0	0.60	63.0	535.0
22TA-32	273.0	276.9	3.9	2.0	0.30	38.0	525.0
22TA-32	279.9	291.0	11.2	5.6	3.90	88.0	516.0
including	280.8	285.0	4.3	2.1	9.20	223.0	517.0
22TA-33	183.00	184.5	1.5	1.1	0.30	46.0	607.0
22TA-33	192.0	193.5	1.5	1.1	0.30	36.0	599.0
22TA-33	199.5	205.3	5.8	4.3	0.70	61.0	589.0
including	202.5	203.9	1.4	1.0	1.40	119.0	589.0
23TA-85	110.1	111.0	0.9	0.8	0.60	4.0	482.0
23TA-85	143.0	145.4	2.4	2.2	0.20	1.0	454.0
23TA-85	328.0	330.0	2.0	1.8	0.20	2.0	301.0
23TA-85	356.3	357.5	1.2	1.1	0.20	4.0	278.0
23TA-85	364.5	368.8	4.4	4.0	0.30	5.0	270.0
23TA-85	371.0	374.7	3.7	3.4	0.20	4.0	265.0
23TA-85	377.3	378.5	1.2	1.0	1.00	3.0	261.0
23TA-85	384.1	391.3	7.2	6.6	3.50	4.0	252.0
including	385.5	388.8	3.3	3.0	3.60	2.0	254.0
including	385.5	387.0	1.5	1.4	6.20	3.0	254.0
& including	390.3	391.3	1.1	1.0	12.10	19.0	249.0
23TA-85	396.0	397.2	1.2	1.1	0.30	1.0	245.0
23TA-85	408.5	411.0	2.6	2.3	0.50	3.0	234.0
23TA-85	423.9	425.0	1.1	1.0	0.20	4.0	222.0
24TA-131	22.6	24.9	2.3	2.3	0.60	25.0	568.0
24TA-131	277.3	283.0	5.7	5.4	0.30	7.0	448.0
24TA-131	287.9	288.8	0.9	0.8	0.30	6.0	444.0
24TA-131	291.9	293.6	1.8	1.7	0.40	7.0	442.0
24TA-131	296.8	303.9	7.1	6.9	0.60	10.0	437.0
24TA-131	305.9	316.9	11.0	10.7	1.20	20.0	431.0
including	308.8	310.4	1.6	1.6	1.70	24.0	431.0
& including	314.6	315.4	0.9	0.8	6.80	37.0	430.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
22TA-53	236.2	237.0	0.9	0.8	3.10	30.0	495.0
22TA-53	241.5	247.0	5.6	5.4	0.40	33.0	491.0
22TA-53	248.7	251.5	2.8	2.7	0.40	43.0	487.0
22TA-53	253.4	262.8	9.4	9.1	1.10	137.0	483.0
including	253.4	254.1	0.7	0.7	4.40	713.0	485.0
& including	255.0	256.9	1.9	1.8	2.10	204.0	485.0
22TA-53	265.7	270.2	4.5	4.3	0.70	18.0	478.0
22TA-48	184.0	185.5	1.5	1.5	0.30	8.0	515.0
22TA-48	201.8	203.0	1.2	1.2	1.20	153.0	503.0
22TA-48	219.3	220.7	1.4	1.4	0.30	26.0	491.0
22TA-48	223.3	230.6	7.3	7.3	1.10	151.0	487.0
including	228.1	230.6	2.5	2.5	2.20	281.0	484.0
22TA-48	254.5	256.0	1.5	1.5	0.20	3.0	468.0
22TA-45	227.0	229.1	2.1	1.9	0.40	28.0	545.0
22TA-45	237.7	244.5	6.8	6.4	1.30	86.0	540.0
including	238.7	240.0	1.3	1.2	4.20	237.0	540.0
21TA-08	16.5	21.4	4.9	3.8	14.50	82.0	681.0
including	18.0	19.2	1.2	0.9	47.10	111.0	681.0
21TA-08	28.3	29.3	1.0	0.8	1.20	22.0	674.0
21TA-08	37.5	40.4	2.9	2.2	4.00	9.0	667.0
21TA-08	145.2	146.0	0.8	0.8	0.60	11.0	591.0
24TA-103	227.7	228.6	1.0	1.0	0.80	2.0	364.0
24TA-103	240.0	241.5	1.5	1.5	0.30	1.0	351.0
24TA-103	282.1	283.5	1.5	1.4	0.30	2.0	310.0
24TA-103	351.9	354.9	3.0	2.9	0.40	16.0	240.0
24TA-103	368.0	369.1	1.1	1.1	0.20	39.0	225.0
24TA-103	370.7	372.0	1.4	1.3	0.30	16.0	222.0
24TA-103	375.9	376.6	0.8	0.7	1.50	49.0	217.0
24TA-103	380.1	381.2	1.2	1.1	1.10	36.0	213.0
23TA-69	249.0	250.3	1.3	1.3	1.10	12.0	398.0
23TA-69	267.0	271.1	4.1	4.1	0.30	2.0	383.0
23TA-69	295.3	306.8	11.5	11.4	4.00	88.0	359.0
including	296.1	297.0	1.0	1.0	2.30	40.0	363.0
including	300.9	302.9	2.0	2.0	19.40	168.0	359.0
including	301.4	302.9	1.5	1.5	24.50	209.0	359.0
including	305.9	306.8	0.9	0.9	1.90	264.0	355.0
23TA-69	317.6	318.3	0.8	0.8	2.40	138.0	346.0
22TA-27	129.0	133.5	4.5	3.9	0.90	104.0	533.0
including	129.0	130.5	1.5	1.3	2.00	244.0	534.0
22TA-27	141.0	142.5	1.5	1.3	0.20	12.0	523.0
22TA-27	156.0	157.5	1.5	1.3	0.30	22.0	509.0
22TA-27	172.5	174.0	1.5	1.3	0.30	47.0	493.0
22TA-27	176.0	177.0	1.0	0.9	1.60	7.0	490.0
22TA-23	97.5	102.0	4.5	4.2	3.10	25.0	573.0
including	99.0	100.5	1.5	1.4	7.70	34.0	573.0
22TA-23	106.5	115.3	8.8	8.0	0.70	118.0	563.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
including	109.9	112.5	2.6	2.4	1.30	265.0	563.0
22TA-23	138.0	139.5	1.5	1.4	0.50	27.0	540.0
21TA-11	48.2	49.1	1.0	0.9	3.90	448.0	609.0
21TA-11	58.4	62.8	4.4	4.0	1.60	230.0	598.0
including	59.8	61.4	1.6	1.5	3.50	515.0	598.0
21TA-11	71.6	73.1	1.5	1.4	0.30	3.0	587.0
21TA-11	107.5	109.6	2.1	1.9	0.50	5.0	553.0
22TA-43	13.5	19.5	6.0	5.4	4.20	59.0	654.0
including	14.7	15.6	0.9	0.8	23.60	103.0	654.0
22TA-43	40.5	43.5	3.0	2.7	0.30	9.0	656.0
24TA-135	265.0	267.4	2.4	0.3	10.00	0.0	337.0
24TA-135	268.6	269.4	0.8	0.3	2.00	0.0	334.0
24TA-135	272.2	278.6	6.4	2.9	5.50	3.0	328.0
including	274.5	276.0	1.5	1.2	1.40	1.0	328.0
& including	276.4	277.5	1.1	13.0	20.30	13.0	328.0
24TA-135	288.8	290.0	1.3	0.2	0.30	0.0	315.0
24TA-135	302.2	303.6	1.4	0.3	0.30	0.0	302.0
24TA-135	306.6	310.1	3.5	4.1	12.20	4.0	297.0
including	306.6	307.5	1.0	13.4	40.40	14.0	298.0
24TA-135	313.9	316.6	2.8	0.4	1.90	0.0	290.0
24TA-135	317.7	319.0	1.4	0.2	1.20	0.0	287.0
24TA-135	320.0	321.0	1.0	0.4	0.60	0.0	285.0
24TA-135	336.6	337.7	1.1	0.2	6.20	0.0	269.0
24TA-135	377.4	379.5	2.1	1.5	135.40	3.0	230.0
including	377.4	378.4	1.0	2.7	280.00	6.0	230.0
23TA-89	85.0	87.0	2.0	2.0	0.80	12.0	550.0
23TA-89	92.1	92.8	0.7	0.7	0.40	6.0	546.0
23TA-89	96.0	97.5	1.5	1.5	0.20	2.0	544.0
23TA-89	121.6	123.0	1.4	1.4	0.40	13.0	529.0
23TA-89	149.2	154.7	5.5	5.5	0.70	84.0	513.0
including	150.2	151.0	0.9	0.9	2.90	123.0	513.0
23TA-89	159.0	160.5	1.5	1.5	0.40	30.0	508.0
23TA-89	181.4	182.5	1.1	1.1	0.20	2.0	496.0
23TA-89	208.0	209.5	1.5	1.4	0.30	0.0	481.0
23TA-91	180.1	182.6	2.5	2.5	0.90	57.0	506.0
including	181.3	182.6	1.3	1.3	1.20	114.0	506.0
23TA-91	190.6	197.8	7.2	7.1	0.80	116.0	499.0
including	192.0	192.9	0.9	0.9	2.90	409.0	499.0
& including	195.1	197.0	1.9	1.8	1.10	69.0	498.0
24TA-139	162.0	163.5	1.5	0.4	3.30	0.0	497.0
24TA-139	185.8	187.1	1.4	0.3	24.30	1.0	480.0
24TA-139	194.3	195.8	1.5	4.8	887.00	16.0	474.0
24TA-139	206.7	217.2	10.5	2.6	522.10	9.0	463.0
including	207.4	208.3	0.9	3.6	740.00	13.0	463.0
including	208.1	216.0	8.0	2.9	572.00	10.0	459.0
24TA-139	234.5	235.5	1.0	0.4	1.30	0.0	447.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
23TA-100	253.4	259.9	7.0	5.7	1.00	212.0	435.0
including	256.5	258.0	1.5	1.3	3.00	616.0	435.0
23TA-100	279.0	280.0	1.0	0.9	0.30	1.0	418.0
23TA-100	308.9	309.6	0.7	0.6	0.30	3.0	397.0
23TA-100	312.5	313.4	0.9	0.8	0.40	3.0	395.0
23TA-100	336.9	337.9	1.0	0.9	0.30	4.0	378.0
24TA-111	331.2	332.1	0.9	0.6	0.30	7.0	318.0
24TA-111	340.5	349.4	8.9	5.7	0.30	6.0	306.0
24TA-111	378.0	379.3	1.3	0.8	7.70	1260.0	275.0
24TA-132	137.0	139.0	2.0	1.4	3.30	1.0	556.0
24TA-132	252.8	259.5	6.7	0.3	22.50	1.0	459.0
24TA-132	264.2	265.4	1.2	0.3	6.30	0.0	452.0

Notes:

1. Elevations are at the midpoint of the interval, in metres above sea level (masl).

Figure 10-5 Los Reyes Z-T Trend Drill Hole Locations

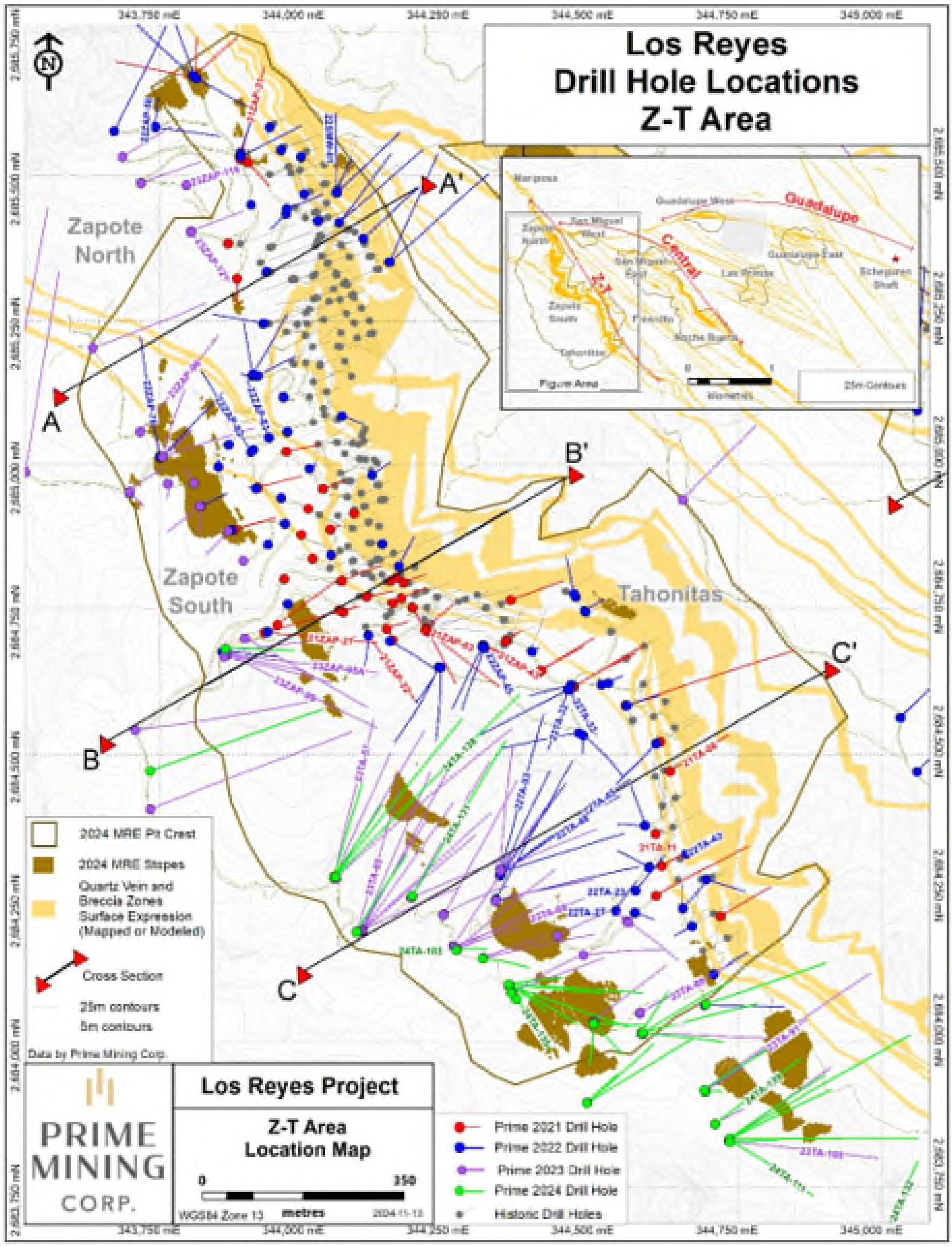


Figure 10-6 Zapote North Cross Section

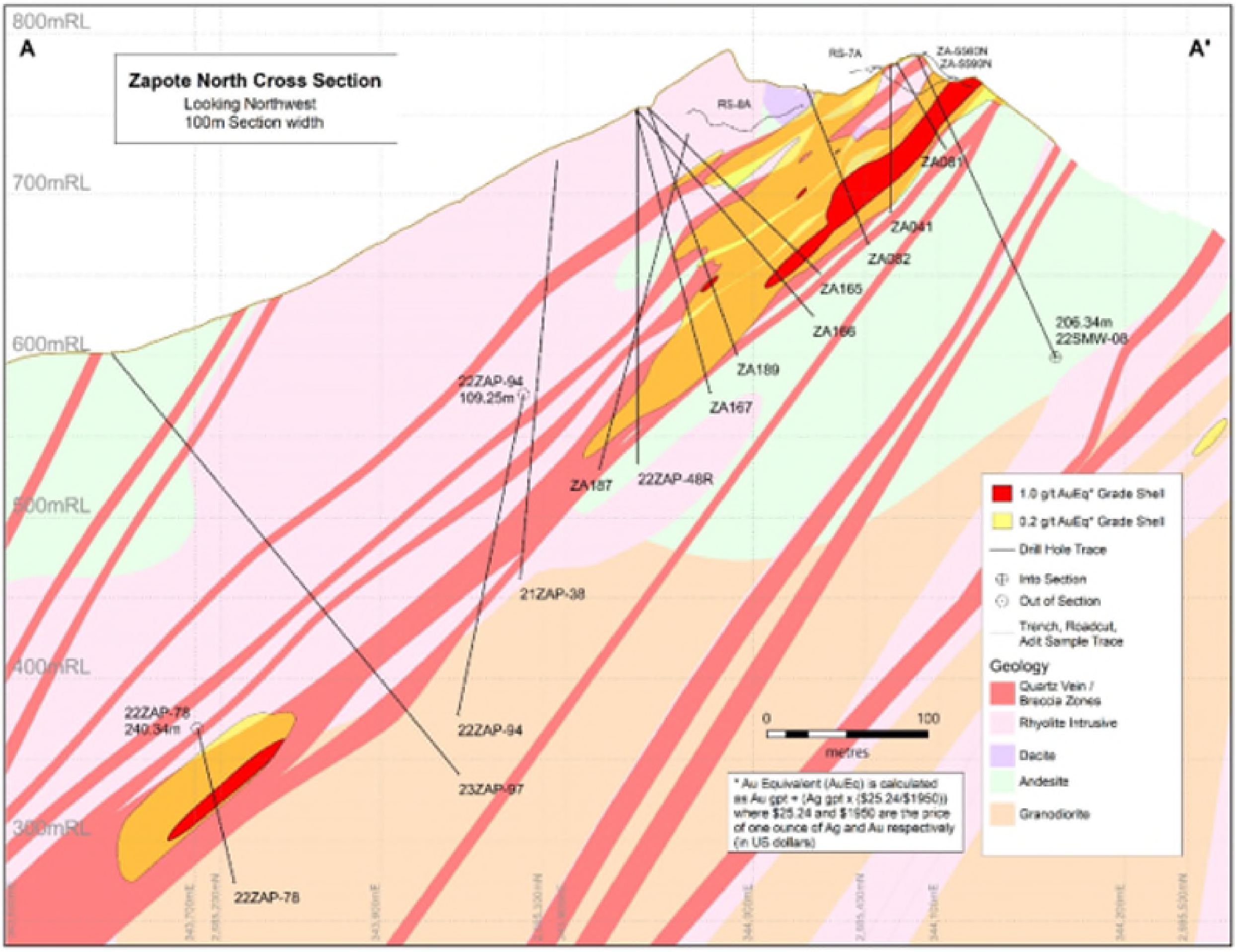


Figure 10-7 Zapote South Cross Section

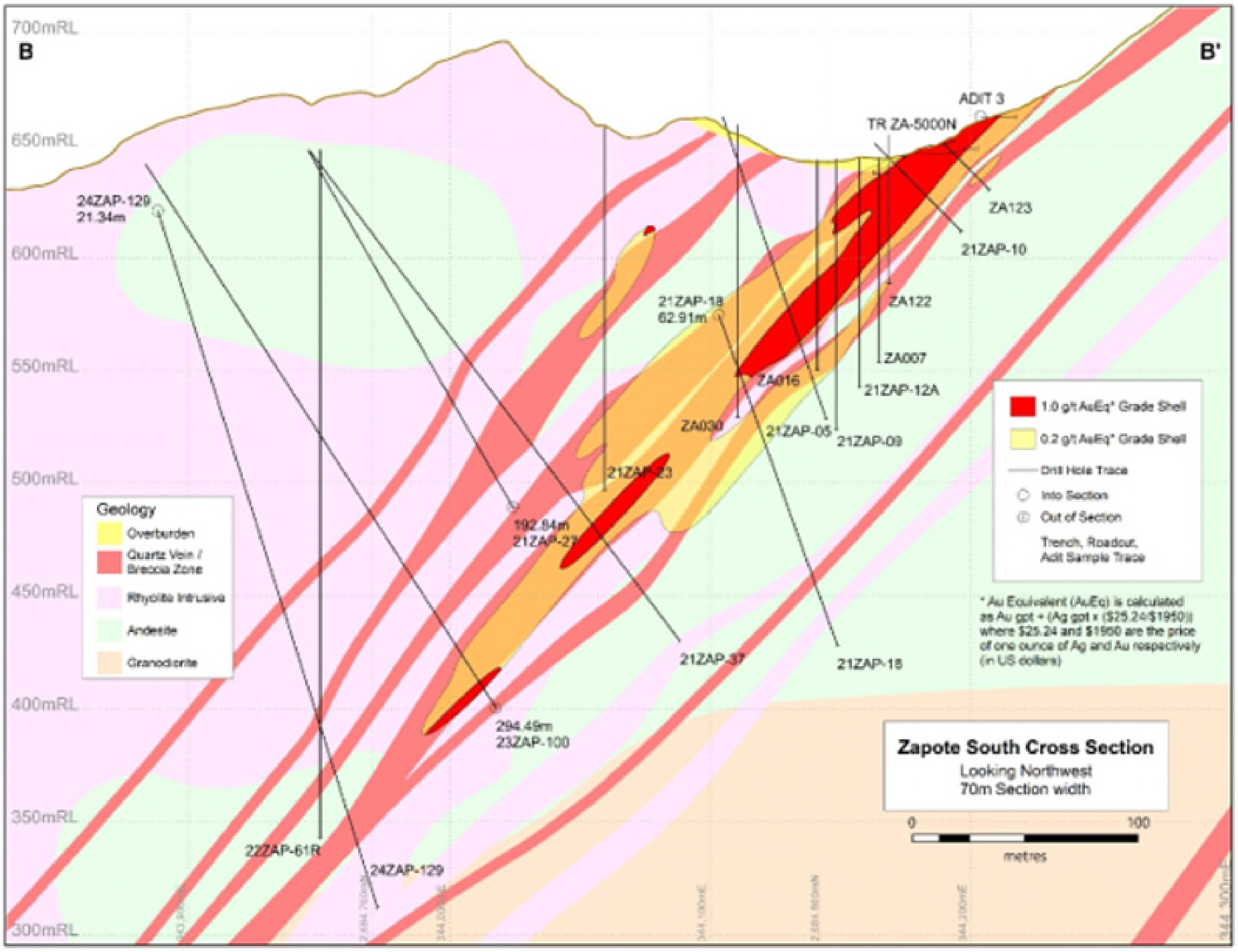
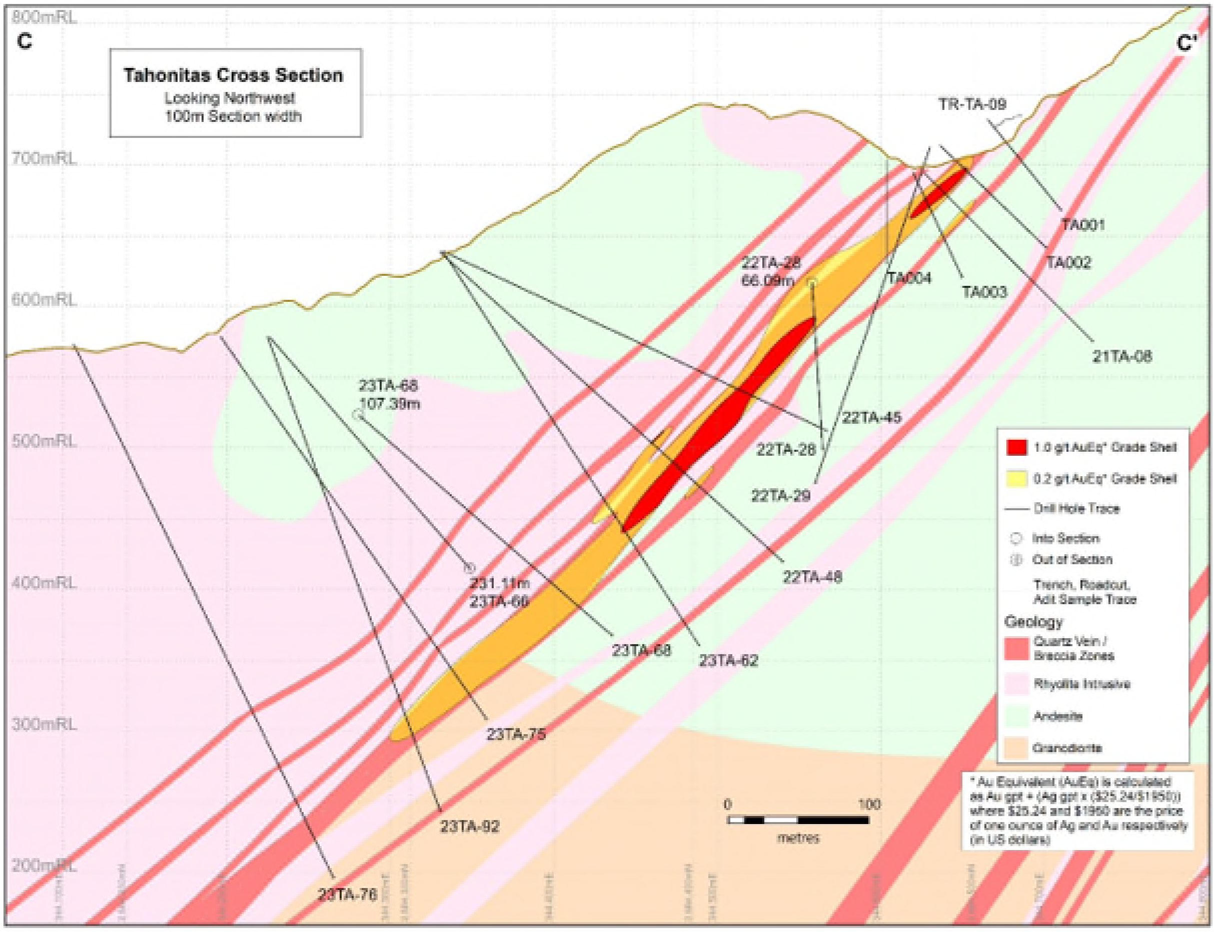


Figure 10-8 Tahonitas Cross Section



10.10.2 *Central Trend*

Previous operators had defined three deposits along the Central trend: San Miguel West, San Miguel East and Noche Buena. Gold and silver mineralization is within the main structure as anastomosing quartz veins and breccia zones and within splays emanating from the main structure. The structure tends to be moderately dipping, between 45° and 60° to the south-southwest.

The San Miguel West deposit is within a moderately south dipping structure with mineralization up to 16.0 metres wide although the veins and breccia zones anastomoses within the structure.

Within the San Miguel East deposit, there are at least two vein/breccia splays that trend eastwards from the main structure. At the point where the splays depart from the main structure, there are higher grade mineralized shoots. The northern splay (historically called the San Miguel North Limb) has been drill tested historically by all previous modern operators and is mineralized out to at least 200 metres from the main structure, up to 9 metres wide and is steeply to moderately dipping to the south. This splay appears to continue to the Las Primas exploration target area. Another splay branches out roughly 100 metres to the south and has been tested 250 metres along strike from the main structure and remains open. Mineralization within this structure is up to 6.0 metres in width. It also trends towards the Las Primas exploration area. The main Central structure is the most mineralized and has received the most drilling. This structure hosts several south plunging higher grade mineralized shoots, one of which is within the San Miguel East deposit where it is up to 17.0 metres wide.

There are several newly recognized mineralized veins discovered southwest of the main structure and running parallel to it. These veins have only been tested at shallow depths but appear to be dipping to the southwest. Drilling to date shows they are up to 6.4 metres in width, but more drilling is required to define these veins and the significance to the resource.

The Noche Buena deposit is within the main structure which hosts a series of anastomosing quartz veins and quartz brecciation zones that host mineralization. Where the veins coalesce, the mineralized zone can be up to 35.0 metres wide but more frequently there are two, three or more discrete mineralized zones, each up to 12.0 metres in width, although where there are more sets of veins they tend to be narrower.

The Central trend remains open to the south-southeast. There is currently no road access to test continuity of mineralization to the south-southeast. On the other end of the Central trend, the structure intersects with the Z-T structure. Drilling west of the San Miguel West deposit shows that the structure is relatively weakly mineralized and probably uneconomic.

The Guadalupe trend main structure intersects with the Central trend main structure at the San Miguel West deposit. This end of the structure has been drill tested along 430 metres of strike length, including four drill holes by Prime, and mineralization is relatively minimal.

Limited testing between the San Miguel West and East deposits indicates the structure is insufficiently mineralized to potentially connect the deposits.

Prime has drilled 110 core holes into the Central trend totaling 27,553.0 metres.

An example of Prime's drill results from the Central trend are shown in Tables 10-5 to 10-7 sorted by historical deposit area and from north to south and listed by collar location from west to east (SMW) or north to south (SME and NB). Figure 10-9 shows all the Central drill hole locations with the example holes labelled. Representative cross sections are in Figures 10-10 to 10-12 and their locations are shown in Figure 10-9.

Table 10-5 Central Drill Results Summary (San Miguel West)

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation[1] (masl)
22SMW-04	215.3	216.8	1.5	1.4	0.30	1.0	617.0
22SMW-04	273.0	274.5	1.5	1.4	0.60	22.0	574.0
22SMW-04	277.5	279.0	1.5	1.4	1.50	14.0	571.0
22SMW-04	295.5	300.0	4.5	4.3	0.80	5.0	557.0
including	297.0	298.5	1.5	1.4	1.80	2.0	557.0
22SMW-04	304.5	306.0	1.5	1.4	0.20	1.0	551.0
22SMW-06	57.5	60.5	3.0	2.1	0.50	25.0	651.0
22SMW-06	62.0	63.0	1.1	0.7	0.20	28.0	648.0
22SMW-09	20.0	22.0	2.0	1.3	0.50	0.0	705.0
22SMW-09	51.0	53.0	2.0	1.3	0.80	7.0	674.0
22SMW-10	30.0	38.8	8.8	5.7	0.30	3.0	668.0
22SMW-10	43.2	52.6	9.4	6.0	2.00	177.0	653.0
including	49.2	51.7	2.5	1.6	6.40	551.0	652.0

Notes:

1. Elevations are at the midpoint of the interval, in metres above sea level (masl).

Table 10-6 Central Drill Results Summary (San Miguel East)

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m)[1]
22SME-18	244.5	252.0	7.5	7.2	0.40	1.0	541.0
21SME-02	0.0	6.8	6.8	5.6	0.80	7.0	763.0
including	0.0	4.5	4.5	3.7	1.10	8.0	764.0
21SME-02	12.0	14.1	2.1	1.8	0.50	1.0	757.0
21SME-02	246.8	247.7	0.9	0.9	0.50	21.0	585.0
21SME-02	250.6	253.2	2.6	2.6	0.50	86.0	582.0
21SME-02	264.4	269.5	5.1	5.0	0.20	3.0	571.0
21SME-02	271.5	272.5	1.1	1.0	0.30	33.0	567.0
21SME-02	274.0	275.5	1.5	1.5	0.20	3.0	565.0
21SME-02	394.1	395.6	1.5	1.3	0.40	11.0	475.0
21SME-02	396.9	398.5	1.7	1.4	0.70	67.0	473.0
22SME-12	36.3	44.1	7.8	6.4	0.70	4.0	733.0
22SME-12	112.5	114.0	1.5	1.3	0.30	1.0	681.0
22SME-12	273.0	277.5	4.5	4.5	0.50	11.0	570.0
22SME-12	289.0	290.0	1.0	1.0	0.30	30.0	561.0
22SME-12	316.5	318.0	1.5	1.5	0.60	4.0	543.0
22SME-11	12.0	15.0	3.0	2.6	1.20	14.0	754.0
22SME-11	48.0	49.5	1.5	1.4	0.30	2.0	724.0
22SME-11	162.0	165.0	3.0	2.8	0.50	1.0	626.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
22SME-11	204.0	205.5	1.5	1.4	0.50	1.0	591.0
22SME-11	223.5	241.5	18.0	16.9	2.70	130.0	568.0
including	223.5	226.5	3.0	2.8	1.80	205.0	574.0
including	231.0	237.0	6.0	5.6	6.50	204.0	567.0
22SME-11	259.5	261.0	1.5	1.4	0.70	1.0	545.0
22SME-11	267.0	268.5	1.5	1.4	0.20	1.0	539.0
22SME-11	303.0	306.0	3.0	2.3	1.10	4.0	508.0
22SME-13	123.0	124.9	1.9	1.8	1.50	5.0	653.0
22SME-13	130.5	136.9	6.4	6.1	4.90	151.0	645.0
including	130.5	131.5	1.0	1.0	15.90	84.0	647.0
& including	135.0	136.9	1.9	1.8	6.30	411.0	643.0
22SME-13	187.5	189.0	1.5	1.2	4.00	2.0	601.0
22SME-13	215.0	216.3	1.3	1.0	0.40	51.0	579.0
22SME-15	0.0	9.0	9.0	7.8	0.40	2.0	737.0
22SME-15	10.5	12.0	1.5	1.3	0.20	4.0	732.0
22SME-15	21.0	22.5	1.5	1.3	0.30	5.0	724.0
22SME-15	107.0	108.0	1.1	1.0	0.30	4.0	657.0
22SME-15	126.0	128.7	2.7	2.5	0.20	55.0	641.0
22SME-15	131.0	132.0	1.0	0.9	0.80	8.0	638.0
22SME-15	201.0	203.0	2.0	1.7	0.30	8.0	586.0
22SME-26	11.9	13.4	1.5	1.3	0.50	10.0	752.0
22SME-26	240.0	241.50	1.5	1.2	0.30	39.0	536.0
22SME-26	268.0	269.9	1.9	1.5	0.40	90.0	510.0
22NB-26	28.8	34.0	5.2	5.1	0.40	1.0	780.0
22NB-26	114.0	116.0	2.0	2.0	0.20	2.0	719.0
22NB-26	181.4	192.0	10.7	10.3	0.90	100.0	668.0
including	186.0	187.5	1.5	1.4	2.40	287.0	668.0
22NB-29	15.0	17.0	2.0	1.8	0.30	1.0	786.0
22NB-29	41.0	43.0	2.0	1.8	0.30	1.0	763.0
22NB-29	180.0	181.5	1.5	1.4	0.60	3.0	636.0
22NB-29	193.7	195.0	1.3	1.2	0.20	32.0	623.0
22NB-29	196.3	197.8	1.5	1.4	0.40	28.0	621.0
22NB-29	200.0	201.1	1.1	1.0	0.30	48.0	617.0
22NB-29	202.2	204.7	2.5	2.3	1.20	96.0	615.0
including	204.0	204.7	0.7	0.7	3.00	236.0	614.0
22NB-29	214.0	215.0	1.0	0.9	0.20	11.0	604.0
22NB-29	271.5	273.0	1.5	1.4	0.70	4.0	551.0
23NB-59	300.0	301.0	1.0	0.9	0.20	17.0	550.0
23NB-59	303.2	310.6	7.5	6.5	0.90	117.0	544.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
including	303.2	305.9	2.8	2.4	2.00	190.0	546.0

Notes:

1. Elevations are at the mid point of the interval, in metres above sea level (masl).

Table 10-7 Central Drill Results (Noche Buena)

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
24NB-63	33.0	33.7	0.7	0.6	0.26	3.3	824.0
24NB-63	123.7	127.5	3.8	3.7	0.52	3.6	771.0
24NB-63	217.5	219.0	1.5	1.5	0.21	1.4	717.0
24NB-63	280.0	281.1	1.1	1.0	0.37	1.2	682.0
24NB-63	289.5	291.0	1.5	1.4	0.25	6.2	676.0
24NB-63	313.8	317.3	3.5	3.5	1.06	19.8	662.0
including	313.8	315.2	1.4	1.4	2.04	39.2	662.0
24NB-63	328.3	330.7	2.4	2.4	0.90	28.5	654.0
24NB-63	338.2	339.2	1.0	1.0	0.89	3.5	648.0
24NB-63	347.1	349.0	2.0	2.0	0.37	6.9	643.0
24NB-63	352.0	358.1	6.1	6.1	0.62	33.0	639.0
22NB-37	56.1	57.0	0.9	0.7	0.20	1.0	688.0
22NB-37	58.5	61.5	3.0	2.3	0.40	2.0	685.0
22NB-37	75.0	76.5	1.5	1.1	0.20	1.0	669.0
22NB-37	107.5	108.9	1.5	1.0	0.30	2.0	637.0
22NB-37	112.5	115.5	3.0	2.1	0.40	2.0	631.0
22NB-37	121.0	122.0	1.0	0.7	0.20	1.0	623.0
22NB-37	125.8	137.1	11.3	8.0	0.50	9.0	613.0
22NB-37	146.6	147.5	1.0	0.7	0.40	39.0	598.0
21NB-08	9.0	10.5	1.5	1.2	0.20	7.0	722.0
21NB-08	16.5	18.0	1.5	1.2	0.30	4.0	715.0
21NB-08	19.5	21.0	1.5	1.2	0.30	2.0	712.0
21NB-08	25.3	29.2	3.9	3.1	0.30	4.0	706.0
21NB-08	32.4	43.5	11.1	8.9	1.20	28.0	696.0
including	33.4	34.5	1.1	0.9	6.10	91.0	699.0
21NB-14	4.5	6.0	1.5	1.3	0.40	9.0	727.0
21NB-14	134.1	138.0	3.9	3.4	0.20	1.0	599.0
21NB-14	148.5	150.0	1.5	1.1	0.20	2.0	586.0
21NB-14	153.0	157.3	4.3	3.3	0.30	6.0	580.0
21NB-14	161.0	162.8	1.8	1.3	0.30	5.0	573.0
21NB-14	172.5	184.3	11.8	9.0	0.40	9.0	557.0
21NB-23	78.7	79.8	1.1	1.1	0.30	18.0	691.0
21NB-23	82.4	102.0	19.7	19.7	1.90	76.0	681.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
including	82.4	86.2	3.8	3.8	4.80	110.0	687.0
& including	93.0	96.0	3.0	3.0	4.80	250.0	680.0
21NB-23	105.0	115.5	10.5	10.5	0.30	9.0	669.0
21NB-23	183.0	184.1	1.1	1.1	0.20	1.0	617.0
21NB-23	280.4	281.2	0.8	0.8	0.40	72.0	550.0
21NB-01	87.0	93.4	6.4	4.1	0.60	31.0	686.0
including	87.0	89.0	2.0	1.3	1.30	61.0	687.0
21NB-22	134.7	137.1	2.5	2.3	0.20	10.0	627.0
21NB-22	138.2	138.6	0.4	0.4	1.20	28.0	625.0
21NB-22	142.3	144.0	1.8	1.6	0.50	39.0	625.0
21NB-22	161.2	161.8	0.6	0.5	0.20	22.0	605.0
21NB-22	162.7	164.2	1.5	1.4	0.20	8.0	604.0
21NB-22	168.0	194.9	26.9	24.3	0.90	44.0	588.0
including	177.0	180.0	3.0	2.7	3.20	75.0	590.0
& including	180.9	181.9	1.0	0.9	3.50	82.0	588.0
21NB-24	46.0	46.8	0.8	0.8	0.30	0.0	734.0
21NB-24	79.5	81.0	1.5	1.5	0.40	0.0	710.0
21NB-24	84.0	90.7	6.7	6.7	0.50	24.0	705.0
21NB-24	105.0	106.1	1.1	1.1	0.30	1.0	692.0
21NB-24	126.0	130.5	4.5	4.5	0.40	2.0	676.0
21NB-24	142.5	143.1	0.6	0.6	0.20	1.0	666.0
21NB-24	173.3	174.8	1.5	1.5	0.20	9.0	644.0
21NB-24	199.0	200.0	1.0	1.0	0.30	1.0	627.0
21NB-19	135.0	135.6	0.7	0.5	1.80	55.0	631.0
21NB-19	144.0	145.0	1.0	0.7	0.30	2.0	624.0
21NB-19	146.0	148.5	2.5	1.8	0.20	2.0	622.0
21NB-19	155.5	157.3	1.8	1.3	0.30	10.0	614.0
21NB-19	199.1	201.0	1.9	1.3	1.40	110.0	578.0
21NB-19	205.0	205.6	0.6	0.4	1.00	20.0	574.0
21NB-19	209.0	210.0	1.0	0.7	0.20	7.0	571.0
21NB-19	212.8	225.0	12.3	8.7	0.30	17.0	563.0
21NB-19	227.2	230.3	3.1	2.2	0.30	27.0	555.0
21NB-19	233.6	237.2	3.7	2.6	0.40	26.0	550.0
21NB-19	272.2	273.1	0.9	0.6	0.30	14.0	520.0
21NB-21	139.4	140.4	1.1	0.9	0.20	5.0	643.0
21NB-21	143.0	145.0	2.0	1.7	0.30	2.0	641.0
21NB-21	160.0	165.0	5.0	4.3	1.10	66.0	627.0
including	161.1	162.4	1.4	1.2	2.30	195.0	627.0
21NB-21	175.0	177.5	2.5	2.2	0.20	7.0	617.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m)[1]
21NB-21	178.7	193.5	14.8	12.8	2.90	24.0	610.0
including	178.7	179.8	1.1	0.9	33.00	51.0	615.0
& including	186.0	189.0	3.0	2.6	1.70	66.0	609.0
21NB-21	201.3	215.2	14.0	12.1	0.50	36.0	593.0
22NB-36	116.4	124.5	8.1	6.2	2.40	63.0	694.0
including	116.4	118.7	2.3	1.8	7.70	210.0	696.0
including	117.6	118.7	1.1	0.8	13.30	155.0	696.0
22NB-36	136.5	138.0	1.5	1.1	0.40	20.0	677.0
23NB-55	252.9	253.6	0.7	0.7	0.44	35.3	599.0
23NB-55	257.4	261.3	3.9	3.7	0.93	33.6	595.0
including	257.4	258.3	0.9	0.9	2.99	102.3	596.0

Notes:

1. Elevations are at the midpoint of the interval, in metres above sea level (masl).

Figure 10-9 Los Reyes Central Trend Drill Hole Locations

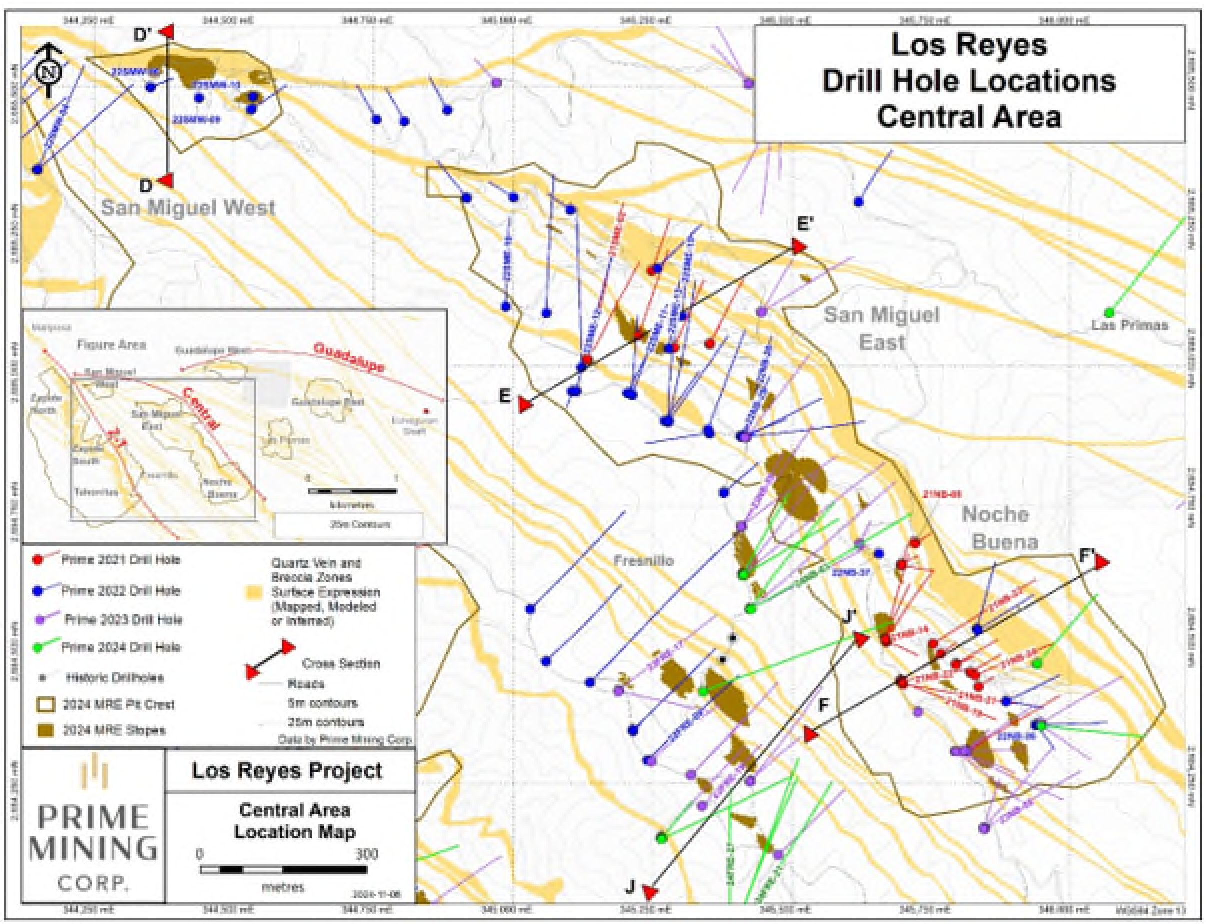


Figure 10-10 San Miguel West Cross Section

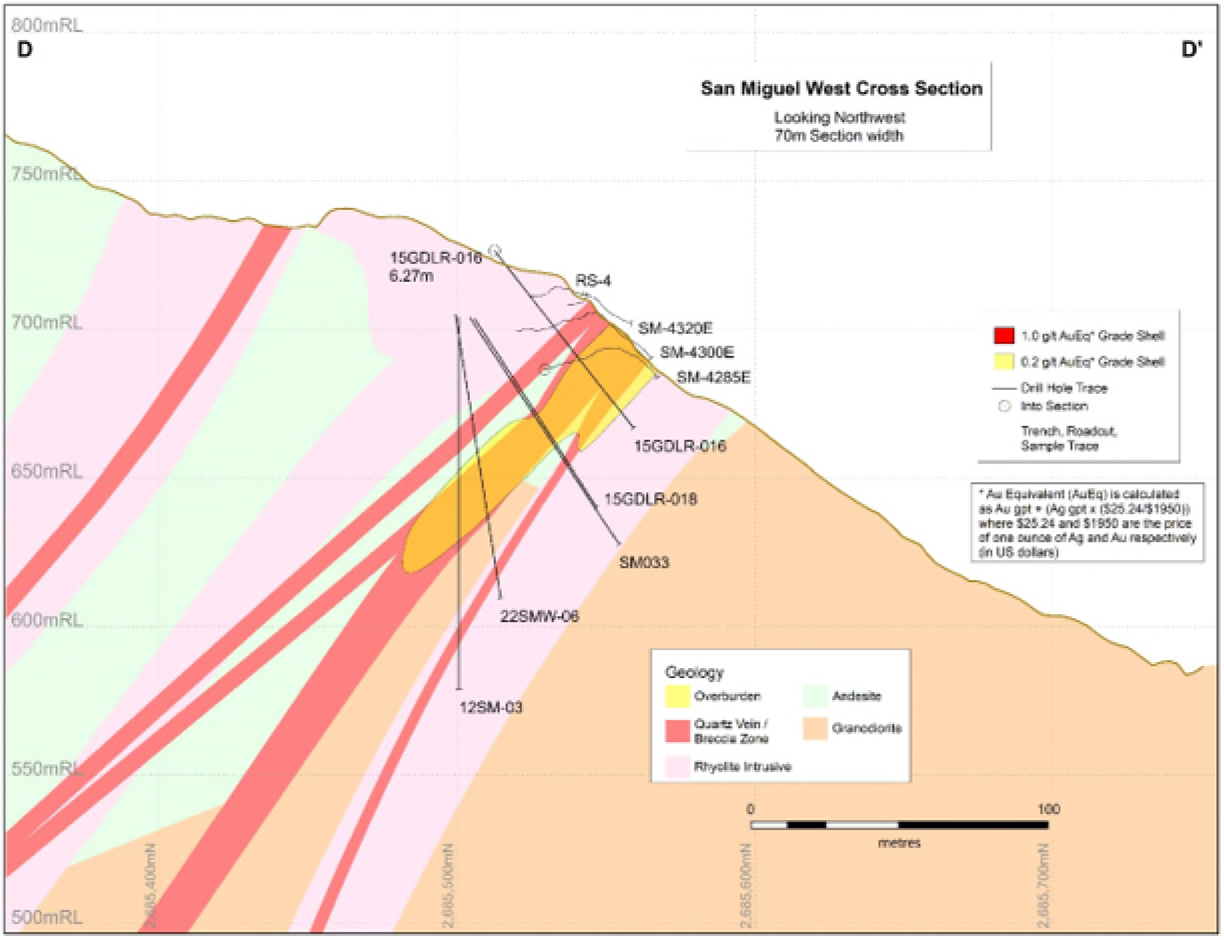


Figure 10-11 San Miguel East Cross Section

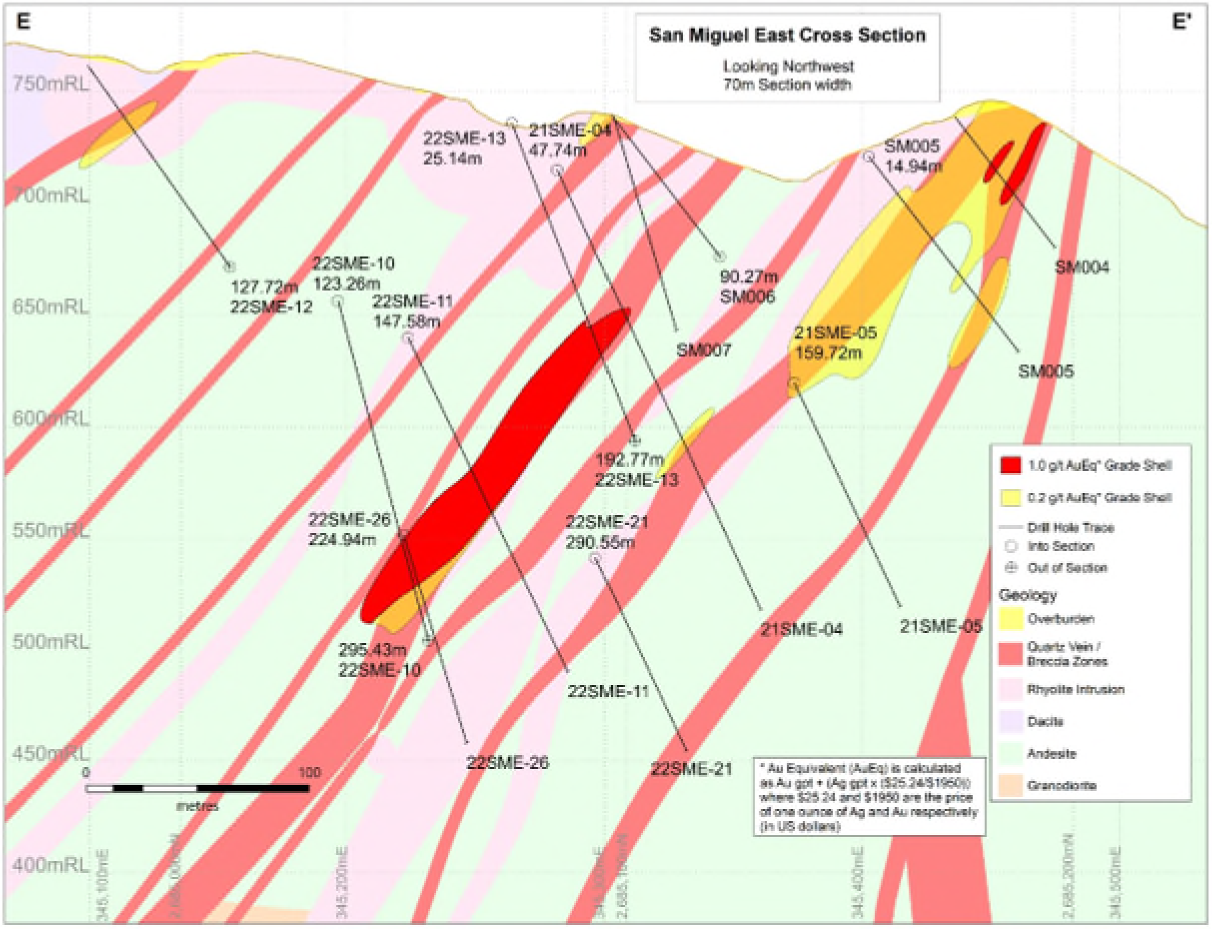
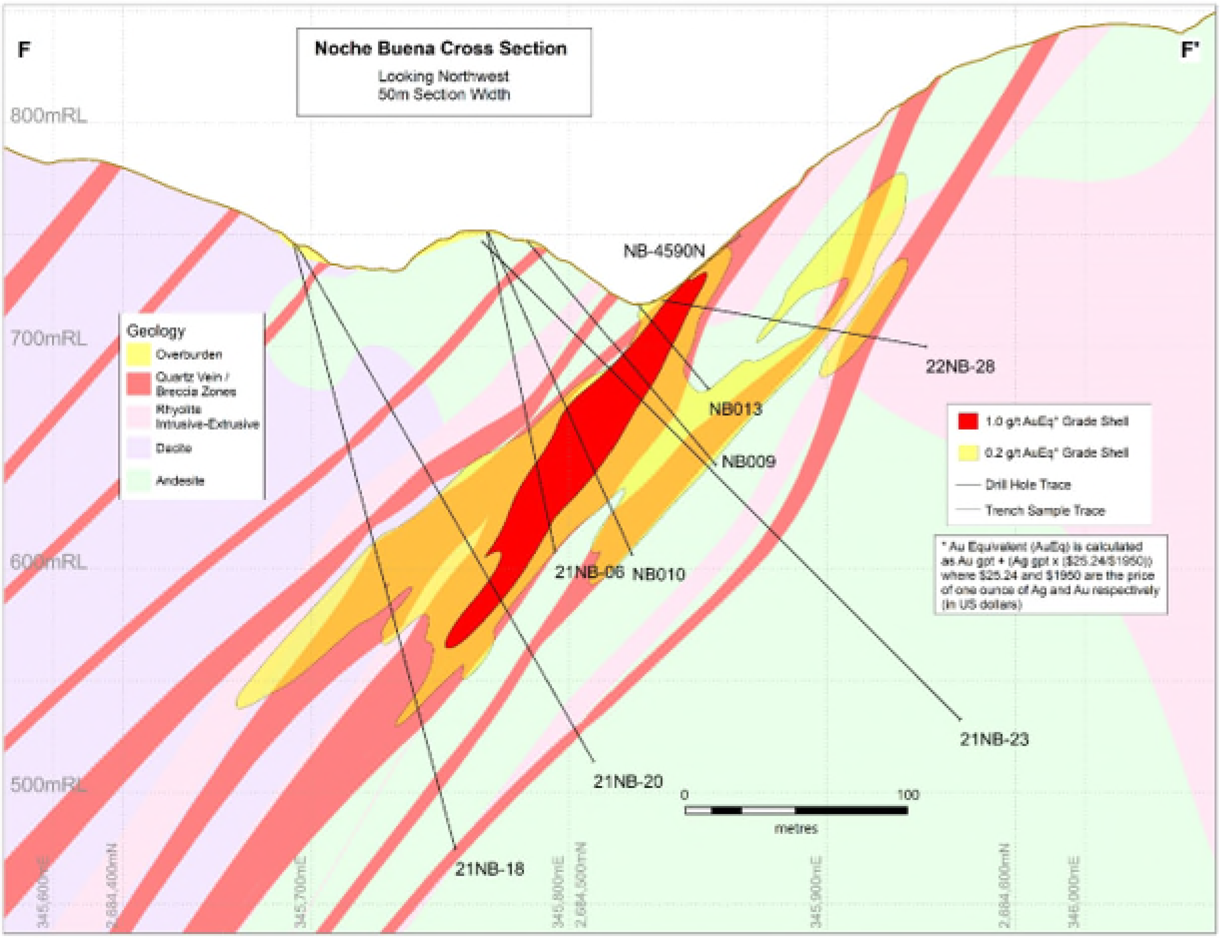


Figure 10-12 Noche Buena Cross Section



10.10.3 *Guadalupe Trend*

Two mineral deposits have been discovered along the Guadalupe trend to date. The largest, Guadalupe East had been historically drilled predominately within the western part of the deposit, historically called Laija. Prime has stepped out to the east and to a lesser degree to the west, as well as down dip, resulting in a significant expansion to the deposit.

The Estaca vein is the main mineralized quartz vein within the Guadalupe East deposit. The Estaca is a steeply south dipping (~70-90°) cohesive quartz vein with at least one major flexure and a general east plunging, higher grade mineralized shoot that averages 100 metres vertical height. In the western part of the deposit, Laija, there are multiple antithetic veins emanating from the Estaca vein into the hanging wall. This part of the deposit appears to be bounded by NW trending faults. In the eastern part of the deposit the antithetic veins are in the footwall of the Estaca vein, dipping to the north-northeast. Where the antithetic veins depart from the Estaca vein they are typically relatively thick, higher grade mineralized zones (called 'clavos'). In the eastern part of the deposit, it is believed that the San Manual and/or San Nicolas veins are antithetic veins emanating from the Estaca but significant erosion has removed where they converge. The eastern part of the deposit also has mineralized northeast trending structures that crosscut the main east-west structure.

The Guadalupe East deposit remains open along strike. On the western side of the deposit, drilling is limited due to topography and access. On the eastern side, drilling shows the structure that hosts the Estaca vein is mineralized but the mineralization is more sporadic. Future drilling will continue to explore this structure as well as other structures in the footwall where there has been historical mining.

The Guadalupe West deposit is a relatively small deposit characterized by a thick, higher grade mineralized core up to 30.0 metres ETW and narrow, parallel veins in both the footwall and hanging wall. It remains open to the east and west but historical drilling on the 6 de Enero claim (not owned by Prime) indicates mineralization is narrow and may have been mined out.

Prime has drilled 161 core holes (55,553.0 metres) and 21 RC holes (4,680.6 metres) into the Guadalupe trend totalling 60,233.6 metres.

An example of Prime's drill results from the Guadalupe trend are shown in Tables 10-8 and 10-9 sorted by historical deposit area and listed by collar location from west to east. The locations of these drill holes are shown labelled on Figure 10-13. Representative cross sections are in Figures 10-14 and 10-15 and their locations are shown in Figure 10-13.

Table 10-8 Guadalupe West Summary of Drill Results

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation[1] (masl)
21GW-03	63.0	64.5	1.5	1.1	0.53	107.6	645.0
21GW-03	101.5	135.1	33.6	23.7	0.38	23.6	593.0
21GW-01	0.0	18.0	18.0	16.3	0.84	33.4	682.0
21GW-01	25.5	28.4	2.9	2.5	0.34	31.4	671.0
21GW-01	29.2	30.0	0.8	0.7	0.29	22.7	669.0
21GW-01	32.4	36.6	4.2	3.6	1.08	37.6	665.0
21GW-05	131.0	133.5	2.5	2.0	0.24	14.0	621.0
21GW-05	163.6	164.6	1.0	0.8	0.57	59.3	593.0
21GW-05	202.4	210.0	7.7	6.3	0.48	1.3	554.0
21GW-05	215.8	221.3	5.6	4.5	0.34	17.6	545.0
21GW-07	1.5	3.0	1.5	1.2	0.49	14.9	707.0
21GW-07	7.5	18.0	10.5	8.6	1.60	50.4	698.0
including	14.0	15.1	1.1	0.9	11.70	111.0	697.0
21GW-07	24.3	45.9	21.6	17.7	1.92	34.3	680.0
including	24.3	25.5	1.2	1.0	4.44	29.5	688.0
& including	34.0	35.5	1.5	1.2	6.85	59.7	680.0
& including	40.9	42.0	1.2	0.9	3.47	43.9	675.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation[1] (masl)
21GW-12R	54.9	58.0	3.1	2.3	0.96	4.0	700.0
21GW-12R	109.8	111.3	1.5	1.3	0.34	2.6	657.0
21GW-12R	112.9	114.4	1.5	1.3	0.61	19.0	654.0
21GW-12R	115.9	117.4	1.5	1.3	2.74	31.4	652.0
21GW-12R	120.5	122.0	1.5	1.3	0.21	5.6	648.0
21GW-12R	132.7	155.6	22.9	19.8	1.68	25.8	629.0
including	134.2	135.7	1.5	1.3	11.3	107.3	638.0
& including	149.5	151.0	1.5	1.3	7.48	13.5	626.0
21GW-08R	111.0	112.5	1.5	1.2	0.24	4.3	691.0
21GW-08R	154.5	162.0	7.5	6.1	0.51	4.5	650.0
21GW-09R	65.6	67.1	1.5	1.3	0.27	27.8	727.0
21GW-09R	71.7	74.7	3.1	2.5	0.25	17.0	722.0
21GW-09R	79.3	80.8	1.5	1.3	0.93	13.1	716.0
21GW-09R	132.7	134.2	1.5	1.3	0.31	31.6	675.0

Notes:

1. Elevations are at the midpoint of the interval, in metres above sea level (masl).

Table 10-9 Guadalupe East Summary of Drill Results

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
22GE-69R	54.9	58.0	3.1	2.6	0.90	26.0	718.0
22GE-69R	143.4	149.5	6.1	6.0	0.40	45.0	654.0
22GE-69R	257.7	265.4	7.6	6.2	1.00	132.0	565.0
24GE-149	31.1	32.4	1.3	Tbd	0.80	87.0	1.9
24GE-149	53.8	54.9	1.1	0.8	0.50	58.0	1.2
24GE-149	221.0	222.0	1.0	0.8	0.30	1.0	0.3
24GE-149	229.2	233.7	4.5	3.5	2.70	327.0	6.9
24GE-149	247.3	248.7	1.5	1.5	1.40	1.0	1.4
24GE-149	255.0	256.5	1.5	1.5	0.70	0.0	0.7
24GE-149	339.5	341.3	1.9	1.6	1.20	1.0	1.2
22GE-104	162.0	163.5	1.5	1.5	0.40	2.0	717.0
22GE-104	186.0	187.5	1.5	1.5	0.20	23.0	712.0
22GE-104	190.5	192.0	1.5	1.5	0.30	25.0	711.0
22GE-104	238.6	239.6	1.0	1.0	0.30	4.0	704.0
22GE-104	241.0	242.5	1.5	1.5	0.20	1.0	704.0
22GE-104	253.0	255.0	2.0	2.0	0.20	2.0	702.0
22GE-70	84.0	85.5	1.5	0.5	0.20	0.0	834.0
22GE-70	97.5	99.0	1.5	0.5	0.20	4.0	823.0
22GE-70	169.0	178.0	9.0	4.5	1.40	38.0	761.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
including	169.0	171.0	2.0	1.0	2.90	96.0	764.0
& including	176.1	178.0	2.0	1.0	2.60	51.0	758.0
22GE-70	189.0	190.5	1.5	0.8	0.30	0.0	748.0
22GE-70	211.5	213.0	1.5	0.8	0.50	100.0	730.0
22GE-70	244.5	246.0	1.5	0.8	0.20	4.0	705.0
22GE-101	5.5	7.0	1.5	1.5	0.30	71.0	819.0
22GE-101	28.5	30.0	1.5	1.5	0.60	18.0	817.0
22GE-101	37.9	39.0	1.1	1.1	NR	NR	
22GE-101	40.0	42.0	2.1	2.0	NR	NR	
22GE-101	42.0	54.0	12.0	11.8	2.70	88.0	815.0
including	42.0	45.0	3.0	3.0	4.40	218.0	815.0
including	50.4	53.0	2.9	2.9	5.30	101.0	815.0
22GE-101	55.5	57.0	1.5	1.5	0.50	5.0	814.0
22GE-101	60.0	61.5	1.5	1.5	0.30	9.0	814.0
22GE-101	64.5	66.0	1.5	1.5	0.50	3.0	813.0
22GE-101	118.5	120.8	2.3	2.2	27.90	509.0	808.0
including	120.0	120.8	0.8	0.7	77.90	1473.0	808.0
22GE-80	305.0	308.0	3.0	1.5	1.20	50.0	745.0
22GE-80	332.0	342.0	10.0	5.7	1.60	43.0	724.0
including	333.4	336.0	2.6	1.5	4.90	142.0	726.0
22GE-80	345.5	347.0	1.5	0.9	0.50	2.0	718.0
22GE-80	421.7	427.0	5.4	4.8	0.60	61.0	665.0
22GE-80	430.0	431.5	1.5	1.4	0.30	14.0	661.0
22GE-80	436.0	437.6	1.6	1.5	0.30	35.0	657.0
22GE-80	437.6	439.6	2.0	1.8	NR	NR	
22GE-80	441.0	446.4	5.4	4.8	1.70	43.0	652.0
including	444.0	446.4	2.4	2.1	3.10	52.0	651.0
22GE-106	120.0	121.5	1.5	1.5	0.30	36.0	719.0
22GE-106	136.7	138.0	1.4	0.7	0.30	31.0	710.0
22GE-106	139.2	141.3	2.1	0.8	NR	NR	
22GE-106	141.3	168.8	27.5	1.3	1.70	59.0	700.0
including	148.2	156.0	7.9	17.0	3.20	131.0	701.0
including	158.1	159.1	1.0	4.9	NR	NR	
& including	160.5	164.5	4.0	0.6	2.50	43.0	696.0
22GE-106	172.1	176.0	3.9	3.9	1.10	28.0	689.0
including	174.8	176.0	1.2	1.2	2.90	75.0	689.0
22GE-106	185.5	192.3	6.8	6.8	1.70	51.0	681.0
including	188.5	192.3	3.8	3.8	2.50	85.0	680.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
22GE-106	209.5	215.3	5.8	5.8	4.90	176.0	669.0
including	213.5	215.3	1.8	1.8	10.50	284.0	668.0
22GE-106	263.4	265.5	2.1	2.1	2.50	113.0	642.0
22GE-33	403.0	405.0	2.1	1.7	0.40	31.0	730.0
22GE-33	416.3	418.2	1.9	1.6	0.50	44.0	721.0
22GE-33	433.5	434.3	0.8	0.7	1.30	37.0	711.0
22GE-33	435.3	436.2	1.0	0.8	0.20	8.0	710.0
22GE-33	441.0	442.5	1.5	1.2	11.60	219.0	706.0
22GE-33	442.5	447.0	4.5	3.7	NR	NR	
22GE-33	447.0	448.5	1.5	1.2	0.30	20.0	703.0
22GE-33	451.5	468.5	17.0	13.9	4.70	114.0	696.0
including	451.5	459.0	7.5	6.1	2.70	94.0	699.0
& including	464.5	466.0	1.5	1.2	30.90	605.0	694.0
22GE-33	468.5	472.2	3.7	3.0	NR	NR	
22GE-33	472.2	482.6	10.4	8.5	3.70	204.0	687.0
including	472.2	474.8	2.6	2.1	8.40	321.0	687.0
22GE-53	290.5	292.0	1.5	0.5	0.40	2.0	819.0
22GE-53	323.0	327.5	4.5	1.5	0.30	2.0	793.0
22GE-53	462.3	463.4	1.1	0.8	9.70	314.0	688.0
22GE-53	465.2	466.5	1.0	0.7	NR	NR	
22GE-53	467.5	468.5	1.0	0.7	0.60	54.0	685.0
22GE-53	474.0	475.0	1.0	0.9	3.00	220.0	680.0
22GE-53	475.0	476.7	1.7	1.5	5.60	128.0	678.0
22GE-53	476.7	480.3	3.6	3.1	62.00	978.0	676.0
including	479.3	480.3	1.0	0.9	200.00	2830.0	675.0
22GE-53	480.3	481.3	1.0	0.9	NR	NR	
22GE-53	481.3	482.0	0.7	0.6	5.90	341.0	674.0
22GE-53	482.0	484.3	2.3	2.0	NR	NR	
22GE-53	484.3	485.2	0.9	0.8	0.80	104.0	672.0
22GE-114	104.6	106.0	1.4	1.4	0.20	8.0	735.0
22GE-114	339.8	357.0	17.2	12.2	1.70	145.0	605.0
including	345.1	346.3	1.2	0.8	2.80	271.0	606.0
& including	349.9	353.5	3.6	2.5	4.60	310.0	603.0
22GE-114	357.9	360.0	2.1	1.5	NR	NR	
22GE-114	360.0	370.0	10.0	7.1	1.20	124.0	596.0
22GE-114	375.0	376.5	1.5	1.1	4.40	191.0	590.0
21GE-03	108.0	112.0	4.0	0.8	0.50	40.0	757.0
21GE-03	121.5	123.0	1.5	0.3	0.20	4.0	747.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
21GE-03	129.0	131.7	2.7	0.5	2.00	85.0	741.0
21GE-03	138.4	141.0	2.6	0.5	0.80	44.0	733.0
21GE-03	144.0	144.8	0.8	0.2	0.30	13.0	729.0
21GE-03	185.1	213.0	28.0	5.6	12.00	1122.0	686.0
including	185.1	195.5	10.5	2.1	21.60	1960.0	693.0
& including	203.2	204.0	0.8	0.2	24.70	2049.0	682.0
& including	205.0	212.0	7.1	1.4	10.00	1171.0	678.0
21GE-03	216.5	226.5	10.1	2.0	11.20	909.0	668.0
including	218.0	222.0	4.1	0.8	24.20	1977.0	669.0
21GE-03	231.0	243.0	12.0	2.4	2.00	20.0	656.0
including	234.0	235.5	1.5	0.3	5.50	140.0	657.0
22GE-72	538.5	539.6	1.1	1.1	0.50	98.0	577.0
22GE-72	544.5	546.0	1.5	1.5	2.50	365.0	572.0
22GE-72	549.0	562.8	13.8	13.5	1.70	236.0	563.0
including	550.5	553.0	2.5	2.4	2.40	355.0	567.0
& including	558.3	561.3	3.0	3.0	4.60	652.0	559.0
including	558.3	559.8	1.5	1.5	7.00	1075.0	560.0
22GE-72	565.8	571.8	6.1	6.0	1.00	125.0	551.0
including	565.8	568.8	3.0	3.0	1.60	195.0	553.0
22GE-72	596.0	597.5	1.5	1.5	0.30	74.0	528.0
21GE-01	13.4	19.6	6.2	2.8	0.50	9.0	844.0
21GE-01	20.7	21.9	1.2	0.5	0.20	2.0	840.0
21GE-01	37.4	41.2	3.8	1.7	3.70	305.0	826.0
including	37.4	39.5	2.1	1.0	6.10	507.0	826.0
21GE-01	72.1	73.2	1.1	0.5	0.40	9.0	799.0
21GE-01	179.0	183.5	4.5	2.0	0.50	31.0	711.0
21GE-01	218.9	219.4	0.5	0.2	0.30	9.0	681.0
21GE-01	377.0	400.1	23.1	13.2	2.90	342.0	546.0
including	392.5	399.0	6.6	3.8	6.50	588.0	541.0
21GE-01	401.0	402.5	1.5	0.9	0.30	34.0	536.0
22GE-76	516.7	517.8	1.2	0.9	NR	NR	
22GE-76	517.8	519.5	1.7	1.3	1.60	135.0	674.0
22GE-76	519.5	521.9	2.5	1.9	NR	NR	
22GE-76	521.9	522.9	1.0	0.7	10.40	683.0	671.0
22GE-76	528.4	529.9	1.5	1.1	0.20	39.0	666.0
22GE-76	532.9	534.4	1.5	1.1	0.90	945.0	662.0
22GE-76	540.4	541.9	1.5	1.0	0.30	55.0	657.0
22GE-45	396.0	399.3	3.3	2.5	12.80	300.0	678.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
including	396.0	398.4	2.4	1.8	17.00	392.0	678.0
22GE-45	399.3	403.5	4.2	3.2	NR	NR	
22GE-45	412.0	413.5	1.5	1.1	0.20	46.0	665.0
22GE-45	416.5	417.4	0.9	0.7	0.20	13.0	661.0
22GE-49M	425.5	428.5	3.0	3.0	0.80	93.0	648.0
22GE-49M	448.5	450.0	1.5	1.5	0.30	63.0	626.0
22GE-49M	477.4	478.9	1.5	1.5	0.30	4.0	599.0
23GE-137	138.9	140.3	1.4	1.4	1.70	81.0	770.0
23GE-137	362.4	363.7	1.3	1.3	1.40	184.0	676.0
23GE-142	191.4	193.6	2.2	2.2	10.10	264.0	752.0
including	192.4	193.6	1.2	1.2	17.80	437.0	752.0
23GE-142	198.6	199.5	1.0	1.0	18.20	2024.0	746.0
23GE-142	208.3	209.0	0.7	0.7	1.00	104.0	737.0
23GE-142	244.7	245.7	1.0	1.0	5.50	615.0	705.0
23GE-142	249.2	250.3	1.1	1.1	0.50	56.0	701.0
23GE-136	304.5	306.0	1.5	0.8	0.30	63.0	691.0
23GE-136	350.5	352.0	1.5	0.8	5.50	742.0	653.0

Notes:

1. Elevations are at the midpoint of the interval, in metres above sea level (masl). "NR" indicates no recovery (possibly due to poor drilling conditions, rock voids, or historical development).

Figure 10-13 Los Reyes Guadalupe Trend Drill Hole Locations

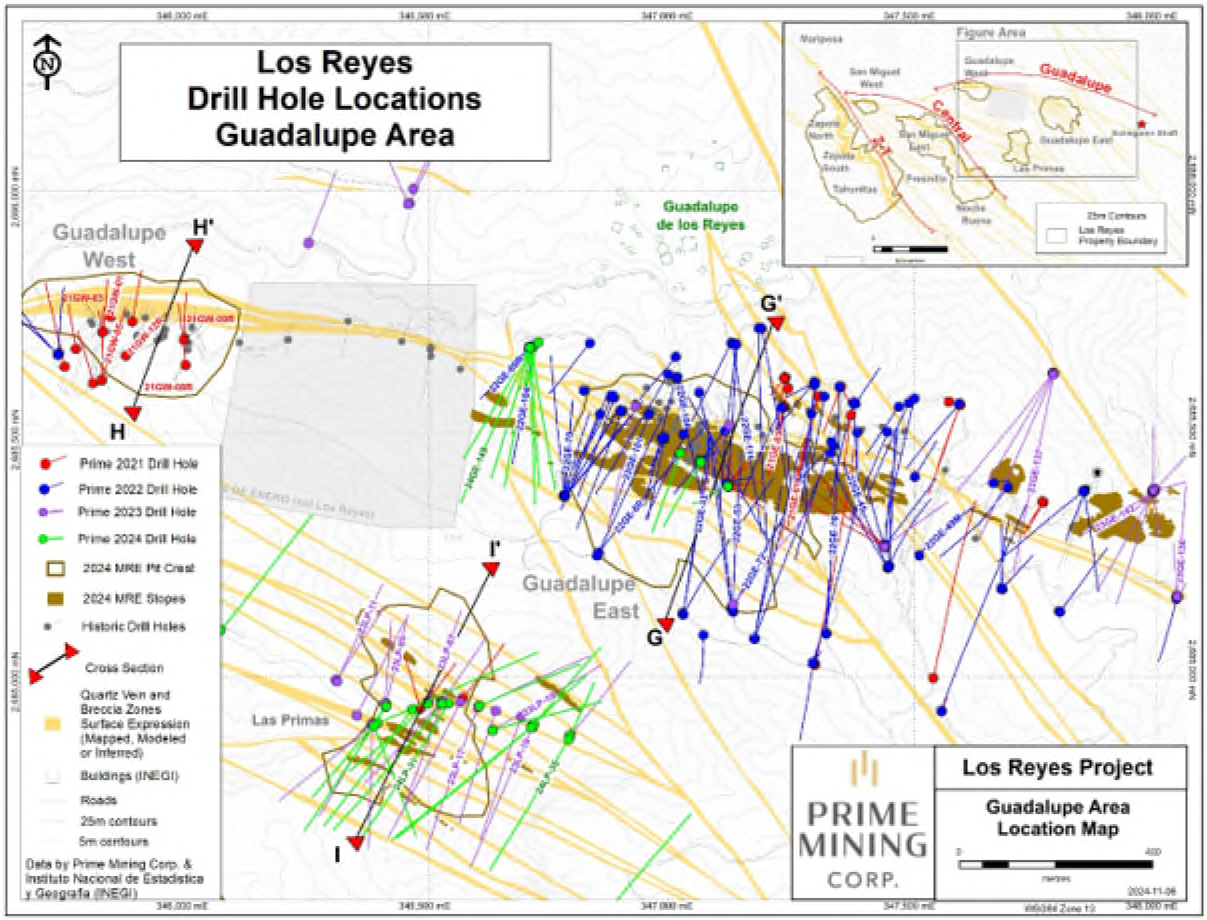


Figure 10-14 Guadalupe East Cross Section

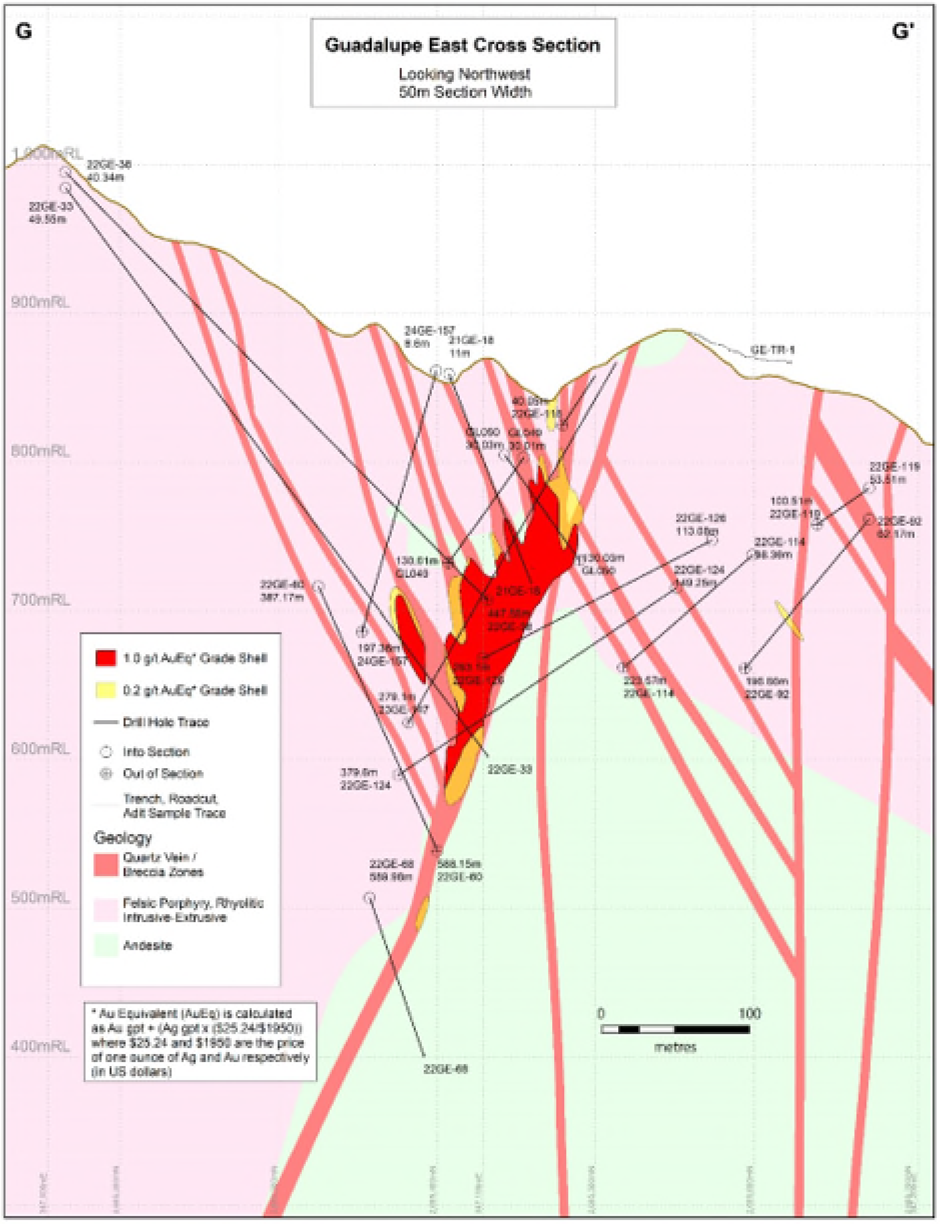
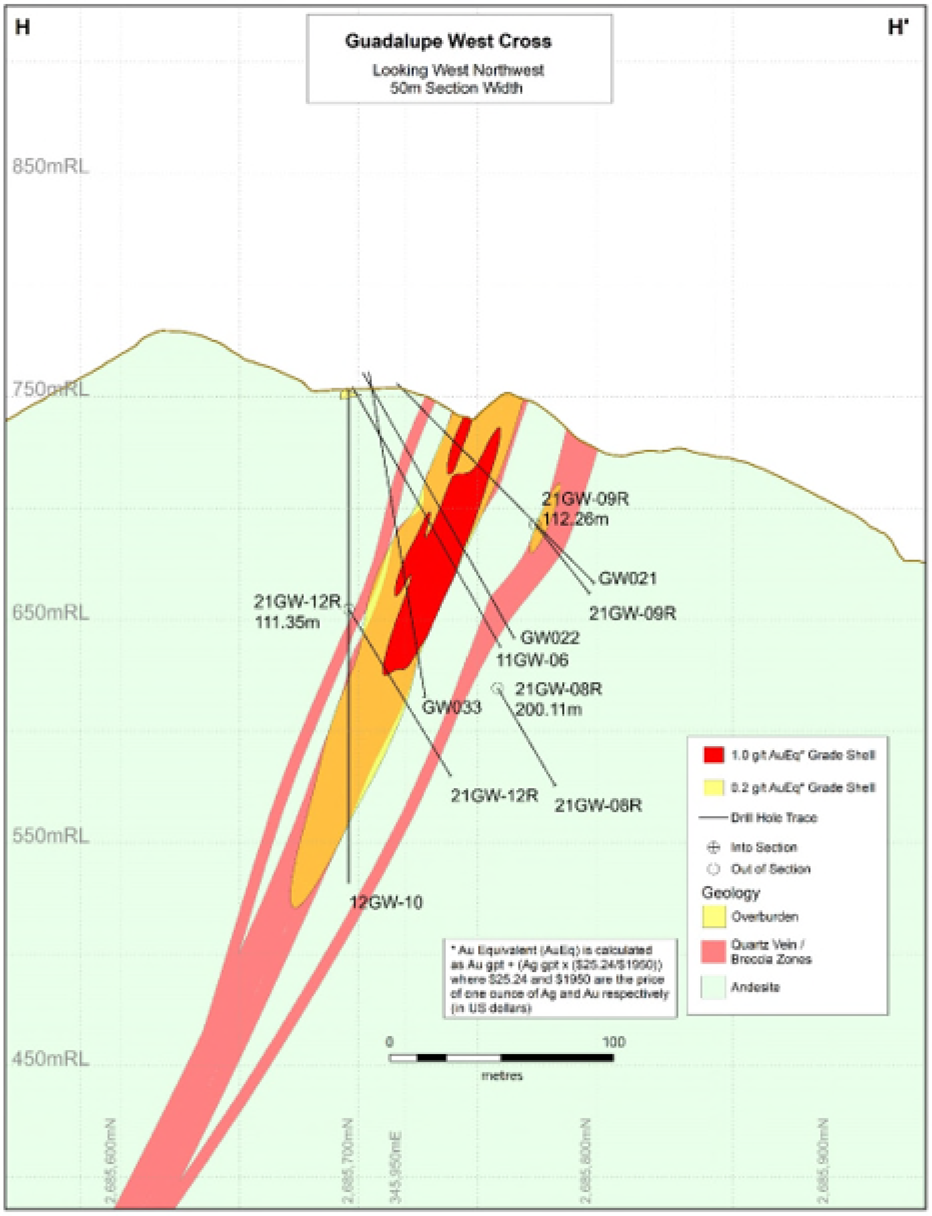


Figure 10-15 Guadalupe West Cross Section



10.10.4 *Other Areas*

Other areas with a significant amount of exploration drilling are Las Primas, Fresnillo and Mariposa.

Las Primas is situated between Guadalupe East and Noche Buena, that is, between the Central and Guadalupe trends. Prior to the Company acquiring the Project, no drilling had been done in the area by previous operators. There are a couple exploration drifts and a shaft that were likely dug in the early 1900s. The area is mostly covered by rhyolitic banded flows that have intruded andesite tuffs and flows. Gold and silver mineralization is widespread in steeply dipping quartz veins and brecciated zones that vary from centimetre scale to 50 metres wide. There is evidence that multiple phases of quartz deposition has occurred, some more silver rich and some nearly barren in both gold and silver.

The Company has drilled 41 core holes into Las Primas for 13,865.3 metres. An example of drill results from Las Primas are shown in Table 10-10, sorted from northwest to southeast and their locations are shown, labeled, on Figure 10-13, along with the other drill holes in Las Primas. A representative cross section through Las Primas is shown in Figure 10-16 and its location is shown on Figure 10-13.

Table 10-10 Las Primas Summary of Drill Results

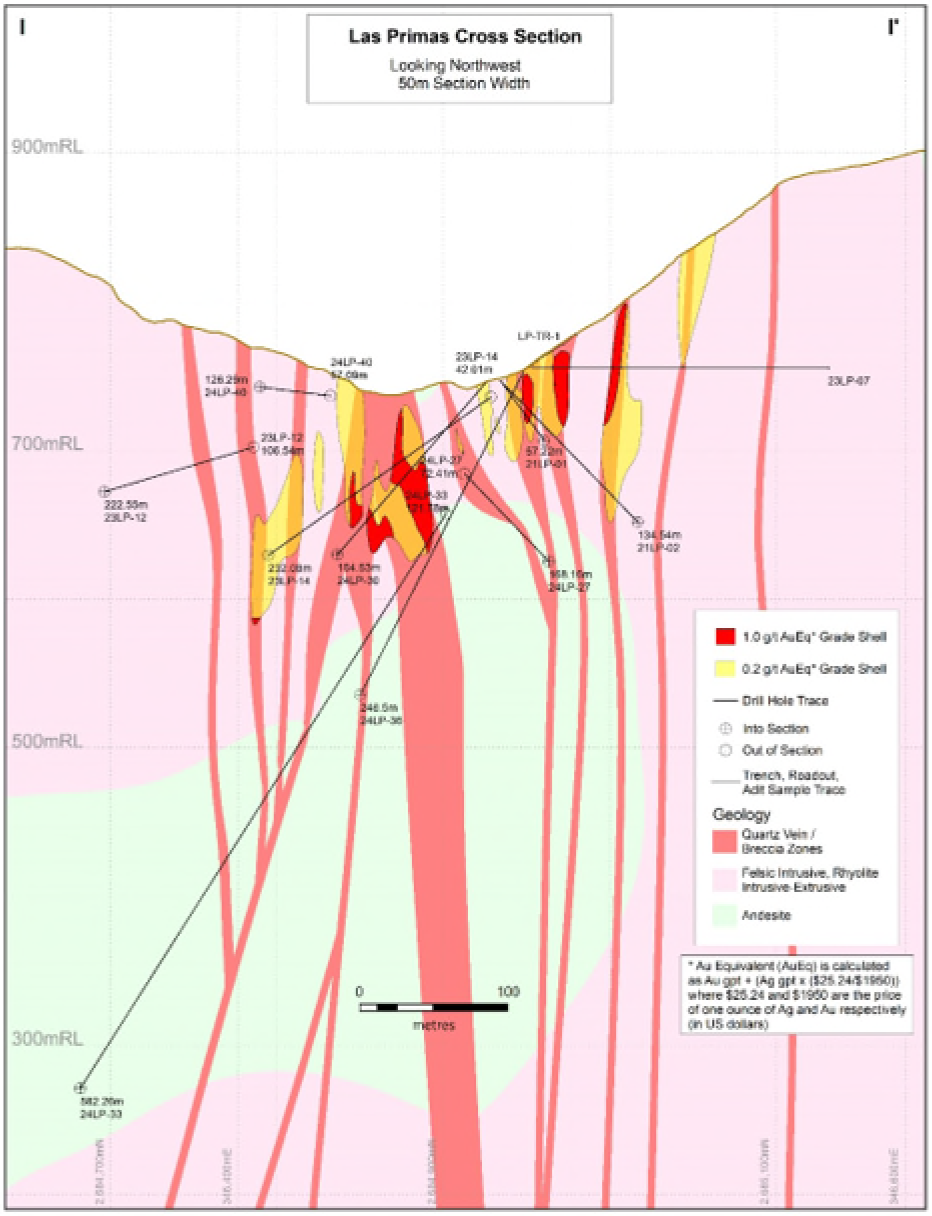
Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
23LP-11	125.4	127.5	2.1	2.1	0.30	14.0	649.0
23LP-11	188.3	189.0	0.7	0.7	2.50	7.0	618.0
23LP-11	241.0	241.7	0.7	0.7	0.20	24.0	591.0
23LP-11	243.0	245.0	2.0	2.0	0.30	4.0	590.0
23LP-05	0.0	6.0	6.0	5.8	1.50	8.0	736.0
23LP-05	30.5	33.3	2.8	2.7	0.80	17.0	743.0
23LP-05	46.4	48.5	2.1	2.1	0.30	4.0	747.0
23LP-05	57.4	58.5	1.1	1.1	0.40	30.0	750.0
23LP-05	71.5	85.3	13.8	13.6	0.60	5.0	755.0
23LP-05	97.5	99.0	1.5	1.5	0.20	2.0	761.0
23LP-05	105.0	106.5	1.5	1.5	0.20	14.0	763.0
23LP-05	127.5	129.0	1.5	1.5	0.30	3.0	768.0
23LP-05	160.3	161.7	1.5	1.4	0.60	22.0	777.0
23LP-05	193.0	195.7	2.7	2.6	0.30	5.0	785.0
23LP-07	0.0	4.5	4.5	4.5	0.40	19.0	755.0
23LP-07	7.5	8.5	1.0	1.0	0.30	2.0	755.0
23LP-07	9.7	24.5	14.9	14.6	0.90	26.0	755.0
including	12.0	15.0	3.0	3.0	1.90	33.0	755.0
& including	17.3	19.2	1.9	1.8	1.10	23.0	755.0
23LP-07	54.5	62.5	8.1	8.0	0.90	21.0	755.0
including	54.5	55.7	1.3	1.3	2.00	47.0	755.0
& including	57.0	58.3	1.3	1.3	1.60	41.0	755.0
23LP-07	76.5	77.5	1.1	1.0	0.40	8.0	755.0
23LP-07	79.9	81.0	1.2	1.1	0.20	1.0	755.0
23LP-07	102.0	103.5	1.5	1.4	1.20	1.0	755.0
23LP-07	161.2	162.0	0.9	0.8	0.50	13.0	755.0
24LP-31	128.0	134.4	6.4	6.3	0.80	12.0	688.0
including	131.5	133.4	2.0	1.9	2.10	21.0	687.0
24LP-31	143.7	144.6	0.9	0.8	16.40	169.0	681.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
24LP-31	146.8	147.6	0.9	0.8	0.20	2.0	679.0
24LP-31	151.7	160.0	8.3	7.5	0.50	19.0	674.0
including	156.0	158.7	2.7	2.4	1.00	46.0	673.0
24LP-31	163.8	165.3	1.5	1.4	0.30	15.0	669.0
24LP-31	175.2	177.6	2.4	2.2	0.30	6.0	663.0
24LP-31	179.4	180.6	1.2	1.1	0.20	23.0	661.0
24LP-31	197.7	198.4	0.8	0.7	0.60	17.0	651.0
24LP-31	200.5	202.7	2.3	2.1	0.30	2.0	649.0
24LP-31	207.3	208.1	0.9	0.8	0.20	3.0	645.0
24LP-31	211.5	212.5	1.1	1.0	0.30	3.0	643.0
24LP-31	220.8	221.6	0.8	0.7	0.40	10.0	638.0
24LP-31	238.8	240.2	1.5	1.4	0.20	3.0	627.0
24LP-31	258.0	259.2	1.2	1.2	0.30	0.0	617.0
24LP-31	336.8	338.4	1.6	1.6	0.50	24.0	573.0
24LP-31	343.3	344.2	0.9	0.9	0.30	7.0	569.0
24LP-31	346.7	347.4	0.8	0.7	0.40	9.0	567.0
24LP-31	375.4	377.0	1.6	1.6	0.20	0.0	551.0
24LP-31	379.4	380.2	0.8	0.8	0.20	8.0	549.0
23LP-18	96.0	97.0	1.0	0.7	0.40	3.0	711.0
23LP-18	142.4	143.2	0.8	0.6	0.40	13.0	678.0
23LP-18	173.9	175.5	1.7	1.2	0.30	3.0	655.0
23LP-18	224.4	230.8	6.4	4.5	11.60	311.0	618.0
including	224.4	228.0	3.6	2.5	20.40	551.0	619.0
including	225.5	227.0	1.5	1.1	41.90	1111.0	618.0
23LP-18	231.9	232.9	1.0	0.7	0.20	4.0	615.0
23LP-18	266.3	267.6	1.3	0.9	0.50	9.0	590.0
23LP-18	306.9	307.9	1.0	0.7	0.30	1.0	562.0
23LP-19	116.5	117.5	1.0	0.7	2.10	3.0	717.0
23LP-19	258.0	259.2	1.2	0.8	0.60	32.0	617.0
23LP-19	343.0	343.8	0.8	0.6	2.90	347.0	557.0
23LP-19	425.5	429.2	3.7	2.6	0.40	64.0	497.0
24LP-35	18.0	20.0	2.0	2.0	0.20	5.0	817.0

Notes:

1. Elevations are at the midpoint of the interval, in metres above sea level (masl).

Figure 10-16 Los Reyes Las Primas Cross Section



Fresnillo is situated between the Central and Z-T trends. This area had received no drilling prior to the Company acquiring the Project and there is no evidence of historical mining in this area either. The area is underlain by a dacitic intrusive that has intruded andesitic tuffs and flows. Capping the dacite intrusive are dacitic tuffs and flows. Later rhyolitic flow dikes cut through these rocks, some contemporaneous with epithermal quartz deposited as veins and matrix fill in brecciated structures. The veins and structures are west dipping at between 40° and 50° and there are apparently multiple anastomosing structures ranging from less than a metre to 30 metres in width.

The Company has drilled 27 core holes into the Fresnillo area recovering 9,682.0 metres of core. An example of drill results from Fresnillo are shown in Table 10-11, sorted by collar location from northwest to southeast and their locations are shown on Figure 10-9. A representative cross section is shown on Figure 10-17 and its location is shown on Figure 10-9.

Table 10-11 Fresnillo Summary of Drill Results

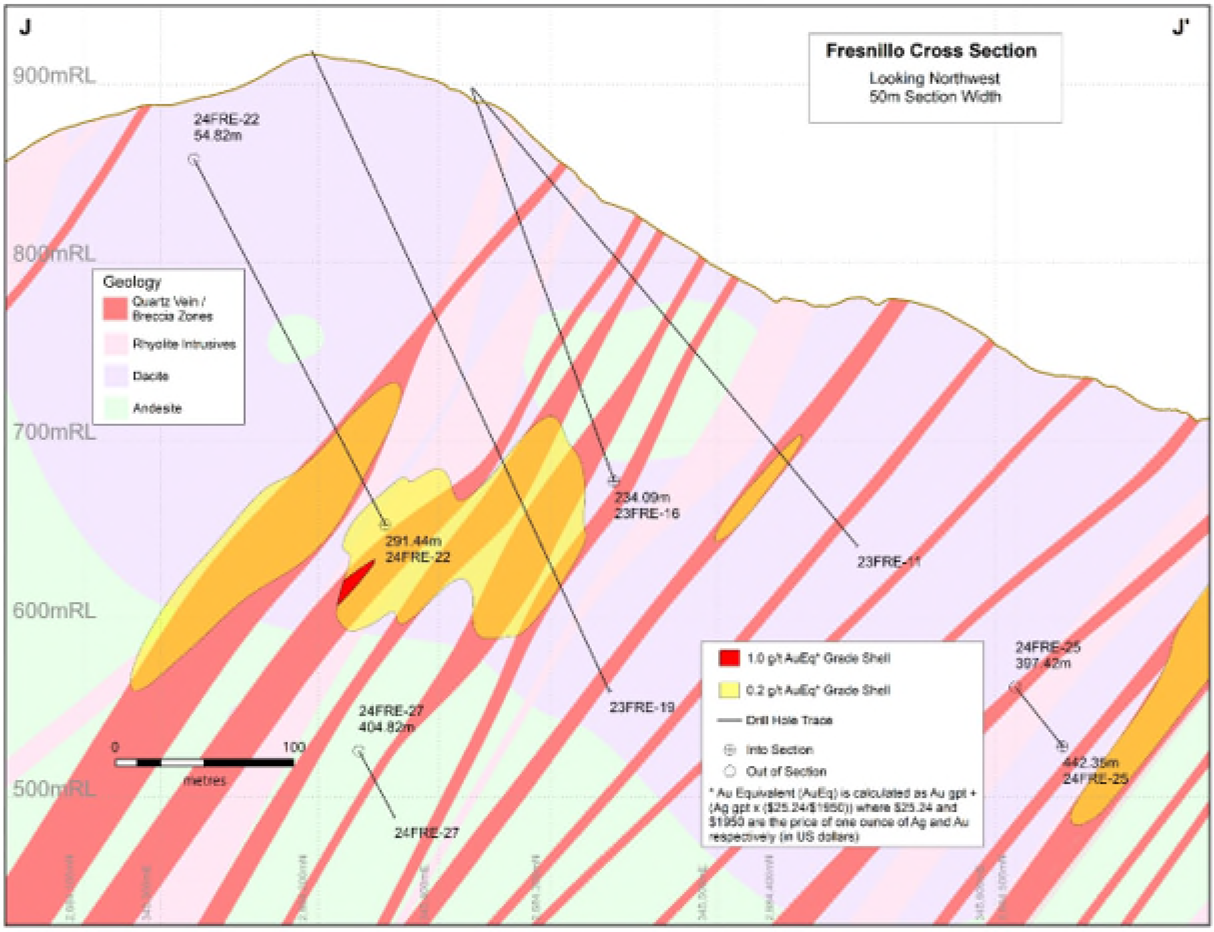
Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
23FRE-17	28.5	29.7	1.2	1.1	7.90	1.0	847.0
23FRE-17	79.5	81.0	1.5	1.4	0.20	3.0	807.0
23FRE-17	141.0	144.0	3.0	2.8	0.20	1.0	758.0
23FRE-17	146.2	148.2	2.0	1.9	4.20	44.0	754.0
including	147.2	148.2	1.0	0.9	8.10	61.0	753.0
23FRE-17	150.3	151.9	1.7	1.6	0.20	5.0	751.0
23FRE-17	180.5	181.7	1.2	1.2	1.00	7.0	727.0
23FRE-17	193.2	194.0	0.8	0.8	0.30	5.0	717.0
23FRE-17	198.4	199.5	1.2	1.1	0.20	5.0	713.0
23FRE-17	214.5	216.2	1.8	1.7	0.20	2.0	700.0
23FRE-17	253.2	254.7	1.5	1.4	0.70	30.0	670.0
22FRE-09	218.3	219.5	1.2	0.8	0.80	37.0	705.0
22FRE-09	231.5	234.5	3.0	1.3	1.20	16.0	694.0
22FRE-09	239.0	242.0	3.0	1.9	0.30	7.0	688.0
22FRE-09	246.5	255.5	9.0	5.8	0.30	5.0	679.0
22FRE-09	258.5	264.5	6.0	5.6	0.60	7.0	670.0
22FRE-09	267.5	286.8	19.3	15.8	1.40	18.0	658.0
including	270.3	273.9	3.6	2.9	4.70	48.0	658.0
including	271.3	272.4	1.1	0.9	11.90	77.0	658.0
& including	277.8	279.3	1.5	1.2	3.20	37.0	658.0
22FRE-09	289.8	291.0	1.2	1.1	0.60	2.0	647.0
22FRE-09	305.1	307.5	2.4	2.0	0.40	5.0	634.0
22FRE-09	318.5	320.0	1.5	1.1	0.40	4.0	623.0
23FRE-19	257.3	258.5	1.2	1.1	0.40	2.0	685.0
23FRE-19	265.2	266.9	1.7	1.5	0.40	16.0	677.0
23FRE-19	267.8	269.1	1.3	1.2	0.20	4.0	675.0
23FRE-19	273.6	286.2	12.6	10.9	1.10	45.0	665.0
including	275.8	276.8	1.0	0.9	6.60	438.0	665.0
23FRE-19	290.4	291.2	0.8	0.7	0.40	4.0	655.0
23FRE-19	292.3	308.1	15.8	13.7	0.50	13.0	646.0
including	292.3	293.1	0.8	0.7	1.20	12.0	653.0
including	304.6	305.5	1.0	0.8	1.90	27.0	647.0
23FRE-19	311.3	324.0	12.8	11.1	0.30	9.0	630.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
23FRE-19	327.6	328.7	1.2	1.0	0.50	2.0	621.0
23FRE-19	329.8	331.2	1.5	1.3	0.30	2.0	619.0
23FRE-19	333.9	338.0	4.1	3.6	0.30	7.0	614.0
23FRE-19	351.5	352.8	1.4	1.2	0.40	2.0	599.0
23FRE-19	369.3	370.0	0.8	0.7	1.10	7.0	583.0
23FRE-19	383.0	385.0	2.0	1.8	0.20	1.0	570.0
24FRE-27	240.0	241.5	1.5	1.4	0.30	19.0	660.0
24FRE-27	244.5	248.4	3.9	3.6	0.30	9.0	656.0
24FRE-27	252.2	269.6	17.5	16.4	0.50	9.0	644.0
including	255.5	256.7	1.3	1.3	1.20	8.0	644.0
& including	266.7	268.2	1.5	1.2	1.10	69.0	637.0
24FRE-27	273.0	290.7	17.7	16.7	0.40	2.0	627.0
24FRE-27	300.4	301.6	1.2	1.1	0.30	1.0	611.0
24FRE-21	328.0	329.2	1.2	1.2	0.30	10.0	606.0
24FRE-21	340.0	342.0	2.0	2.0	0.20	3.0	597.0
24FRE-21	361.4	362.5	1.1	1.0	0.40	10.0	581.0
24FRE-21	363.8	364.7	0.9	0.9	0.20	6.0	579.0
24FRE-21	371.4	372.4	1.0	1.0	0.30	1.0	573.0
24FRE-21	374.7	378.0	3.3	3.2	0.40	4.0	570.0
24FRE-21	382.8	385.4	2.7	2.6	0.30	10.0	564.0
24FRE-21	393.8	394.7	0.9	0.9	0.20	17.0	556.0
24FRE-21	396.0	397.5	1.5	1.4	0.30	3.0	554.0
24FRE-21	409.5	411.0	1.5	1.5	0.20	1.0	544.0
24FRE-21	428.4	429.3	0.9	0.9	1.30	89.0	529.0
24FRE-21	433.6	434.3	0.7	0.7	0.30	8.0	526.0
24FRE-21	439.3	442.0	2.8	2.8	0.60	3.0	520.0
24FRE-21	448.6	449.9	1.4	1.4	0.20	1.0	514.0
24FRE-21	475.9	476.7	0.8	0.8	0.50	2.0	493.0
24FRE-21	484.0	489.0	5.0	5.0	0.40	1.0	485.0

Notes:

1. Elevations are at the mid point of the interval, in metres above sea level (masl).

Figure 10-17 Los Reyes Fresnillo Cross Section



Mariposa is situated at the north end of the Z-T trend, just north of where the Guadalupe trend intersects the Z-T trend. There are historical workings into the Mariposa deposit including three levels, the largest of which saw several thousand tonnes extracted for processing in the 1940's and possibly a ten thousand tonne sample extracted in the early 1980's, the latter reportedly at a grade of 5.2 grams per tonne gold. Northern Crown Mining drilled one RC hole into the Mariposa deposit in 1997 (166.1 metre). Mineralization at Mariposa is within the brecciated, quartz infilled structure along the contact of an early granodiorite and later andesite tuffs and flows as well as related quartz veins hosted in andesite within the footwall of the structure. The structure is up to 35 metres in width but there is evidence that a dilation zone twice this width may have been the target of the historical mining.

Prime has drilled 13 core holes into Mariposa for 2,906.0 metres. An example of the drill results from Mariposa are shown in Table 10-12, sorted northwest to southeast and their locations are shown on Figure 10-18. A representative cross section is shown on Figure 10-19.

Table 10-12 Mariposa Summary of Drill Results

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
23MA-13	90.5	91.6	1.1	0.6	1.60	17.0	620.0
23MA-13	117.4	118.5	1.1	0.5	0.60	7.0	595.0
23MA-11	52.4	54.6	2.2	1.3	0.50	6.0	655.0
23MA-11	72.0	79.0	7.0	4.0	0.60	9.0	634.0
including	72.0	73.6	1.6	0.9	1.00	7.0	637.0
& including	76.8	78.2	1.5	0.8	1.10	19.0	634.0
23MA-11	84.2	84.9	0.7	0.4	0.70	10.0	626.0
23MA-11	96.0	96.9	0.9	0.5	0.40	6.0	615.0
23MA-11	104.2	105.0	0.8	0.5	0.30	10.0	608.0
23MA-11	115.4	116.2	0.8	0.5	0.20	6.0	598.0
23MA-11	117.2	118.5	1.3	0.7	0.20	6.0	596.0
23MA-11	120.5	121.5	1.0	0.5	0.20	7.0	593.0
23MA-11	131.5	133.0	1.5	0.9	0.20	4.0	583.0
23MA-11	140.4	141.0	0.7	0.4	0.50	3.0	575.0
23MA-11	156.0	160.6	4.6	2.6	0.30	9.0	559.0
23MA-11	165.8	167.0	1.2	0.7	0.30	5.0	551.0
23MA-11	184.0	186.2	2.2	1.3	3.10	15.0	534.0
21MA-02	64.1	69.2	5.1	3.6	0.70	5.0	647.0
including	68.2	69.2	1.0	0.7	2.10	18.0	645.0
21MA-02	77.4	99.0	21.7	15.3	0.90	1.0	628.0
including	85.6	86.5	1.0	0.7	5.80	23.0	628.0
& including	94.0	95.5	1.5	1.1	2.60	16.0	628.0
22MA-09	76.9	78.0	1.1	0.4	1.00	11.0	633.0
22MA-09	91.5	93.0	1.5	1.0	0.90	6.0	619.0
22MA-09	100.2	102.0	1.8	1.2	1.10	9.0	610.0
22MA-09	118.5	123.0	4.5	2.9	1.50	15.0	591.0
including	119.5	120.5	1.0	0.6	5.40	29.0	592.0
22MA-09	129.0	132.0	3.0	2.4	0.30	11.0	582.0
22MA-09	136.5	139.5	3.0	1.7	0.70	13.0	574.0
22MA-09	142.5	143.5	1.0	0.2	0.30	8.0	570.0
22MA-09	144.5	147.0	2.5	1.3	0.30	8.0	567.0
22MA-09	150.0	151.5	1.5	1.0	0.40	9.0	562.0
22MA-09	153.0	154.5	1.5	1.0	0.60	15.0	559.0
22MA-09	159.0	160.5	1.5	1.0	0.30	7.0	553.0
22MA-09	162.0	164.0	2.0	1.3	0.30	10.0	550.0
22MA-09	166.5	168.0	1.5	1.0	0.20	14.0	546.0
22MA-09	177.0	181.5	4.5	2.4	0.40	10.0	535.0
22MA-09	183.0	184.5	1.5	1.0	0.30	7.0	530.0

Drill Hole	From (m)	To (m)	Interval (m)	etw (m)	Au (g/t)	Ag (g/t)	Elevation (m) [1]
22MA-09	189.0	190.5	1.5	1.0	0.30	6.0	524.0
22MA-09	199.5	201.0	1.5	1.0	0.30	8.0	514.0
22MA-09	236.7	238.0	1.3	0.8	0.20	1.0	478.0
22MA-08	175.7	187.5	11.8	8.3	1.10	11.0	524.0
including	175.7	177.0	1.3	0.9	3.40	23.0	529.0
& including	178.5	180.0	1.5	1.1	1.90	16.0	524.0
& including	183.0	185.0	2.0	1.4	1.80	12.0	520.0
22MA-08	195.0	202.1	7.1	5.4	1.00	9.0	508.0
including	199.1	200.6	1.5	1.1	2.10	11.0	508.0
22MA-08	206.1	212.6	6.5	4.9	0.70	9.0	497.0

Figure 10-18 Los Reyes Mariposa Area Drill Hole Locations

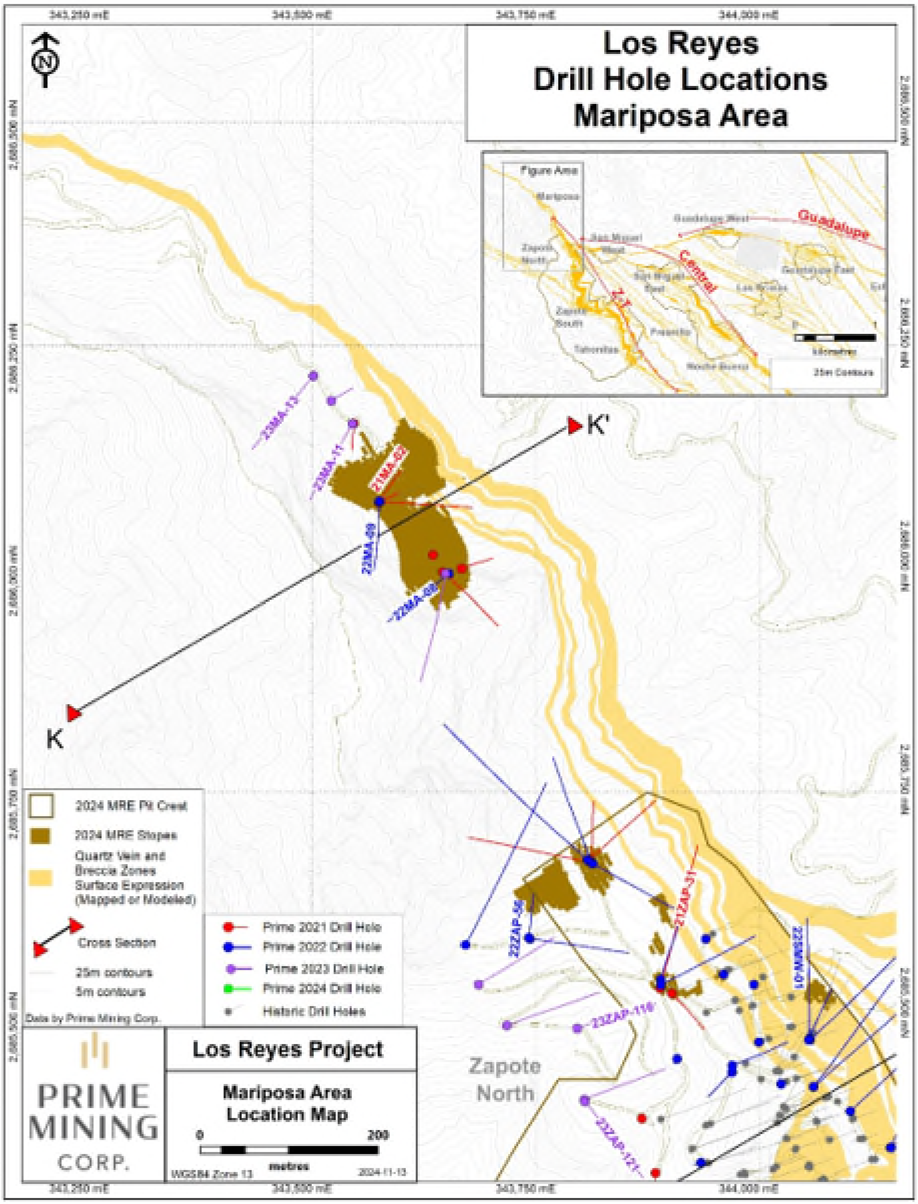
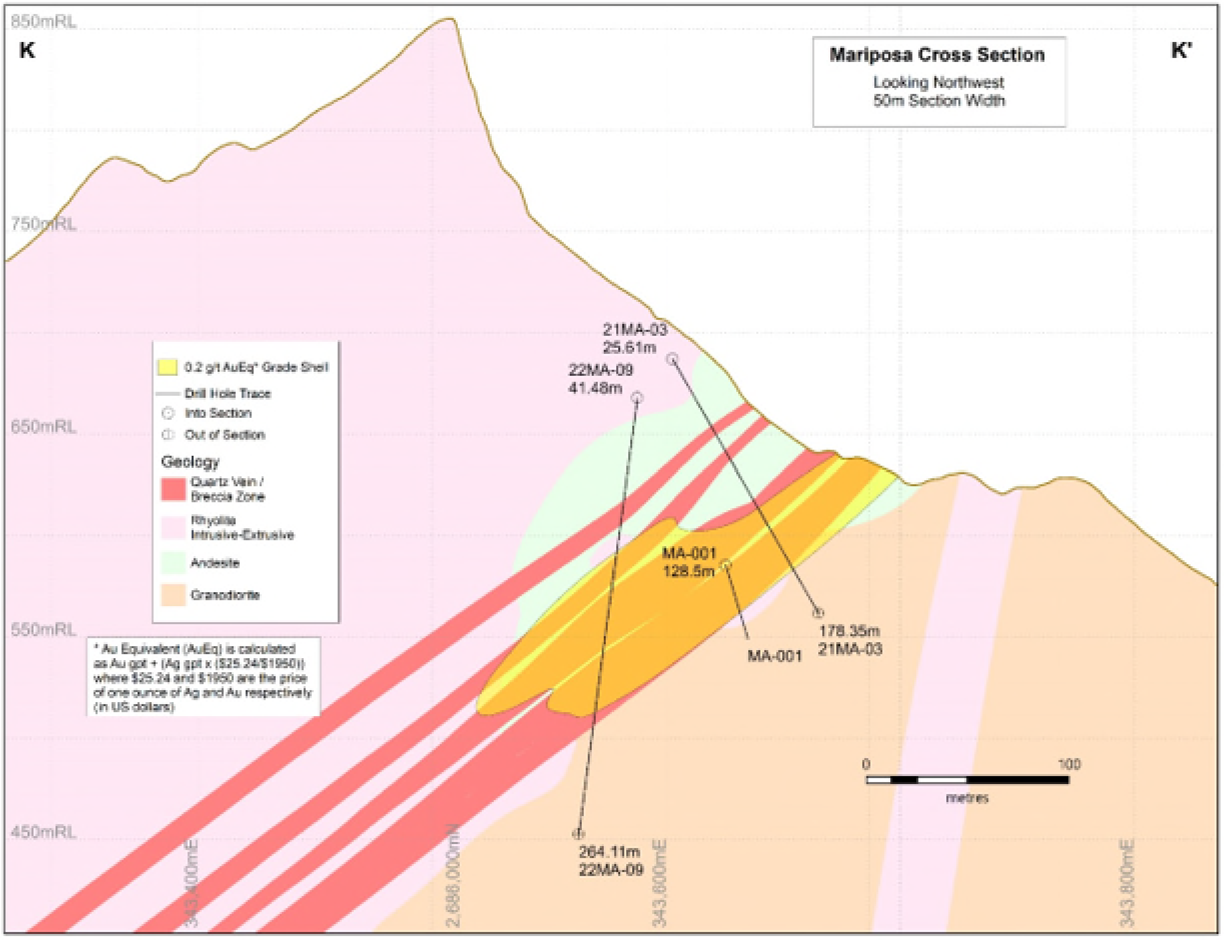


Figure 10-19 Los Reyes Mariposa Cross Section



10.11 Comments on Drill Programs

In the opinion of the Independent QP, the quantity and quality of the lithological, geotechnical, collar and down hole survey data collected in the drill programs are sufficient to support mineral resource and mineral reserve estimation as follows:

- Core logging meets industry standards for gold exploration.
- Collar surveys have been performed using industry-standard instrumentation.
- Downhole surveys have been performed using industry-standard instrumentation.
- Recovery data from core drill programs are acceptable.
- There are no apparent drill, sampling or recovery factors that could impact the accuracy and reliability of the drilling results.
- Geotechnical logging of drill core meets industry standards.

Drilling is normally perpendicular to the strike of the mineralization but due to topographical conditions and road access, oblique intersections are common. Depending on the dip of the drill hole, and the dip of the mineralization, drill intercept widths are typically greater than true widths.

Drill hole orientations are appropriate for the mineralization style and have been drilled at orientations that are optimal for the orientation of mineralization for the bulk of the deposit area. Drill orientations are shown in plan figures (Figure 10-2 to Figure 10-4) and representative cross-sections above and can be seen to test the mineralization appropriately.

11. SAMPLE PREPARATION, ANALYSES, AND SECURITY

The Prime samples were submitted for crushing and pulverization to the ALS and BV facilities in Mexico.

11.1 Sample Preparation and Analysis

11.1.1 *ALS Global, Zacatecas/Guadalajara, México*

Prime submitted diamond drill core samples to ALS for preparation and analysis.

The samples were prepared using ALS's standard sample preparation procedure PREP-31 which consists of logging the sample in the ALS internal tracking system and attaching a barcode to each sample. The sample is weighed, and if necessary, will be dried. The entire sample is then crushed to better than 70 percent passing two millimeters. The crushed sample is then riffle split to obtain a 250-gram subsample. The subsample is pulverised to better than 85 percent passing 0.075 millimeters.

A 30-gram aliquot of the prepared sample is fused with a mixture of lead oxide, sodium carbonate, borax, silica, and other reagents as required, inquarted with 6 milligrams of gold-free silver and then cupelled to yield a precious metal bead. The bead is digested in 0.5 milliliters dilute nitric acid in the microwave oven, 0.5 milliliters concentrated hydrochloric acid is then added, and the bead is further digested in the microwave at a lower power setting. The digested solution is cooled, diluted to a total volume of 4 milliliters with de-mineralized water, and analyzed for gold by atomic absorption spectroscopy against matrix-matched standards. (ALS procedure document)

If the gold results are greater than ten ppm a new aliquot of the prepared sample is fused, the bead is parted to remove the silver and the bead weighed for gold.

A 0.25-gram aliquot of the prepared sample is digested with perchloric, nitric, hydrofluoric, and hydrochloric acids. The residue is topped up with dilute hydrochloric acid and the resulting solution is analyzed by inductively coupled plasma-atomic emission spectrometry ("ICP"). Results are reported for a suite of thirty-four elements. (ALS procedure document) The suite of elements is listed in Table 11-1.

No aspect of the sample preparation process was conducted by an employee, officer, director, or associate of Prime.

Table 11-1 List of Analytes, ME-ICP61, ALS Global

Analyte	Units	Lower Limit	Upper Limit	Analyte	Units	Lower Limit	Upper Limit
Silver	ppm	0.5	100	Mangane	ppm	5	100000
Aluminum	%	0.01	50	Molybde	ppm	1	10000
Arsenic	ppm	5	10000	Sodium	%	0.01	10
Barium	ppm	10	10000	Nickel	ppm	1	10000
Beryllium	ppm	0.5	1000	Phospho	ppm	10	10000
Bismuth	ppm	2	10000	Lead	ppm	2	10000
Calcium	%	0.01	50	Sulphur	%	0.01	10
Cadmium	ppm	0.5	1000	Antimon	ppm	5	10000
Cobalt	ppm	1	10000	Scandiu	ppm	1	10000
Chromium	ppm	1	10000	Strontiu	ppm	1	10000
Copper	ppm	1	10000	Thorium	ppm	20	10000
Iron	%	0.01	50	Titanium	%	0.01	10
Gallium	ppm	10	10000	Thallium	ppm	10	10000
Potassium	%	0.01	10	Uranium	ppm	10	10000
Lanthanum	ppm	10	10000	Vanadiu	ppm	1	10000
Lithium	ppm	10	10000	Tungsten	ppm	10	10000
Magnesium	%	0.01	50	Zinc	ppm	2	10000

11.1.2 *Bureau Veritas, Durango, México*

Prime submitted diamond drill core samples and reverse circulation samples to BV for preparation and analysis.

The samples were prepared using BV's PRP70-250 preparation procedure. The samples are logged in the BV Laboratory Information Management System, weighed, and if necessary dried before being crushed to greater than 70 percent passing two millimeters. The crushed sample is then riffle split to obtain a 250-gram subsample. The subsample is pulverised to better than 85% passing 0.075 millimeters.

Like the samples submitted to ALS, the samples are analyzed for gold by fire assay and for multiple elements by four-acid digestion with ICP finish.

No aspect of the sample preparation process was conducted by an employee, officer, director, or associate of Prime.

11.1.3 *Security*

The core is boxed at the drill rig (RC samples are bagged) and picked up daily by Prime personnel for direct transport to the Prime's fenced-in logging facility. The core remains in the fenced yard until it has been logged, photographed, and split. All sample intervals are recorded in Primes's Access Capture software and a sample submittal inventory form is prepared for the laboratory.

Split samples are bagged in prelabeled sample bags (with a sample tag inside the bag), and double bagged in a larger rice bag and labelled with sample from-to and bag number. These are stored in the secure logging area until personnel from the laboratory collects them. Sample collection usually occurs once or twice per week. The laboratory personnel check the sample count and transports the samples directly to the laboratory facility. Confirmation is sent to Prime from the laboratory that all samples submitted as per the form have been received. If the laboratory sample count differs from the Prime's submittal form, the differences will be flagged for review.

Core samples (or RC samples) not submitted for analysis are stored in their original core box (or RC cuttings bag) and transported to a locked warehouse for storage.

11.1.4 *Analytical Quality Control*

Prime has submitted half drill core samples and reverse circulation samples. The samples were assayed for gold by fire assay, and multiple elements by four-acid digest.

Prime has maintained a quality control program that includes the insertion of blank materials, CRMs, the selection of preparation duplicates and the submission of pulps to a secondary laboratory for check assaying.

Prime submitted samples to both ALS and BV for sample preparation and analysis. The samples were prepared and analyzed in Zacatecas, Guadalajara, and Durango, Mexico, as well as some analyses in Vancouver, British-Columbia, Canada.

Blanks materials and CRMs were inserted at a rate of one in fifty samples.

ALS Global, México

Blank Materials

A locally sourced basalt was inserted as a blank material 689 times in regular sequence with samples submitted to ALS. The blank materials are determined to have failed when they assay more than ten times the detection limit of 0.05ppm gold or 5ppm silver. There are five blank material failures. The failure rate for the blank materials is less than 1% and there is no evidence of systematic contamination. The blank material results are acceptable.

Certified Reference Materials

Eleven different reference materials were inserted 930 times in regular sequence with the samples and analyzed for gold by fire assay and multiple elements by four-acid digest. The performance for gold and silver are summarized in Table 11-2 and Table 11-3.

A quality control failure is defined as an assay result for a certified reference material that is outside plus or minus three standard deviations of the expected value. A total of twenty-four quality control failures were identified for gold and twenty-five for silver. This represents a failure rate of less than 3% for both gold and silver. The overall failure rate is acceptable.

The failures were removed to calculate the percent of expected (the "Percent of Expected"). The Percent of Expected demonstrates that there are no significant biases in the results but that on average the gold and silver results are reporting higher than the expected values.

Based on the results of the CRMs, it can be concluded that the accuracy of the results from ALS are acceptable.

Table 11-2 Summary Reference Material Statistics for Gold, ALS Global

RM	N	Failures Excluded	Au ppm		Observed Au ppm		Percent of Expected
			Expected	Std. Dev.	Average	Std. Dev.	
CDN-GS-1ZB	6	-	6.47	0.280	6.53	0.148	101%
CDN-GS-6G	81	6	6.30	0.150	6.41	0.188	102%
OREAS 609b	251	1	4.97	0.260	5.15	0.150	104%
CDN-GS-1Z	158	4	1.16	0.048	1.17	0.051	101%
CDN-CM-47	57	1	1.13	0.055	1.13	0.071	100%
GDN-GS-P8K	15	5	0.83	0.045	0.84	0.051	101%
OREAS 601b	43	-	0.78	0.021	0.77	0.017	100%
OREAS 607b	173	1	0.70	0.025	0.71	0.016	102%
CDN-ME-1601	25	3	0.61	0.023	0.62	0.028	102%
OREAS 600b	91	3	0.20	0.007	0.21	0.004	102%
CDN-SS-2201	6	-	0.07	0.004	0.08	0.002	105%
Total	**906**	**24**					**102%**

Table 11-3 Summary Reference Material Statistics for Silver, ALS Global

RM	N	Failures Excluded	Ag ppm		Observed Ag ppm		Percent of Expected
			Expected	Std. Dev.	Average	Std. Dev.	
CDN-GS-1Z	149	10	89.5	2.2	91.6	2.6	102%
CDN-GS-6G	75	9	84.0	2.5	86.6	2.3	103%
CDN-GS-1ZB	6	-	81.0	3.5	79.9	4.7	99%
CDN-CM-47	57	1	69.0	3.0	69.5	3.3	101%
OREAS 601b	43	-	50.1	1.7	50.1	1.1	100%
CDN-ME-1601	26	2	39.6	0.9	40.4	1.4	102%
CDN-SS-2201	6	-	31.6	1.4	31.3	0.8	99%
OREAS 600b	91	1	25.1	1.0	25.7	0.7	102%
OREAS 609b	252	-	24.6	1.0	24.4	0.7	99%
CDN-GS-P8K	19	1	8.1	0.3	8.3	0.4	103%
OREAS 607b	173	1	6.1	0.3	6.2	0.3	101%
Total	**897**	**25**					**101%**

Field Duplicates

The field duplicate results received from ALS consist of quarter core duplicates. The quarter core duplicates are taken for every 50th and 100th sample, with the duplicate result reported in the 55th and 105th sample.

During 2022, the submission of quarter core duplicates was discontinued. Prime has already obtained a significant quantity of quarter core duplicate results for the Project, and understand the variability associated with sampling the core.

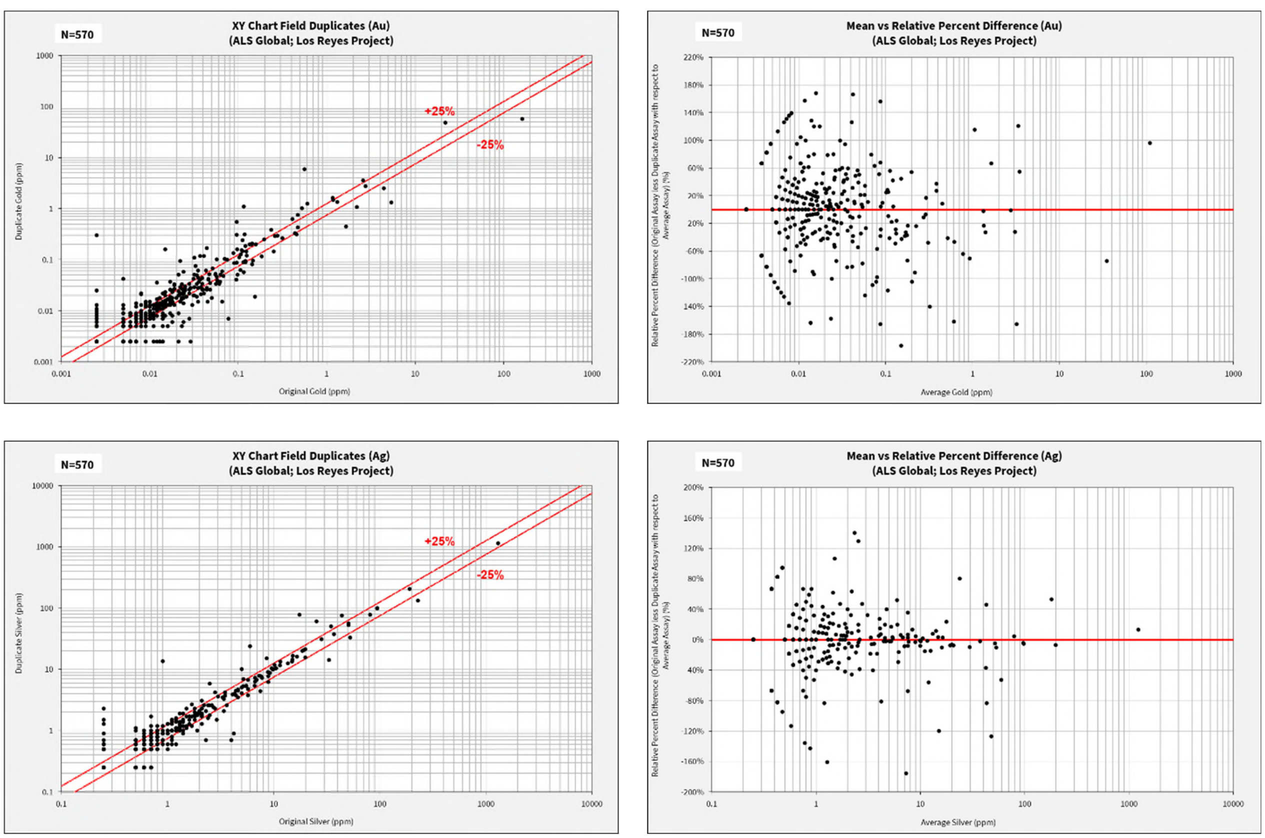
Precision, by definition, is about ±100% at ten times the detection limit. Assays close to the detection limit are not included in calculations of precision. This applies to all discussions of precision in this section.

A total of 570 quarter core duplicates were collected and submitted for analyses. A total of 73 quarter core duplicates out of 570 reported above 0.05ppm gold, and 60 reported above 5ppm silver. Twenty-nine percent of the duplicate pairs are reporting within ±25% for gold, and seventy-five percent for silver. This is considered acceptable for quarter core duplicates.

Table 11-4 Summary of Field Duplicate Results for Gold, ALS Global

			% of Sample Pairs (>10x d.l.) Reporting within			
Analyte	***# of Pairs***	***# of Pairs above 10x d.l.***	***±5%***	***±10%***	***±20%***	***±50%***
Au	570	73	7%	14%	29%	63%
Ag	570	57	33%	56%	75%	84%

Figure 11-1 XY and RPD Chart for Gold and Silver in Field Duplicates, ALS Global



Preparation Duplicates

Preparation duplicates are created by splitting a second cut of the crushed sample in the same way and for the same weight as the original sample.

Prime select samples ending in '25', or one sample in one hundred samples as a preparation duplicate. It is expected that the preparation duplicate pairs will be more similar than the quarter core duplicates due to the smaller particle size during sub-sampling.

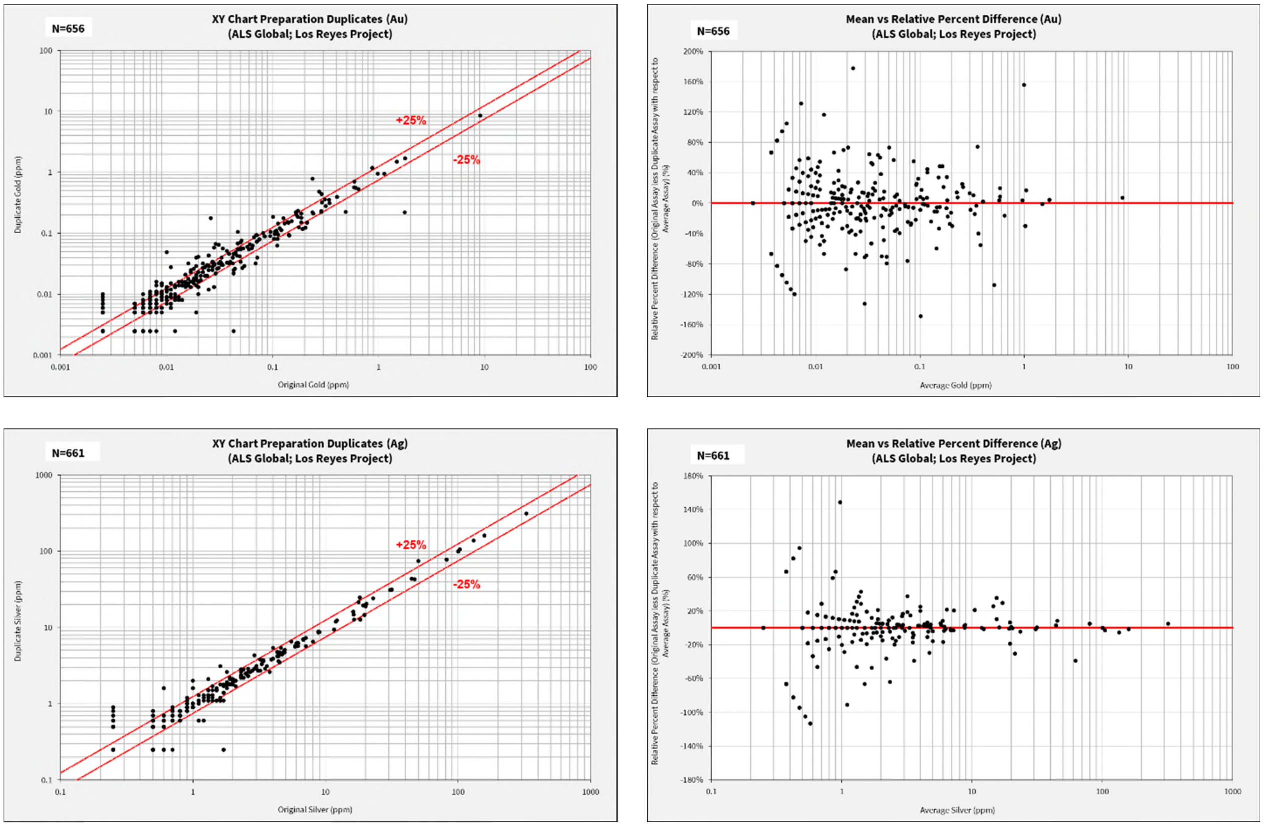
A total of 656 preparation duplicates were analyzed for gold. A total of 107 duplicate pairs out of 656 reported above 0.05ppm gold. The preparation duplicates for gold have 63% of the duplicate pairs reporting within ±25%. These results are considered acceptable.

A total of 661 preparation duplicates were analyzed for silver. Sixty-two duplicate pairs out of 661 reported above 5ppm silver. The preparation duplicates for silver have 85% of the duplicate pairs reporting within ±25%. These results are considered acceptable.

Table 11-5 Summary of Preparation Duplicate Results for Gold and Silver, ALS Global

			% of Sample Pairs (>10x d.l.) Reporting within			
Analyte	***# of Pairs***	***# of Pairs above 10x d.l.***	***±5%***	***±10%***	***±20%***	***±50%***
Au	656	107	17%	42%	63%	91%
Ag	661	62	55%	71%	85%	100%

Figure 11-2 XY and RPD Chart for Gold and Silver in Preparation Duplicates, ALS Global



Pulp Duplicates

The assays for pulp duplicates provide an estimate of the reproducibility related to the uncertainties inherent in the analytical method and the homogeneity of the pulps. The precision or relative percent difference calculated for the pulp duplicates indicates whether pulverizing specifications should be changed and/or whether alternative methods should be considered.

Commercial laboratories routinely assay a second aliquot of the sample pulp, for approximately one in ten samples, these are pulp duplicates. The pulp duplicate results are used by the laboratory for their internal quality control monitoring. Prime selects every sample ending in '75', or one sample in one hundred samples, to be analyzed in duplicate. Only the Prime pulp duplicates are plotted below.

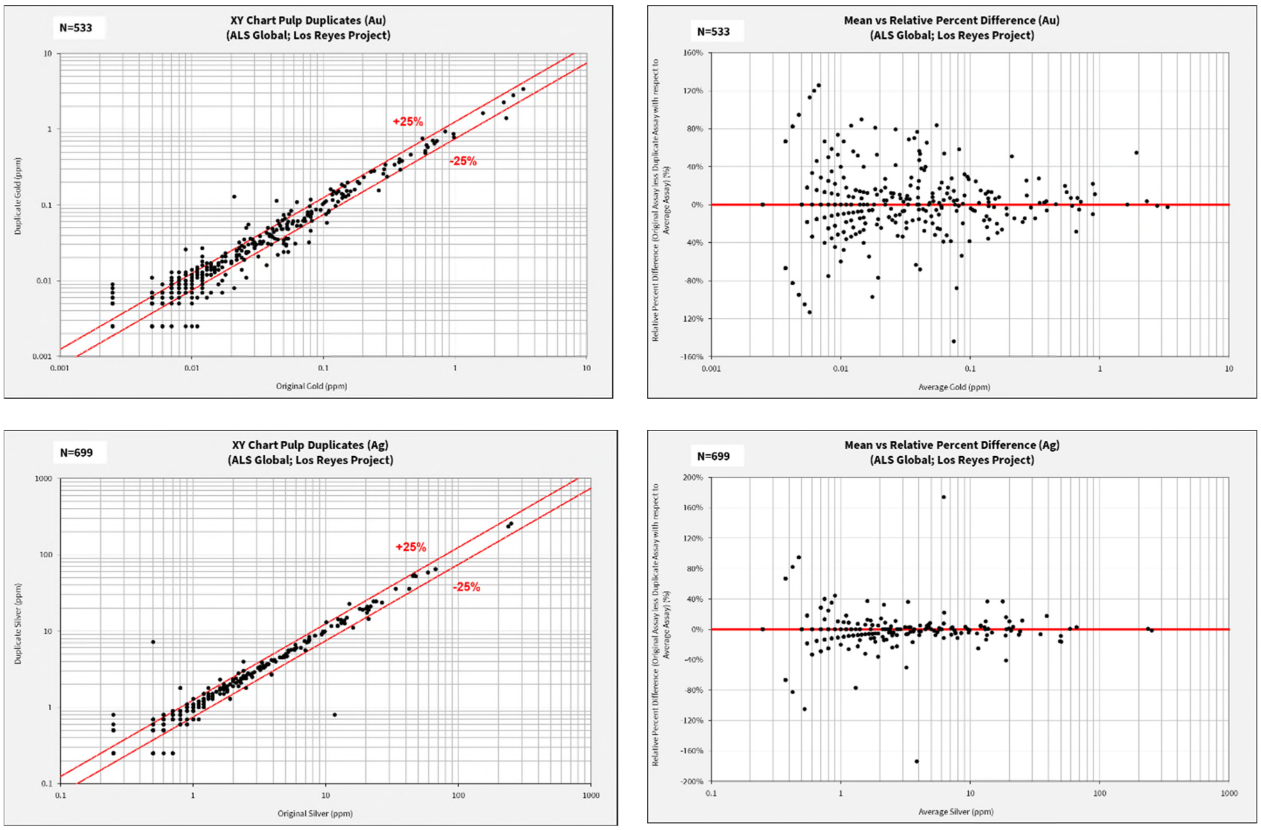
Pulp duplicate results for gold are available for 533 samples. A total of 100 duplicate pairs out of the 533 reported above 0.05ppm gold. The pulp duplicates for gold have 70% of the duplicate pairs reporting within ±25%. Precision for the pulp duplicates is acceptable.

Pulp duplicate results for silver are available for 699 samples. A total of 91 duplicate pairs out of the 699 reported above 5ppm silver. The pulp duplicates for silver have 92% of the duplicate pairs reporting within ±25%. Precision for the pulp duplicates is acceptable.

Table 11-6 Summary of Pulp Duplicate Results for Gold and Silver, ALS Global

			% of Sample Pairs (>10x d.l.) Reporting within			
Analyte	***# of Pairs***	***# of Pairs above 10x d.l.***	***±5%***	***±10%***	***±20%***	***±50%***
Au	533	100	26%	42%	70%	89%
Ag	699	91	55%	74%	92%	99%

Figure 11-3 XY and RPD Chart for Gold and Silver in Pulp Duplicates, ALS Global



Check Assays

Check assays are recommended where the same pulp that was assayed originally is submitted to a different laboratory for the same analytical procedures primarily to augment the assessment of bias based on the reference materials and in-house control samples submitted to the original laboratory.

A total of 260 pulps were selected from the samples analyzed at ALS. The samples were submitted to BV for check assaying. The methods from both laboratories are comparable.

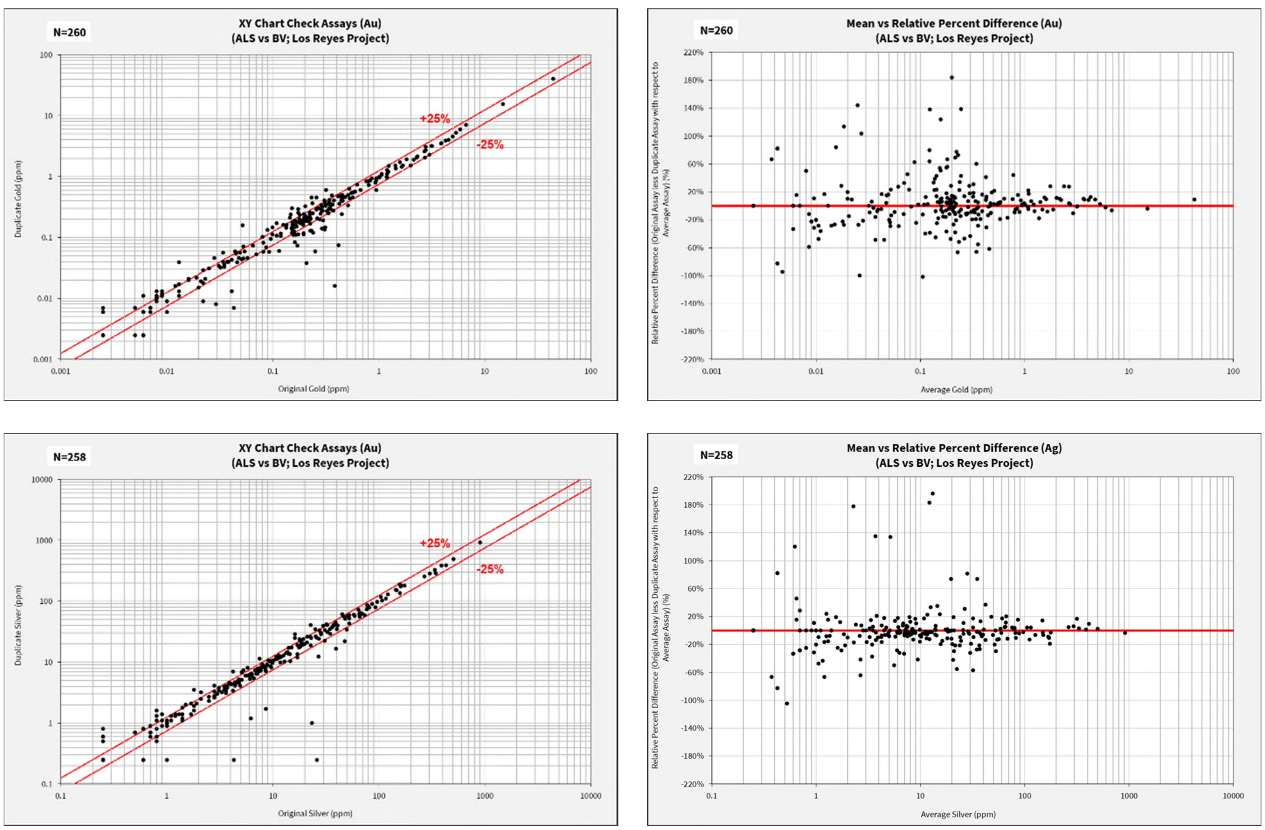
Seventy-five percent of the check assay results for gold are within ± 25% of the two sets of laboratory results; this is acceptable agreement. In fifty-eight percent of cases ALS is higher than BV. The average RPD for gold between ALS and BV is 6%, this indicates that on average the ALS results are higher than BV results by about 6%. Based on the charts in Figure 11-4, the results are well distributed above and below zero percent relative difference, especially for results above 0.5ppm gold.

For the silver results, 85% are within ± 25% of the two sets of laboratory results. The results are well distributed above and below zero relative percent difference. The average difference between the two laboratories is 3%, with the results being higher at BV for 56% of the case.

Table 11-7 Summary of Check Assay Results for Gold and Silver, ALS vs BV

				% of Sample Pairs (>10x d.l.) Reporting within			
Analyte	***# of Pairs***	***# of Pairs above 10x d.l.***	***Average RPD***	***±5%***	***±10%***	***±25%***	***±50%***
Au	260	198	6%	20%	46%	75%	89%
Ag	258	158	3%	41%	58%	85%	94%

Figure 11-4 XY and RPD for Gold and Silver in Check Assays, ALS vs BV



Bureau Veritas, Mexico

Blank Materials

A locally sourced basalt was inserted as a blank material 761 times in regular sequence with samples submitted to BV. Blank materials were determined to have failed when they assayed more than ten times the detection limit or 0.05ppm gold and 5ppm silver. There is a failure rate of less than 1% for blank materials and no evidence of systematic contamination.

Certified Reference Materials

Ten different reference materials were inserted 1,600 times in regular sequence with the samples and analyzed for gold by fire assay and multiple elements by four-acid digest. The performance for gold and silver are summarized in Table 11-8 and Table 11-9.

A total of seventy-seven quality control failures were identified for gold and forty-two for silver. This represents a failure rate of 3% for gold and 5% for silver. The overall failure rate is acceptable.

The Percent of Expected demonstrates that there are no significant biases in the results but that on average the gold results are reporting 1% above the expected values and silver results are reporting at the expected values.

Based on the results of the CRMs, it can be concluded that the accuracy of the results from BV are acceptable.

Table 11-8 Summary Reference Material Statistics for Gold, Bureau Veritas

RM	N	Failures Excluded	Au ppm		Observed Au ppm		Percent of Expected
			Expected	Std. Dev.	Average	Std. Dev.	
CDN-GS-6G	57	4	6.30	0.150	6.34	0.201	101%
OREAS 609b	341	-	4.97	0.260	5.17	0.127	104%
CDN-GS-1P5T	139	5	1.75	0.170	1.78	0.173	102%
CDN-GS-1Z	202	19	1.16	0.048	1.16	0.060	100%
CDN-CM-47	136	11	1.13	0.055	1.14	0.070	101%
OREAS 601b	283	17	0.78	0.021	0.76	0.023	98%
OREAS 607b	118	1	0.70	0.025	0.71	0.022	103%
CDN-ME-1601	193	15	0.61	0.023	0.62	0.027	100%
CDN-ME-1101	5	-	0.56	0.028	0.62	0.022	109%
OREAS 600b	49	5	0.20	0.007	0.21	0.008	101%
Total	**1,523**	**77**					**101%**

Table 11-9 Summary Reference Material Statistics for Silver, Bureau Veritas

RM	N	Failures Excluded	Ag ppm		Observed Ag ppm		Percent of Expected
			Expected	Std. Dev.	Average	Std. Dev.	
CDN-GS-1P5T	136	9	92.0	2.55	93.5	3.19	102%
CDN-GS-1Z	206	16	89.5	2.20	90.2	2.72	101%
CDN-GS-6G	59	2	84.0	2.50	83.5	2.91	99%
CDN-CM-47	146	1	69.0	3.00	67.8	3.46	98%
CDN-ME-1101	5	-	68.2	2.30	65.4	2.75	96%
OREAS 601b	296	4	50.1	1.74	50.7	1.82	101%
CDN-ME-1601	200	8	39.6	0.90	39.8	0.99	101%
OREAS 600b	54	-	25.1	1.00	25.0	0.89	100%
OREAS 609b	342	-	24.6	1.03	24.1	0.74	98%
OREAS 607b	118	2	6.1	0.26	6.2	0.28	101%
Total	**1561**	**42**					**100%**

Field Duplicates

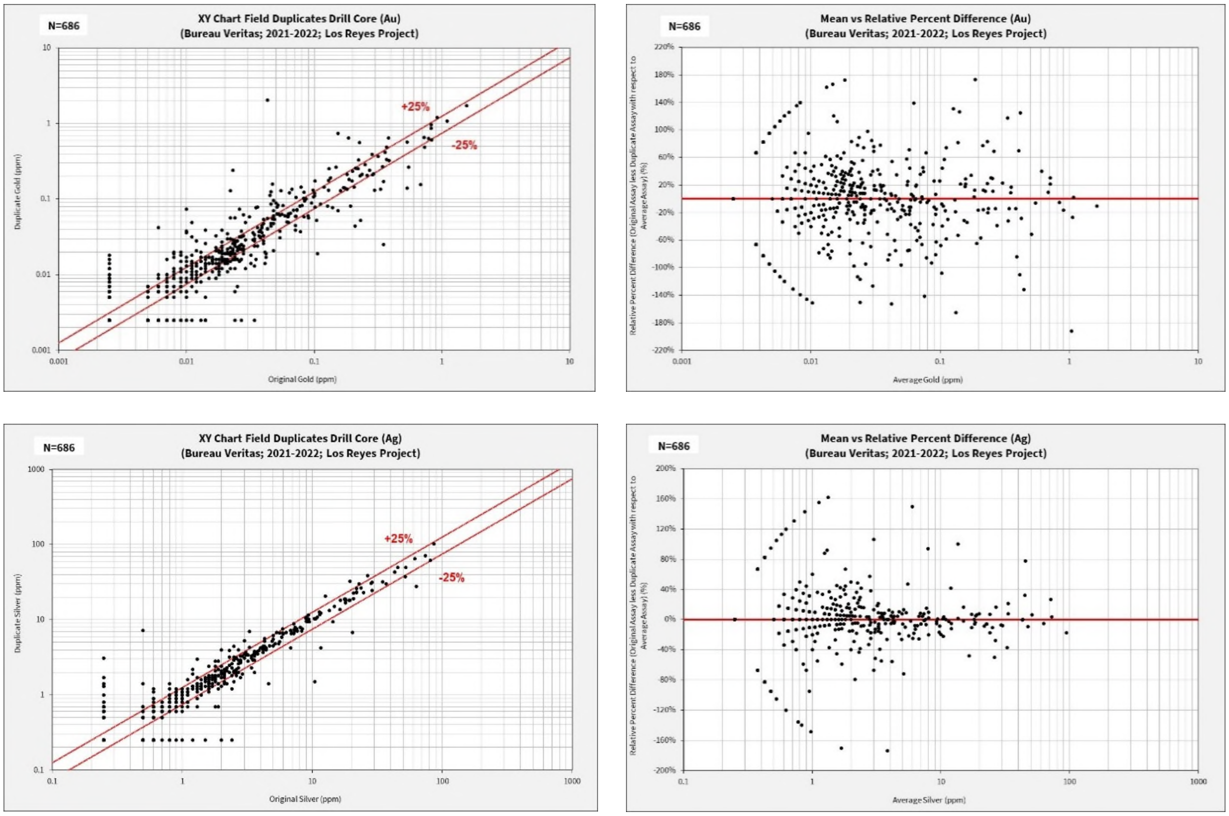
The field duplicates results received from BV consist of quarter core duplicates and reverse circulation duplicates. For reverse circulation, the duplicate is taken from the original sample split, one mineralized interval and one un-mineralized interval, they are selected after the hole is completed.

A total of 686 quarter core duplicates were collected and submitted for analyses. A total of 108 quarter core duplicates out of 686 reported above 0.05ppm gold. Forty-eight percent of the duplicate pairs are reporting within ±25% for gold and eighty-four percent for silver. This is considered acceptable for quarter core duplicates.

Table 11-10 Summary of Quarter Core Duplicate Results for Gold and Silver, Bureau Veritas

			% of Sample Pairs (>10x d.l.) Reporting within			
Analyte	***# of Pairs***	***# of Pairs above 10x d.l.***	***±5%***	***±10%***	***±20%***	***±50%***
Au - QCore	686	108	10%	18%	48%	73%
Ag - QCore	686	81	25%	59%	84%	95%

Figure 11-5 XY and RPD Chart for Gold and Silver in Quarter Core Duplicates, Bureau Veritas

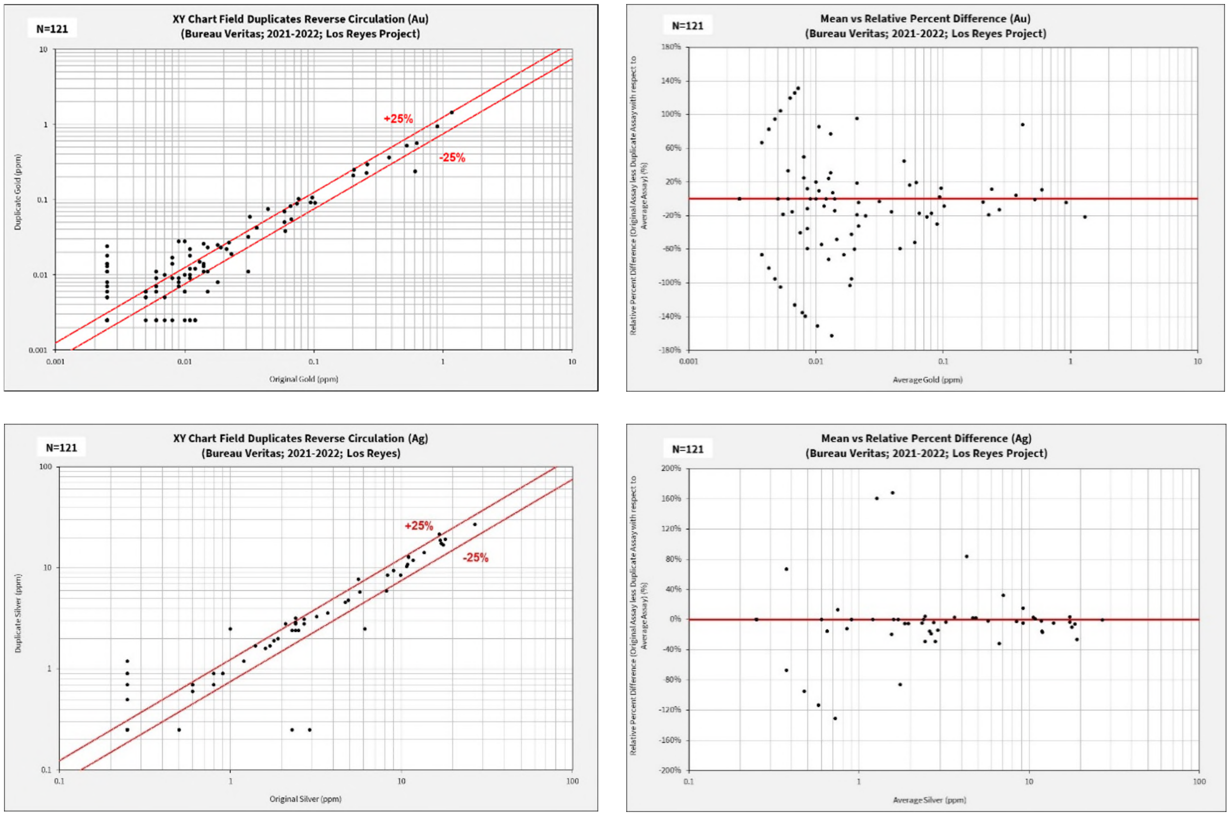


A total of 121 reverse circulation duplicates were collected and submitted for analyses. A total of twenty reverse circulation duplicates out of 121 reported above 0.05ppm gold. Eighty-five percent of the duplicate pairs are reporting within ±25% for gold and 74% for silver. This is considered acceptable for reserve circulation duplicates.

Table 11-11 Summary of Reverse Circulation Duplicate Results for Gold and Silver, Bureau Veritas

			% of Sample Pairs (>10x d.l.) Reporting within			
Analyte	***# of Pairs***	***# of Pairs above 10x d.l.***	***±5%***	***±10%***	***±20%***	***±50%***
Au - RC	121	20	25%	30%	85%	95%
Ag - RC	121	19	47%	53%	74%	84%

Figure 11-6 XY and RPD Chart for Gold and Silver in Reverse Circulation, Bureau Veritas



Preparation Duplicates

Preparation duplicates are created by splitting a second cut of the crushed sample in the same way and for the same weight as the original sample.

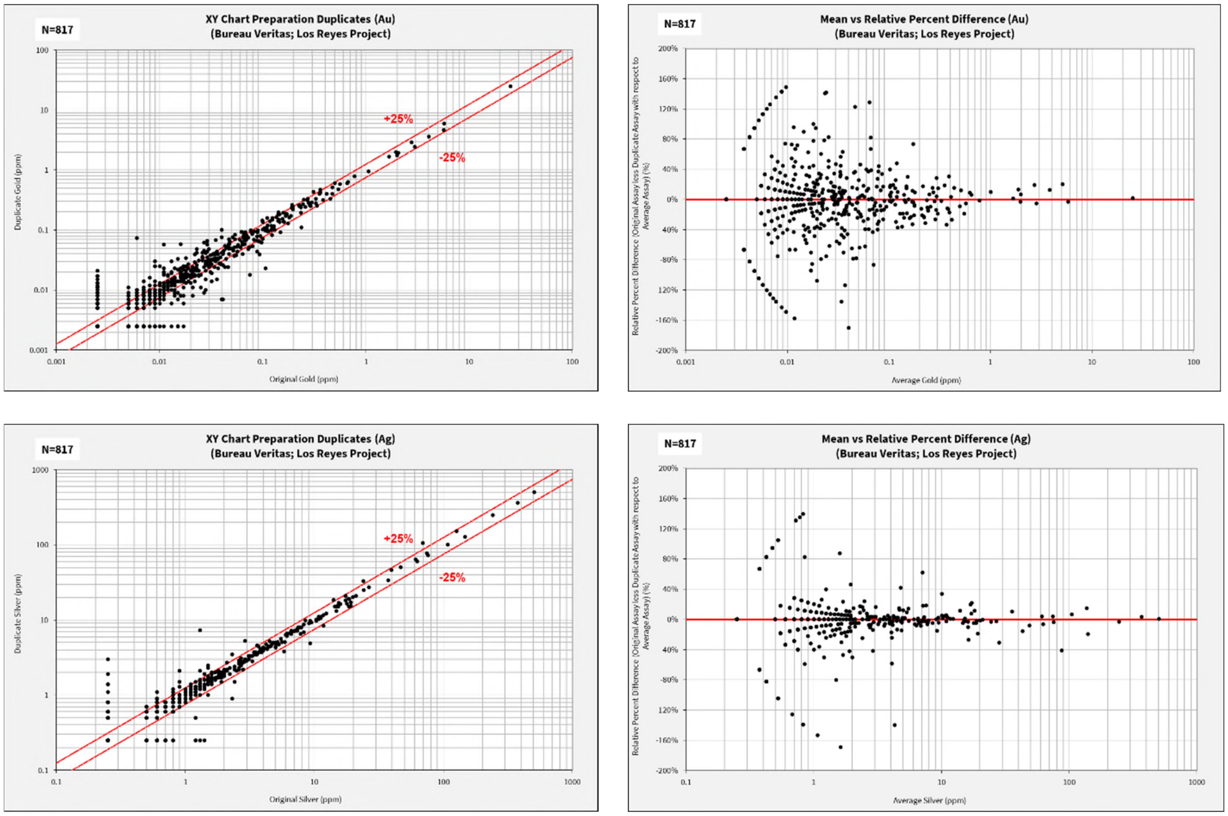
Prime select samples ending in ‘25’, or one sample in one hundred samples as a preparation duplicate. It is expected that the preparation duplicate pairs will be more similar than the quarter core duplicates due to the smaller particle size during sub-sampling.

A total of 817 preparation duplicates were analyzed for gold and silver. A total of 141 duplicate pairs out of 817 reported above 0.05ppm gold. The preparation duplicates for gold have 74% of the duplicate pairs reporting within ±25%. A total of 83 duplicate pairs out of 817 reported above 5ppm silver. The preparation duplicates for silver have 93% of the duplicate pairs reporting within ±25%. These results are considered acceptable.

Table 11-12 Summary of Preparation Duplicate Results for Gold and Silver, Bureau Veritas

			% of Sample Pairs (>10x d.l.) Reporting within			
Analyte	***# Pairs***	***# of Pairs above 10x d.l.***	***±5%***	***±10%***	***±25%***	***±50%***
Au	817	141	21%	36%	74%	96%
Ag	817	83	59%	72%	93%	99%

Figure 11-7 XY and RPD Chart for Gold and Silver in Preparation Duplicates, Bureau Veritas



Pulp Duplicates

A pulp duplicate is created by taking a second aliquot of the already pulverized sample material in the same way and for the same weight as the original sample. The assays for the pulp duplicate provide an estimate of the reproducibility related to the uncertainties inherent in the analytical method and the homogeneity of the pulp sample.

Prime selects every sample ending in '75', or one sample in one hundred samples to be analyzed in duplicate.

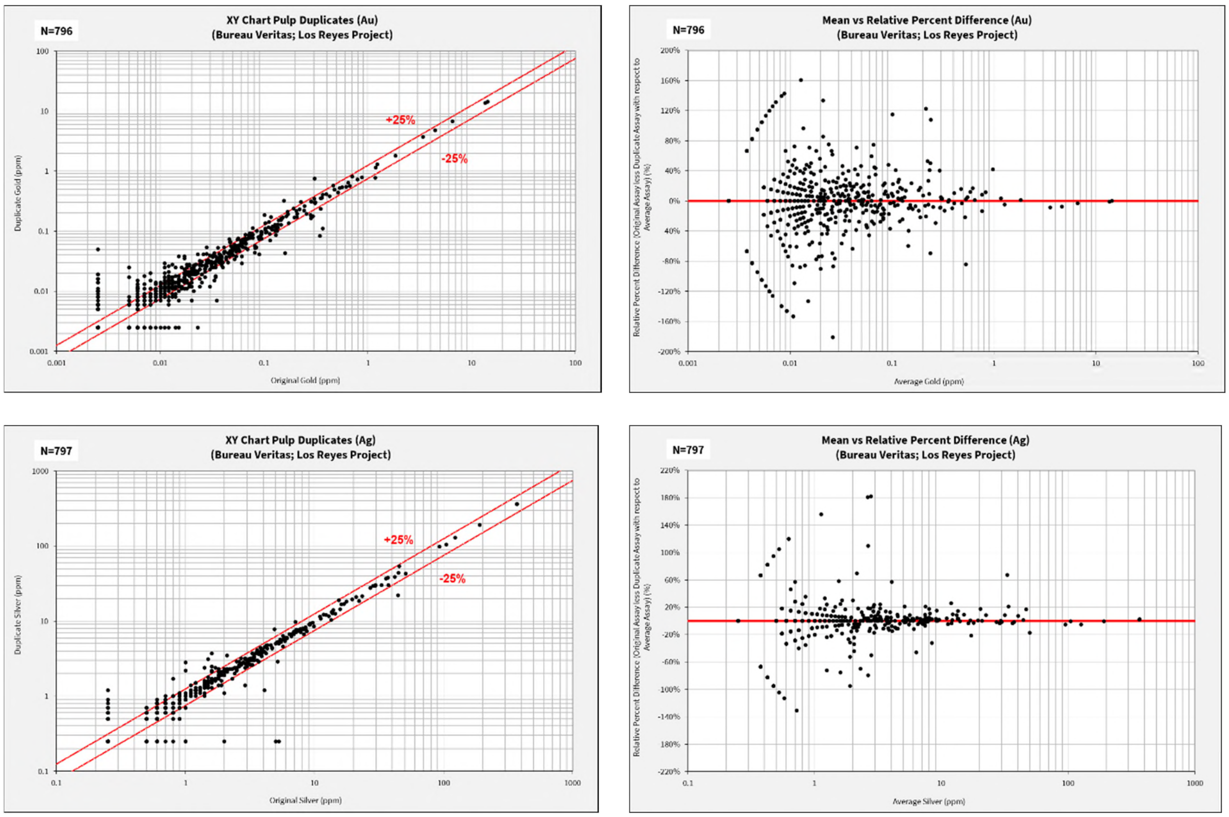
There are 796 pulp duplicate results for gold. A total of 139 duplicate pairs out of the 796 reported above 0.05ppm gold. The pulp duplicates for gold have 76 of the duplicate pairs reporting within ±25%. Precision for the gold pulp duplicates is acceptable.

There are 797 pulp duplicate results for silver. A total of 89 duplicate pairs out of the 797 reported above 5ppm silver. The pulp duplicates for silver have 93% of the duplicate pairs reporting within ±25%. Precision for the silver pulp duplicates is acceptable.

Table 11-13 Summary of Pulp Duplicate Results for Gold and Silver, Bureau Veritas

Analyte	# of Pairs	# of Pairs above 10x d.l.	% of Sample Pairs (>10x d.l.) Reporting within			
			±5%	±10%	±20%	±50%
Au	796	139	22%	45%	76%	92%
Ag	797	89	64%	80%	93%	96%

Figure 11-8 XY and RPD Chart for Gold and Silver in Pulp Duplicates, Bureau Veritas



Check Assays

BV vs SGS

A total of 654 pulps were selected from the samples analyzed at BV. The samples were submitted to SGS for check assaying. The methods from both laboratories are comparable.

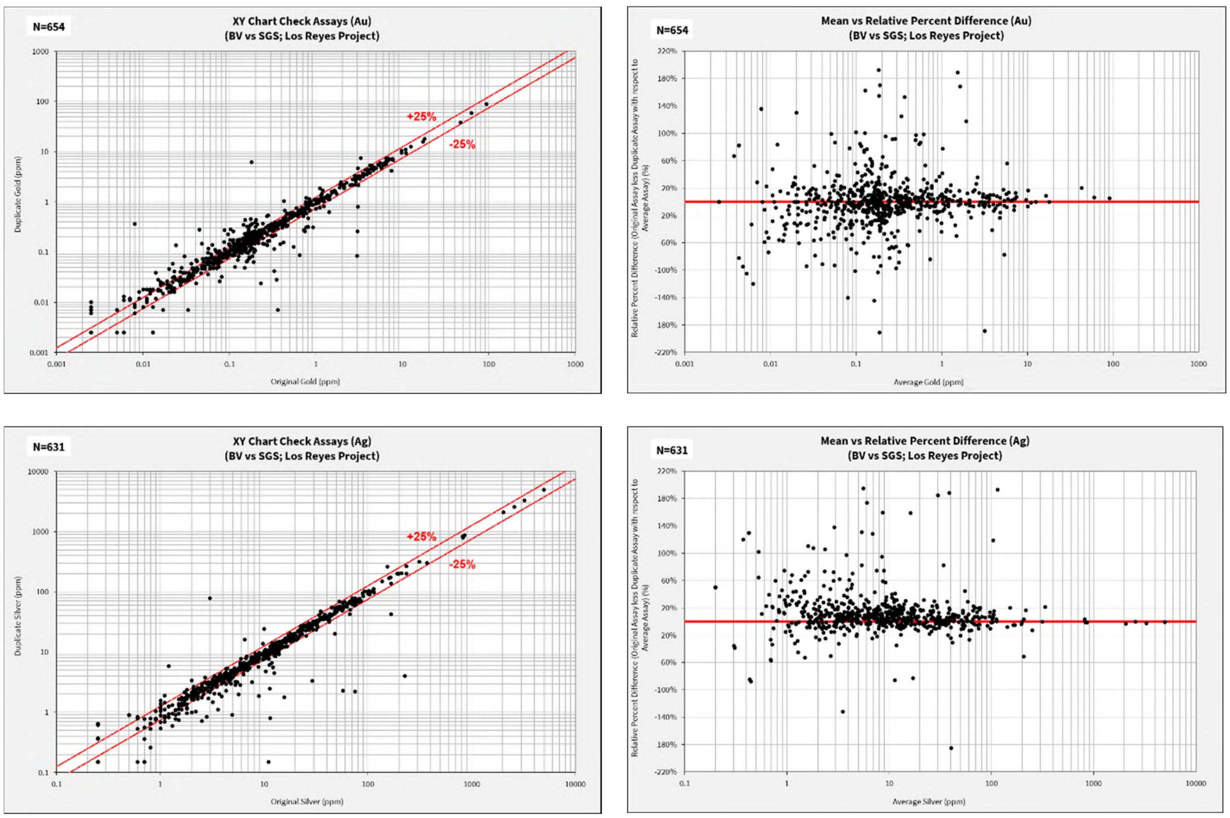
Seventy-three percent of the check assay results for gold are within ± 25% of the two sets of laboratory results; this is acceptable agreement. The pairs are evenly distributed with 49% being higher at BV and 49% being higher at SGS. The average RPD for gold between BV and SGS is 3%, this indicates that on average the BV results are higher than SGS results by about 3%. Based on the charts in Figure 11-9, the results are well distributed above and below zero percent relative difference.

For the silver results, 85% are within ± 25% of the two sets of laboratory results. The results tend to report higher at BV than at SGS. The results are mostly plotting above the zero relative percent difference for all grade ranges. The average difference between the two laboratories is 12%, with the results being higher at BV for seventy-seven percent of the case.

Table 11-14 Summary of Check Assay Results for Gold and Silver, BV vs SGS

				% of Sample Pairs (>10x d.l.) Reporting within			
Analyte	***# of Pairs***	***# of Pairs above 10x d.l.***	***Average RPD***	***±5%***	***±10%***	***±25%***	***±50%***
Au	654	542	3%	24%	46%	73%	88%
Ag	631	407	11%	33%	55%	87%	94%

Figure 11-9 XY and RPD Chart for Gold and Silver in Check Assays, BV vs SGS



BV vs ALS

A total of 152 pulps were selected from the samples analyzed at BV. The samples were submitted to ALS for check assaying. The methods from both laboratories are comparable.

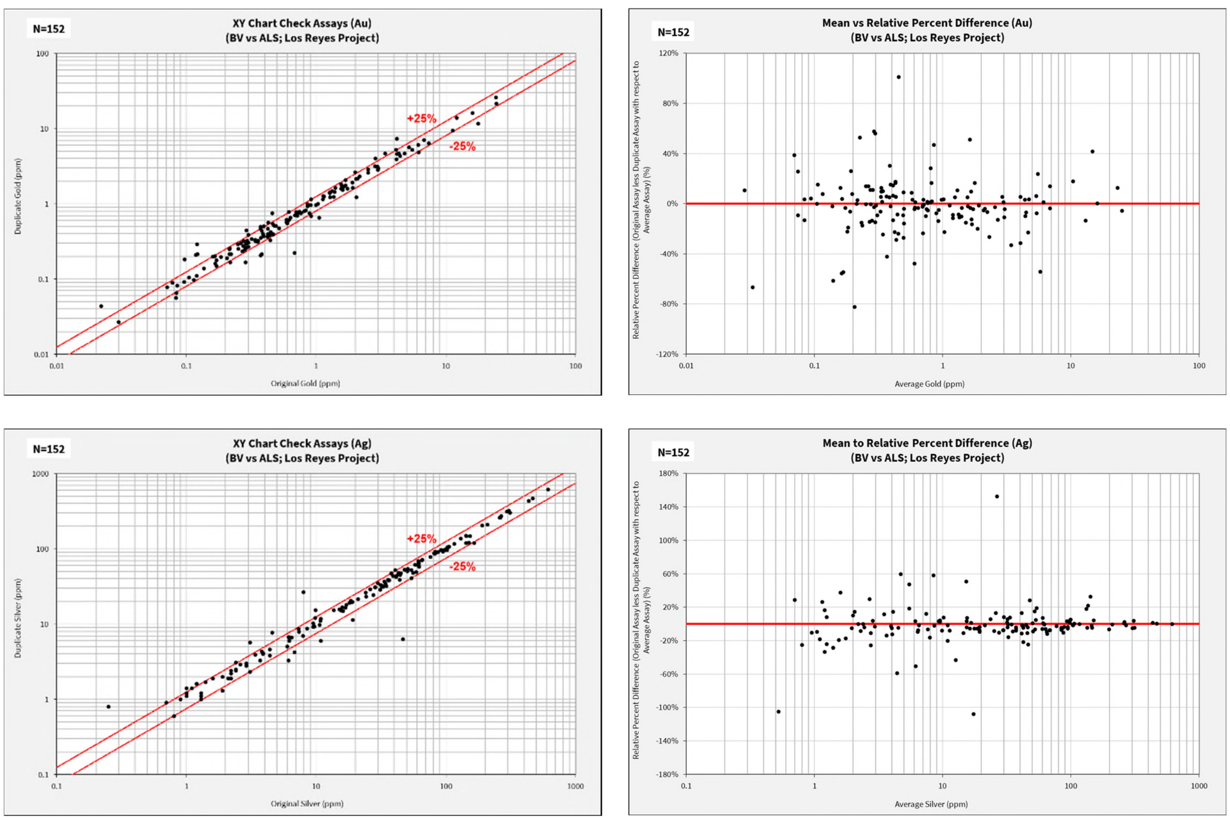
Eighty-four percent of the check assay results for gold are within ± 25% of the two sets of laboratory results; this is acceptable agreement. In fifty-five percent of cases ALS is higher than BV. The average RPD for gold between ALS and BV is -1%, this indicates that on average the ALS results are higher than BV results by about 1%. Based on the charts in Figure 11-10, the results are well distributed above and below zero percent relative difference.

For the silver results, 92% of the duplicate pairs are within ± 25%. In 63% of cases ALS is higher than BV. The average RPD for silver between ALS and BV is 0.5%, this indicates that on average the ALS results are lower than BV results by about 0.5%. The results are well distributed above and below the zero relative percent difference line for all grade ranges.

Table 11-15 Summary of Check Assay Results for Gold and Silver, BV vs ALS

				% of Sample Pairs (>10x d.l.) Reporting within			
Analyte	***# of Pairs***	***# of Pairs above 10x d.l.***	***Average RPD***	***±5%***	***±10%***	***±25%***	***±50%***
Au	654	542	3%	24%	46%	73%	88%
Ag	152	115	0.5%	43%	76%	92%	96%

Figure 11-10 XY and RPD Chart for Gold and Silver in Check Assays, BV vs ALS



12. DATA VERIFICATION

The following section summarizes the data verifications that were carried out and documented by the authors for this Technical Report, including verification of all drill data collected by Prime during their drill programs from December 2020 through to July 17, 2024.

12.1 Drill Hole Database Validation

Spot checks of the 2024 drill hole database (DHDB) revealed only minor errors which were flagged and rectified by the Company. Systematic spot-checking of collar information and assays to confirm the DHDB was suitable for ongoing use through the addition of incoming data was performed. The DHDB contained a total of 688 holes (Table 10-1). Not all of the 493 historical drill holes have complete collar, assay and drill log data.

12.2 Verification of Analytical Quality Control Data

Chantal Jolette from Qualitica Consulting Inc. analyzed the analytical quality control data produced by Prime from 2020 to 2024.

Prime provided the external analytical control data containing the assay results for the quality control samples. All data were provided in Microsoft Excel spreadsheets. Ms. Jolette aggregated the assay results of the external analytical control samples for further analysis.

Control samples were charted as follows to highlight their performance:

- Control charts for blank material
- Control charts for reference materials
- Scatter plot and RPD chart for field duplicates
- Scatter plot and RPD chart for preparation duplicates
- Scatter plot and RPD chart for pulp duplicates
- Scatter plot and RPD chart for check assays

The performance of the analytical control data is discussed in Section 11 – Sample Preparation, Analyses and Security.

In the opinion of the Independent Qualified Person, the sample preparation, security, and analytical procedures for all assay data are adequate to support the MRE.

12.3 Data and Spatial Validation

During the site investigation of the Property the Independent Qualified Person:

- Located drill collars from the previous and current field campaigns and validated coordinates from the database using a handheld Garmin GPS.
- Reviewed the down hole survey and collar locations spatially in Leapfrog software to ensure that drill collars were on topography and there were no unusual drill hole deviations.
- Reviewed drill logging and procedures to confirm the presence of hydrothermal alteration, banded chalcedonic quartz and heterolithic breccias in drill core.
- Validated the logged geology by visiting various outcrops in the field near drilled areas.
- Compared assays in the Access database against the lab assay certificates as part of the validation process.
- Tracked the logging and assay data from the source Access database to the resource modeling data held in Leapfrog software to ensure the data matched as part of the data transfer validation process.
- The 3D wireframes were reviewed spatially in Leapfrog software to validate them with respect to the logged geology and grade based domaining strategy.
- The exploratory data analysis was reviewed and included: target composite length, data isolation, hard vs. soft boundaries, grade capping, and variography.
- The resource estimation process was reviewed and included: block model set up, various estimation methods, interpolation run strategies, model validation, resource classification strategies, metal loss due to capping and grade restrictions, cut-off grade development, and Mineral Resource reporting.

12.4 Limitation to Data Validation by Qualified Person

Limitations to the validation that the Independent Qualified Person was able to complete are listed below:

- The Independent Qualified Person was not involved in the Property prior to 2022, and therefore cannot validate the field procedures used during drilling and sample collection prior to the involvement by Prime.
- Laboratory inspections were not completed by the Independent Qualified Person.
- The BGBG.MX law firm did not have access to all of the original tenure documents.

12.5 Opinion of the Independent Qualified Person

The Independent Qualified Person site inspection, which was conducted by John Sims, CPG., during November 11th to the 15th of 2022, satisfies the NI 43-101 criteria. It is the opinion of the

Independent Qualified Person that the field procedures and sampling protocols that were implemented by Prime are reasonable. Also, the quality of the laboratory testing completed during the various stages of the Project is reasonable. The Independent Qualified Person is confident that the samples and associated laboratory datasets that are used in this Technical Report are accurate.

Based on this review, Mr. Sims has no reason to question the validity of the exploration and/or drilling conducted and/or the results thereon. That is, the adequacy of the data used in this Technical Report is considered accurate in the Independent Qualified Person's opinion.

Mr. Sims reserves the right, but will not be obligated, to revise the Technical Report and conclusions if additional information becomes known to them after the effective date of this Technical Report.

13. MINERAL PROCESSING & METALLURGICAL TESTING

A significant amount of metallurgical testing has been conducted on samples from the main mineralized areas (Z-T [Zapote & Tahonitas], Central [San Miguel East, San Miguel West & Noche Buena] and Guadalupe [Guadalupe East & Guadalupe West]) of the Los Reyes Project by previous owners starting in 1997 including Tenoco (1997), Companía Minera Campanillas (1998), Vista Gold (2012) and most recently since 2020 by Prime. The tests have focused primarily on CIL and direct bottle roll tests with programs completed by Resource Development Inc. ("RDi", now Forte Analytical or "Forte") in 2012 and between 2021 and 2024 and KCA in 2024 with preliminary gravity and flotation test work also being performed by RDi/Forte during this period. A detailed review of available metallurgical test work was completed by KCA to determine preliminary conditions, reagent requirements and metal recoveries for the Project. Drill hole locations for the samples used in the RDi/Forte 2021 to 2023 work are presented in Figure 13-1 and drill hole locations used to obtain samples tested by KCA in 2024 are presented in Figure 13-2.

Limited column leach test data are available with only one program being completed by McClelland Laboratories Mexico ("MLM") in 1998 on samples from the Zapote deposit. Additional column leach tests are currently in progress at KCA.

Significant test work and results relevant to the Project are presented in the following sections.

Figure 13-1 Drillhole Locations for Metallurgical Test Samples, RDi 2021-2023 (Prime, 2024)

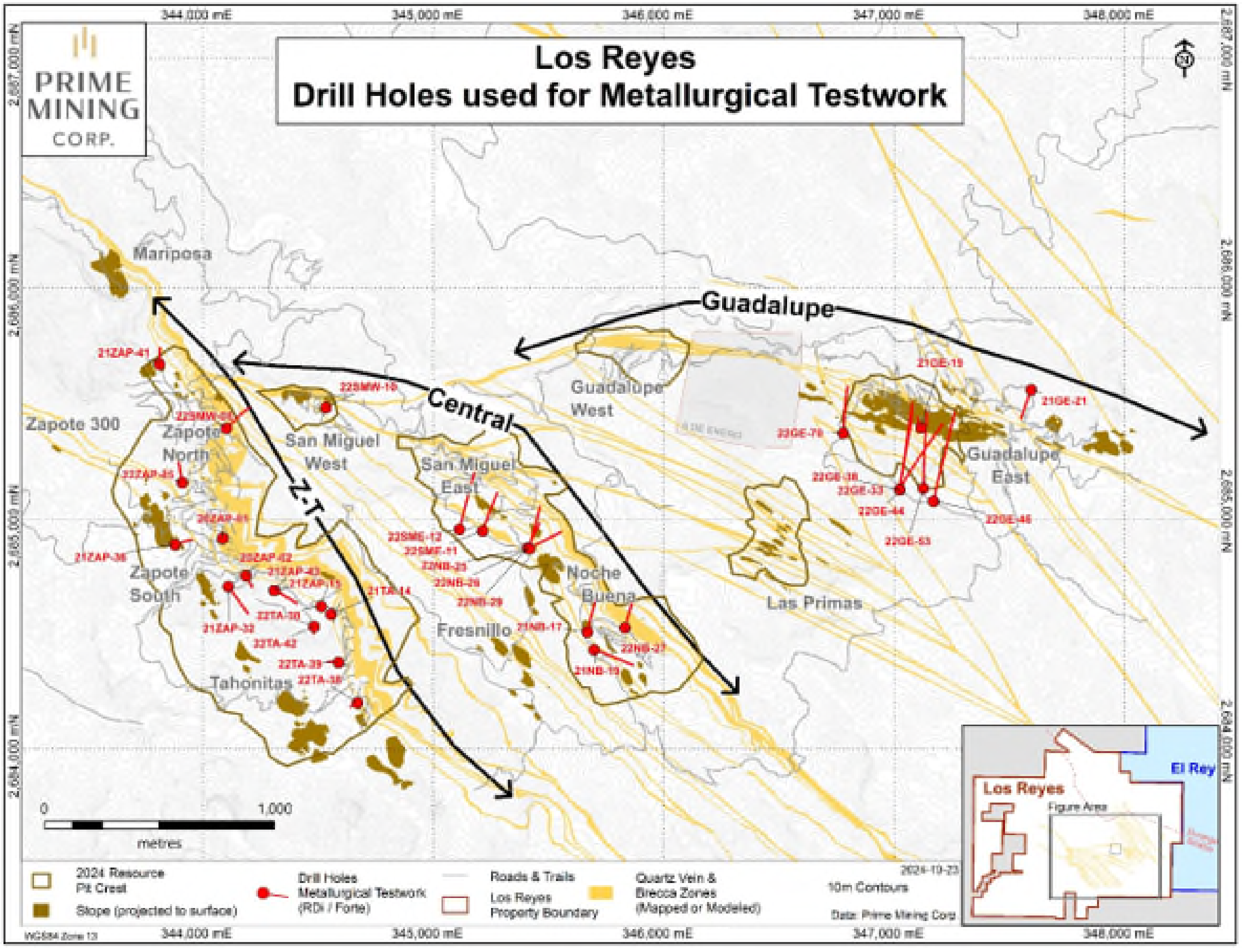
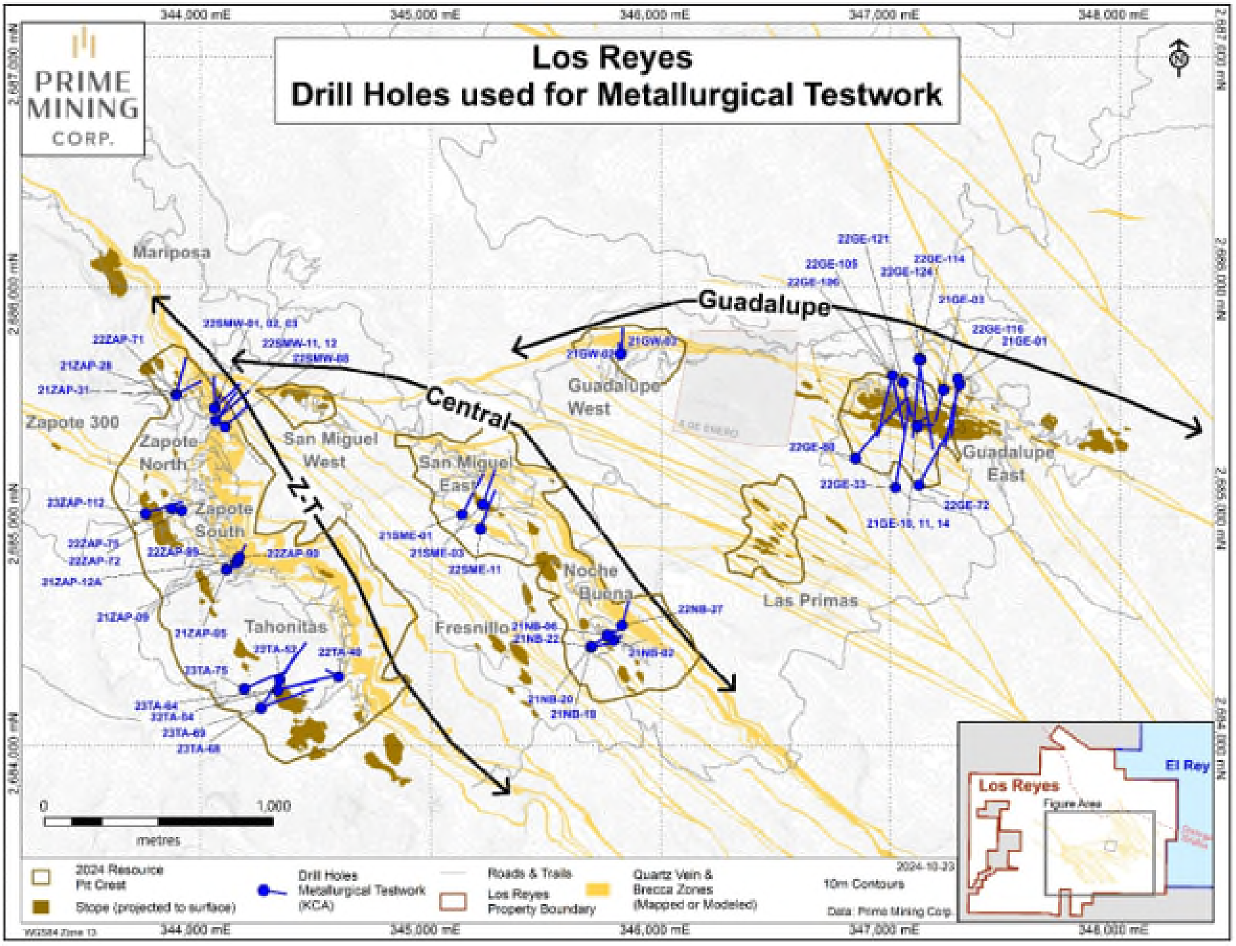


Figure 13-2 Drillhole Locations for Metallurgical Test Samples, KCA 2024 (Prime, 2024)



13.1 Metallurgical Test Work Results – Gravity Concentration Summary

13.1.1 *RDi/Forte Gravity Test Programs 2012, 2021-2023*

Gravity concentration testing was completed by RDi/Forte in 2012 and between 2021 and 2023. The 2012 program included two-stage gravity concentration (Knelson followed by Gemini Table) on nine composites generated from drill core rejects. The gravity concentration tests produced gold recoveries ranging between 11.8% and 32.8% and silver recoveries ranging between 1.7% and 24.3% with mass pulls ranging from trace amounts to 0.4% of the initial feed weight. Results from the 2012 RDi gravity program are presented in Table 13-1.

The 2021 to 2023 gravity concentration tests included single stage gravity concentration using a Knelson concentrator on eight composites from drill core rejects. Gemini table cleaning of the Knelson concentrate was also reported; however, no weights were presented and is therefore not considered. Gravity recoveries ranging between 4.3% and 51% for gold and 8% and 23% for silver with mass pulls ranging between 0.2% and 9.1% were achieved. For both the 2012 and 2021-

2023 test work the higher recoveries were closely associated with higher mass pulls. Results from the 2021-2023 RDi/Forte test work are presented in Table 13-2.

Additional details are available in the RDi technical report titled “Scoping Level Metallurgical Study for Guadalupe de Los Reyes Precious Metals Project, Sinaloa, Mexico” dated 24 September 2012 (the “RDi Report”) and the RDi/Forte Analytical Report titled “Prime Mining Corp. Los Reyes Scoping Metallurgical Test Program” dated 11 December 2023 (the “Forte Analytical Report”).

Table 13-1 2012 RDi Gravity Test Work Results

	Assay, g/t		Distribution %		
Product	**Au**	**Ag**	**Wt**	**Au**	**Ag**
Composite No. 1: P_{80} = 48 Mesh (T-1), GLW					
Gemini Conc.	119.5	6948.6	0.3	17.1	16.9
Gemini Tail	5.07	279.3	12.3	28.3	26.6
Cal. Knelson Conc.	7.92	445.9	12.6	45.4	43.5
Knelson Tail	1.37	83.3	87.4	54.6	56.5
Cal. Feed	2.19	128.9	100.0	100.0	100.0
Composite No. 1: P_{80} = 100 Mesh (T-2), GLW					
Gemini Conc.	160.4	8927.8	0.3	23.1	20.8
Gemini Tail	4.28	298.2	10.2	20.6	23.2
Cal. Knelson Conc.	8.82	549.2	10.5	43.7	44.0
Knelson Tail	1.34	82.2	89.5	56.3	56.0
Cal. Feed	2.13	131.4	100.0	100.0	100.0
Composite No. 2: P_{80} = 48 Mesh (T-3), GL Vein					
Gemini Conc.	123.7	5756.6	0.3	13.6	8.5
Gemini Tail	5.11	344.3	11.9	21.2	19.0
Cal. Knelson Conc.	8.19	484.7	12.2	34.8	27.5
Knelson Tail	2.13	177.7	87.8	65.2	72.5
Cal. Feed	2.87	215.2	100.0	100.0	100.0
Composite No. 2: P_{80} = 100 Mesh (T-4), GL Vein					
Gemini Conc.	125.5	6488.1	0.4	15.2	10.4
Gemini Tail	5.2	415.0	10.8	20.0	19.9
Cal. Knelson Conc.	9.39	610.7	11.1	35.2	30.2
Knelson Tail	2.16	176.1	88.9	64.8	69.8
Cal. Feed	2.96	224.4	100.0	100.0	100.0
Composite No. 3: P_{80} = 48 Mesh (T-5), Zapote					
Gemini Conc.	450.6	778.4	0.1	13.2	2.5
Gemini Tails	5.45	36.7	12.1	21.9	16.2
Cal. Knelson Conc.	8.67	42.1	12.2	35.1	18.7
Knelson Tails	2.23	25.4	87.8	64.9	81.3
Cal. Feed	3.02	27.4	100.0	100.0	100.0
Composite No. 3: P_{80} = 100 Mesh (T-6), Zapote					
Gemini Conc.	581.1	586.7	0.1	20.4	1.7
Gemini Tails	6.27	47.7	9.3	20.6	12.9
Cal. Knelson Conc.	12.37	53.4	9.4	41.0	14.6
Knelson Tails	1.85	32.6	90.6	59.0	85.4
Cal. Feed	2.84	34.6	100.0	100.0	100.0
Composite No. 5: P_{80} = 65 Mesh (T-7), NB					
Gemini Conc.	97.09	875.1	0.2	22.2	24.3
Gemini Tail	1.86	23.8	11.0	23.0	35.7
Cal. Knelson Conc.	3.59	39.3	11.2	45.2	60.0
Knelson Tail	0.55	3.3	88.8	54.8	40.0
Cal. Feed	0.89	7.3	100.0	100.0	100.0

Product	Assay, g/t		Distribution %		
	Au	Ag	Wt	Au	Ag
Composite No. 6: P_{80} = 65 Mesh (T-8), Zapote					
Gemini Conc.	1836.4	2154.4	Trace	15.4	1.7
Gemini Tail	7.20	47.5	11.3	16.8	10.7
Cal. Knelson Conc.	13.78	55.1	11.3	32.2	12.4
Knelson Tail	3.71	49.5	88.7	67.8	87.6
Cal. Feed	4.85	50.1	100.0	100.0	100.0
Composite No. 7: P_{80} = 65 Mesh (T-9), Zapote					
Gemini Conc.	1111.3	3371.2	Trace	11.8	3.1
Gemini Tail	4.58	56.8	10.8	17.8	18.9
Cal. Knelson Conc.	7.59	65.8	10.8	29.6	22.0
Knelson Tail	2.19	28.3	89.2	70.4	78.0
Cal. Feed	2.77	32.4	100.0	100.0	100.0
Composite No. 9: P_{80} = 100 Mesh (T-10), SM					
Gemini Conc.	5698.7	16544.9	0.1	32.8	8.3
Gemini Tail	23.25	212.2	11.6	25.5	20.2
Cal. Knelson Conc.	52.89	297.5	1.7	58.3	28.5
Knelson Tail	5.01	98.9	88.3	41.7	71.5
Cal. Feed	10.61	122.1	100.0	100.0	100.0

Table 13-2 2021-2023 RDi Gravity Test Work Results

Test # DH # Composite		GC 1 21GE-19 11936-	GC 2 22GE-38 22871-	GC 3 22GE-38 222871-	GC 4 22GE-38 222871-	GC 5 21TA-14 19851-	GC 6 21TA-14 19851-	GC 7 21TA-14 19851-	GC 8 22GE-70 50705-
Grind, p80	**Tyler**	100 mesh	48 mesh	65 mesh	100 mesh	48 mesh	65 mesh	100 mesh	Pre-Screened
	Micr-ons	150	300	212	150	300	212	150	48, 100, 325
Feed	**Wt., g**	4040	988	992	994	991	992	993	2348
	Wt.,	100	100	100	100	100	100	100	100
	Au g/t	1.71	1.01	0.79	0.64	0.39	0.38	0.40	0.80
	Ag g/t	55.0	26.7	28.0	22.0	31.2	49.6	52.7	31.6
Knelson Tail	**Wt., g**	4022.70	898.8	913.2	933.5	930.7	934.2	946.5	2342.9
	Wt.,	99.6	91.0	92.1	93.9	93.9	94.2	95.3	99.8
	Au g/t	1.17	0.55	0.53	0.34	0.31	0.31	0.30	0.77
	Ag g/t	51.9	23.2	23.8	18.0	26.2	45.0	47.3	31.1
Gravity Conc.	**Wt., g**	17.30	89.2	78.8	60.5	60.3	57.8	46.5	5.1
	Wt.,	0.4	9.0	7.9	6.1	6.1	5.8	4.7	0.2
	Au g/t	127.83	5.69	3.82	5.38	1.57	1.47	2.30	15.10
	Ag g/t	775.0	61.7	76.1	83.8	108.0	123.8	161.9	232.2
% Recovery	**Au**	32.3%	50.8%	38.4%	50.5%	24.9%	22.6%	27.3%	4.3%
	Ag	6.1%	20.9%	21.7%	23.0%	21.1%	14.5%	14.4%	1.7%

The results from the RDi gravity tests show significant variability for both recovery and mass pull.

13.1.2 *Forte Dynamics Gravity Test Program 2024*

Single stage Knelson concentrator tests with cyanide leaching of the gravity tails were performed as part of the 2024 Forte Dynamics test program. The gravity tests were conducted on 12 different composites samples left over from previous test programs. Gravity recoveries ranged from 30.8% to 74.4% for gold and 13% to 39% for silver with mass pulls ranging between 3.1% and 7.4%. Recoveries from the bottle roll leach tests on the gravity tails ranged between 77.1% and 97.4% for gold and 26.6% and 99.9% for silver with overall recoveries ranging from 89.5% to 99.9% for gold and 40.4% to 99.9% for silver. Results for the 2024 gravity test work are presented in Table 13-3 (gravity concentration), Table 13-4 (gravity tails leach) and Table 13-5 (gravity and leach combined).

Additional details are available in the Forte Analytical Report titled “Prime Mining Corp. Los Reyes Phase II Metallurgical Testing” dated 2 July 2024.

Table 13-3 2024 Forte Dynamics Gravity Concentration Results

Sample #	Test #	Gravity Concentrate Weight (g)	Mass Fraction in Concentrate	Gold Measured Head g/t	Gold Calculated Head (g/t)	Gravity Concentrate Grade Gold (g/t)	% Gold Extracted by Knelson	Initial Assayed Head Grade Silver (mg/kg)	Silver Calculated Head (g/t)	Gravity Concentrate Grade Silver (mg/kg)	% Silver Extracted by Knelson
2 - 21GE-21	PBR-18	34.8	0.035	0.28	0.27	3.76	49.5	BD	6.4	58	0.32
3 - 22GE-46	PBR-22	33.6	0.034	0.37	0.51	6.74	44.1	30	27.2	151	0.19
4 - 21GE-19	PBR-25	44.2	0.044	1.39	2.57	45	77.2	62	61.1	501	0.36
5 - 22GE-33	PBR-33	67.9	0.068	6.23	5.43	48.6	60.9	143	123.2	434	0.24
6 - 22GE-53	PBR-26	74.4	0.074	15	14.1	147	77.5	325	302.4	1577	0.39
7 - 22SME-12	PBR-23	34.1	0.034	0.33	0.72	18.5	87.9	BD	2.6	25	0.33
8 - 21ZAP-32	PBR-27	31.1	0.031	0.48	3.09	89.4	89.9	24	29.3	158	0.17
9 - 21ZAP-43	PBR-21	47.3	0.047	1.45	1.32	16.1	57.4	24	24.2	67	0.13
10 - 21ZAP-36	PBR-20	32.2	0.032	2.65	3.98	83.6	67.6	12	14.4	79	0.18
12 - 21GE-03	PBR-24	30.8	0.031	11.9	10.08	125	38.3	705	700.1	5172	0.23
13 - 22TA-39	PBR-19	38.4	0.038	0.39	0.42	2.83	25.9	54	52.6	270	0.2
14 - 22NB-27	PBR-34	31.5	0.032	4.72	4.47	47	33.5	102	96.2	516	0.17

Table 13-4 2024 Forte Dynamics Gravity Tails Leach Tests Results

Sample #	Test #	Gold Recovery in Leach %	Gold Calc. Leach Head Grade (g/t)	Residue Grade Gold (g/t)	Silver Recovery in Leach %	Silver Calc. Leach Head Grade (g/t)	Residue Grade Silver (g/t)	NaCN Consumption (kg/mt)	Lime Consumption (kg/mt)
2 - 21GE-21	PBR-18	79.2	0.14	0.03	77.8	4.5	BD	2.276	2.275
3 - 22GE-46	PBR-22	93.3	0.3	0.02	91.3	22.9	BD	1.66	2.36
4 - 21GE-19	PBR-25	95.1	0.61	0.03	97.5	40.7	BD	1.642	2.114
5 - 22GE-33	PBR-33	97.4	2.28	0.06	99.9	100.6	BD	2.035	1.076
6 - 22GE-53	PBR-26	97.37	3.4	0.09	92.5	200	15	2.032	1.924
7 - 22SME-12	PBR-23	77.1	0.09	0.02	83.4	1.81	BD	1.31	2.99
8 - 21ZAP-32	PBR-27	96.8	0.32	BD	28.4	25.1	18	1.19	1.948
9 - 21ZAP-43	PBR-21	93.2	0.59	0.04	45.8	22.1	12	1.239	2.718
10 - 21ZAP-36	PBR-20	97	1.33	0.04	26.6	12.3	9	1.85	2.09
12 - 21GE-03	PBR-24	96	6.43	0.26	86.9	558	73	1.888	4.44
13 - 22TA-39	PBR-19	90.7	0.32	0.03	65.8	43.9	15	1.275	2.093
14 - 22NB-27	PBR-34	97.4	3.09	0.08	97.6	82.5	BD	1.073	0.79

Notes:

Conditions: Grind (P80): 200 Mesh, PbNO3 (as defined below) 200 kg/t, Leach Time: 48 Hours

Table 13-5 2024 Forte Dynamics Combined Gravity & Leach Results

Sample #	Test #	Individual Gold Recovery %		Gravity plus Leach Au Recovery %	Individual Silver Recovery %		Gravity plus Leach Ag Recovery %
		Gravity	Leach		Gravity	Leach	
2 - 21GE-21	PBR-18	49.5	40	89.5	32	53	84.8
3 - 22GE-46	PBR-22	44.1	52.2	96.3	19	74	92.9
4 - 21GE-19	PBR-25	77.5	21.9	98.9	36	62	98.4
5 - 22GE-33	PBR-33	60.9	38.1	99	24	76	99.9
6 - 22GE-53	PBR-26	77.5	21.9	99.4	39	57	95.4
7 - 22SME-12	PBR-23	87.9	9.3	97.2	33	56	88.9
8 - 21ZAP-32	PBR-27	89.9	9.8	99.7	17	24	40.4
9 - 21ZAP-43	PBR-21	57.4	39.7	97.1	13	40	52.9
10 - 21ZAP-36	PBR-20	67.6	31.4	99	18	22	39.6
12 - 21GE-03	PBR-24	38.3	59.2	97.5	23	67	89.9
13 - 22TA-39	PBR-19	25.9	67.2	93.1	20	53	72.5
14 - 22NB-27	PBR-34	33.5	64.8	98.3	17	81	98

Notes:

Leach Recovery Calculated based on Gravity Test Calculated Heads. Bottle Roll Conditions: Grind (P80): 200 Mesh, PbNO3 200 kg/t, Leach Time: 48 Hours.

Although the gravity test results showed significant variability, the gravity tests combined with cyanide leaching of the tails showed consistently high overall recoveries. Further, when compared to the CIL bottle roll leach tests on the same samples presented in Table 13-23, the combined gravity and leach tests resulted in an average increased recovery of 1.6% for gold and 6.8% for silver. Additional gravity and leach testing is recommended for future test programs.

13.2 Metallurgical Test Work Results – Flotation

13.2.1 *RDi/Forte 2012, 2021-2023 Flotation Test Programs*

Preliminary rougher flotation testing was completed by RDi/Forte as part of test programs performed in 2012 and between 2021-2023. The 2012 flotation work was performed on three separate composites (two from Guadelupe West and one from Zapote) from drill core rejects at varying grind sizes and with different collectors. The 2021-2023 flotation tests were performed on two separate composites (one from Guadelupe East and one from Tahonitas) from drill core rejects at varying grind sizes. Results from the flotation test work are presented in Table 13-6 and Table 13-7 for the 2012 and 2021-2023 programs, respectively.

Additional details are available in the RDi Report and the Forte Analytical Report.

Table 13-6 2012 RDi Flotation Test Results

				Concentrate (9 min's)					Assay, g/t			
				Recovery %			Grade, g/t		Tailing		Cal. Feed	
Composite #	Composite Description	Grind P_{80} mesh	Reagents	Wt.	Au	Ag	Au	Ag	Au	Ag	Au	Ag
1	GLW	100	PAX, AP404	6.2	85.7	90.9	27.77	1909.72	0.31	12.7	2.02	131.2
1	GLW	200	PAX, AP404	9.3	91.5	95.7	21.03	1350.52	0.20	6.2	2.13	130.6
1	GLW	200	AP404, AP3477	15.0	90.8	99.4	12.95	800.15	0.23	<1.7	2.14	120.9
2	GL Vein	100	PAX, AP404	5.8	88.1	89.4	50.08	3393.50	0.42	24.8	3.30	220.2
2	GL Vein	200	PAX, AP404	11.8	89.6	88.2	23.81	1643.13	0.37	29.3	3.13	219.0
2	GL Vein	200	AP3477, AP404	7.3	88.4	94.4	41.34	2737.21	0.43	12.7	3.40	211.0
3	Zapote	100	PAX, AP404	4.6	77.7	15.4	50.42	130.06	0.70	34.6	3.00	39.0
3	Zapote	200	PAX, AP404	8.2	86.7	22.0	31.42	82.97	0.43	26.3	2.98	31.0
3	Zapote	200	AP3477, AP404	7.8	86.8	23.5	34.81	96.72	0.45	26.6	3.13	32.1

Table 13-7 2021-2023 RDi/Forte Flotation Test Results

Test #	Drill Hole	Sample #	Grind (P_{80})	Conc. Wt%	% Recovery (Au)	Conc. Grade (Au g/t)	Calc. Head Grade (Au g/t)	% Recovery (Ag)	Conc. Grade (Ag g/t)	Calc. Head Grade (Ag g/t)
FT1	22GE-38	22871-22910	100 mesh	5	93.3	13.2	0.7	86.4	437	25.1
FT2	22GE-38	22871-22910	150 mesh	7	93.5	9.54	0.72	89.5	361	28.4
FT3	22GE-38	22871-22910	200 mesh	17.6	95.3	4.7	0.87	93	155	29.4
FT4	21TA-14	19851-19864	100 mesh	12.3	84.2	1.91	0.28	64.4	238	45.3
FT5	21TA-14	19851-19864	150 mesh	12.5	84.3	1.88	0.28	70	240	42.6
FT6	21TA-14	19851-19864	200 mesh	12.4	85.4	2.07	0.3	85.4	206	39.7

The flotation testing shows generally good recoveries for gold and silver with moderate mass pulls for the Guadalupe material, with lower recoveries observed for the Zapote and Tahonitas material (KCA notes that the head grades for the test work completed in 2021-2023 are significantly lower than what would be typical for a flotation plant). Although the flotation work may be able to be optimized, it is noted that overall higher recoveries were achieved through cyanide leaching (see

Tables 13-20, 13-23 and 13-25). Flotation recoveries for gold and silver do not appear to be significantly influenced by the grind size between P80 0.15 mm (100 mesh) and 0.075 mm (200 mesh); however, mass pulls were generally higher at the finer particle sizes. A variant of collectors were tested and all produced similar results.

13.2.2 *Forte Analytical 2024 Flotation Test Program*

Rougher flotation tests were completed on five composite samples from drill core rejects (three samples from Guadalupe East, one sample from San Miguel and one sample from Zapote) as part of the 2024 Forte Analytical test program. The flotation tests were conducted at a grind size of 80% passing 0.075 mm (200 mesh) using reagents Potassium Amyl Xanthate (PAX), Aero Promoter 3477, Aero Promoter 404, MIBC and AeroFroth 65. The flotation tails were subjected to cyanide leaching in CIL bottle roll leach tests and the rougher concentrate were further processed using a Gemini Table. Results for the flotation and flotation concentrate gravity concentration tests are presented in Table 13-8 and flotation tails leach results are presented in Table 13-9.

Table 13-8 2024 Forte Analytical Flotation Test Results

Stage	Product wt (g)	Mass Distribution (%)	Cumulative Mass Distribution (%)	Gold (g/t)	Individual Gold Distribution (%)	Cumulative Gold Distribution (%)	Silver (g/t)	Individual Silver Distribution (%)	Cumulative Silver Distribution (%)
FT-1: Sample 2 - 21GE-21: 28172-28192									
Feed (analyzed)	1000			0.28			6		
Feed (calculated)	1001.3	100		0.46	100		12	100	
Ro Conc	65.2	6.5	6.8	13.4	91.9	96.5	326	68.8	74.1
Gem Conc	3.1	0.3	0.3	6.92	4.6	4.6	203	5.2	5.2
Gem Tail	62.1	6.2	6.5	6.5	87.3	91.9	123	63.6	68.8
Ro Tail	936.1	93.5	100	0.04	8.1	100	4	31.2	100
FT-2: Sample 3 - 22GE-46: 32712-32717									
Feed (analyzed)	1000			0.37			30		
Feed (calculated)	1001.5	100		0.7	100		30	100	
Ro Conc	56.2	5.6	5.9	20.4	39.2	45.4	1548	84.4	94.4
Gem Conc	2.7	0.3	0.3	16.1	6.2	6.2	1126	10	10
Gem Tail	53.5	5.3	5.6	4.32	33	39.2	422	74.4	84.4
Ro Tail	945.3	94.4	100	0.45	60.8	100	5	15.6	100
FT-3: Sample 4 - 21GE-19: 11936-11945									
Feed (analyzed)	1000			1.39			62		
Feed (calculated)	997.5	100		1.59	100		59	100	
Ro Conc	65.6	6.6	6.9	330.1	92.9	149.7	4280	88.9	106.1
Gem Conc	2.8	0.3	0.3	321	56.7	56.7	3607	17.2	17.2
Gem Tail	62.8	6.3	6.6	9.14	36.2	92.9	673	71.8	88.9
Ro Tail	931.9	93.4	100	0.12	7.1	100	7	11.1	100
FT-4: Sample 7 - 22SME-12: 47614-47622									
Feed (analyzed)	1000			0.33			3		
Feed (calculated)	1006.8	100		0.61	100		5	100.1	
Ro Conc	40.4	4	4.1	355.5	62.5	102.4	472	46.5	51.4
Gem Conc	0.7	0.1	0.1	352	39.9	39.9	416	5.4	5
Gem Tail	39.7	3.9	4	3.51	22.6	62.5	56	41.1	46.4
Ro Tail	966.4	96	100	0.24	37.5	100	3	53.6	100
FT-5: Sample 9 - 21ZAP-43: 31100-31114									
Feed (analyzed)	1000			1.45			24		
Feed (calculated)	1000	100		1.77	100		24	100	

Stage	Product wt (g)	Mass Distribution (%)	Cumulative Mass Distribution (%)	Gold (g/t)	Individual Gold Distribution (%)	Cumulative Gold Distribution (%)	Silver (g/t)	Individual Silver Distribution (%)	Cumulative Silver Distribution (%)
Ro Conc	50.4	5	5.1	473.4	50.1	71	790	29.3	31.5
Gem Conc	0.8	0.1	0.1	463	20.9	20.9	658	2.2	2.2
Gem Tail	49.6	5	5	10.4	29.2	50.1	132	27.1	29.3
Ro Tail	949.6	95	100	0.93	49.9	100	18	70.7	100

Notes:

Conditions: Grind (P80): 200 Mesh.

Table 13-9 2024 Forte Analytical Float Tail Leach Test Results

Sample #	Test #	Flot Tail/BR Gold Head Grade (g/t)	Calc. Head Grade Gold (g/t)	Residue Grade Gold (g/t)	% Gold Extraction	Flot Tail/BR Silver Head Grade (g/t)	Calc. Head Grade Silver (g/t)	Residue Grade Silver (g/t)	% Silver Extraction	NaCN Consumption (kg/mt)	Lime Consumption (kg/mt)
2 - 21GE-21	PBR-28	0.04	0.05	0.01	88.9	4	2.7	0.8	70.3	1.1302	2.042
3 - 22GE-46	PBR-29	0.45	0.07	0.01	92.9	5	5	1.2	75.9	0.832	2.382
4 - 21GE-19	PBR-32	0.12	0.14	0.03	77.9	7	13.1	6.8	48.1	1.258	1.272
7 - 22SME-12	PBR-30	0.24	0.04	0.01	76.7	3	1.7	1	41.3	1.072	1.45
9 - 21ZAP-43	PBR-31	0.93	0.25	0.04	83.9	18	22.9	15.8	30.9	1.134	0.796

The rougher flotation showed variable recoveries for gold and silver with gold recoveries ranging between 40% and 93% and silver recoveries ranging between 30% to 89% and mass pulls ranging between 4.0% and 6.5%. Recoveries for the flotation tails leach were generally good averaging 84% for gold and 53% for silver.

A 10 kg simulated complete flowsheet (gravity/flotation/leach) was also completed on one sample from Guadalupe East as part of the 2024 program with results presented in Table 13-10 through Table 13-13. Overall flowsheet recoveries were 95% for gold and 87.4% for silver.

Additional details are available in the Forte Analytical Report titled “Prime Mining Corp. Los Reyes Phase II Metallurgical Testing” dated 2 July 2024.

Table 13-10 2024 Forte 10 kg Test Series Gravity Concentration

	mass (g)	Gold Grade (g/t)	Silver Grade (g/t)
Gem conc	19.99	36	1564
Gemini Tail	51.88	5	198.4
Knelson Tail (calc)	9928.1	0.59	28

Table 13-11 2024 Forte 10 kg Test Series Gravity Tails Flotation

Stage	Product wt (g)	Mass Distribution (%)	Cumulative Mass Distribution (%)	Gold (g/t)	Individual Gold Distribution (%)	Cumulative Gold Distribution (%)	Silver (g/t)	Individual Silver Distribution (%)	Cumulative Silver Distribution (%)
Feed (analyzed)	9928.1			0.43			26		
Feed (calculated)	10000	100		0.59	100		20	100	
Flotation Conc	586.7	5.9	5.9	8.47	84.1	84.1	273	81	81
Ro Tail	9413.3	94.1	100	0.1	15.9	100	4	19	100

Table 13-12 2024 Forte 10 kg Test Series Flotation Tails Leach

Test #	Assayed Head Grade Gold (g/t)	Calc. Head Grade Gold (g/t)	Residue Grade Gold (g/t)	% Extraction (Gold)	Assayed Head Grade Silver (g/t)	Calc. Head Grade Silver (g/t)	Residue Grade Silver (g/t)	% Extraction (Silver)	NaCN Consumption (kg/mt)	Lime Consumption (kg/mt)
PBR-35b	0.1	0.16	0.02	87.4	7	25.7	20.6	19.7	1.777	1.102

Table 13-13 2024 Forte 10 kg Test Series Simulated Flowsheet Summary

Stage	% wt	Gold Grade g/t	% Gold Recovery Individual	% Gold Recovery Cumulative	Silver Grade g/t	% Silver Recovery Individual	% Silver Recovery Cumulative
Feed	100	0.75	100		23.91		
Knelson Conc	0.72	13.6	13		577.7	17.4	17.4
Gemini Conc	0.2	36	10	10	1564		
Gemini Tail	0.52	5	3		198.4		
Gravity Tail	99.28	0.65	87		19.9		
Flotation Conc	5.87	8.47	67	76	273	67	84.4
Flotation Tail (CN Leach Feed)	93.4	0.16	20		4		
CN Leach Soln			18	95			
Final Tail	93.4	0.02	3		20.6*	3	87.4

Flotation test results suggest that flotation is not the most effective processing method and additional optimization testing would be required to determine if flotation could be viable as a standalone processing option. Due to the favorable results from agitated cyanide leaching and cyanide leaching in combination with gravity concentration, it is unlikely that flotation will be a preferred processing option at this time.

13.3 Metallurgical Test Work Results – Cyanide Leaching

Cyanidation test work includes column leach tests and coarse and fine direct bottle roll leach tests completed by MLM in 1998 and various direct and CIL bottle leach tests by RDi/Forte in 2012 and 2021 to 2024 and KCA in 2024. The 2012 RDi program evaluated several variability parameters including grind size, cyanide concentration, pulp density, CIL vs. direct leaching, and leaching with or without lead nitrate. Additional variability CIL bottle roll tests were completed for the 2021-2023 RDi/Forte program at different grind sizes and with or without lead nitrate. The 2024 Forte test program included lead nitrate addition optimization testing and CIL bottle roll leach tests and the 2024 KCA program included variability direct bottle roll leach tests at varying grind sizes. Cyanidation leach tests and results are discussed in the following section.

13.3.1 *MLM Test Program 1998*

Column leaching test work was completed by MLM in 1998 on samples from the Zapote deposit classified as "Zapote Saddle", "Gaitan Footwall" and "Gaitan Stringer". The program evaluated crush sizes ranging between 6.3 mm (1/4") and 12.7 mm (1/2") and samples were leached for approximately 60 days. Results from the column tests are presented in Table 13-14.

Table 13-14 1998 MLM Column Leach Test Results

			Assay Head		% Recovery			
Sample	**P100 (mm)**	**Leach (days)**	**Au (g/t)**	**Ag (g/t)**	**Au**	**Ag**	**NaCN, kg/t**	**Lime, kg/t**
Zapote Saddle	12.7	67	3.31	16.8	64.56	14.28	1.45	1.0
Zapote Saddle	9.53	53	3.31	16.8	62.81	15.15	1.23	1.2
Zapote Saddle	6.35	53	3.31	16.8	71.61	17.50	1.17	1.1
Gaitan Footwall	12.7	67	2.80	18.1	85.76	17.14	1.25	1.0
Gaitan Footwall	9.53	67	2.80	18.1	83.88	18.64	1.37	0.9
Gaitan Footwall	6.35	47	2.80	18.1	91.08	19.50	1.34	1.0
Gaitan Footwall	6.35	67	2.80	18.1	83.93	19.84	1.34	1.0
Gaitan Stringer	12.7	60	1.73	27.6	83.74	26.88	1.24	1.3
Gaitan Stringer	9.53	60	1.73	27.6	81.52	29.86	1.19	1.2
Gaitan Stringer	6.35	53	1.73	27.6	94.31	35.01	1.31	1.2

The column tests showed modest to good recoveries for gold ranging between 63% and 94% with lower recoveries for silver ranging between 14% and 35% and moderate requirements for lime and cyanide, respectively. Gold and silver recoveries generally improved with finer crushing.

Corresponding coarse and fine direct bottle roll leach tests were also conducted with results presented in Table 13-15.

Table 13-15 1998 MLM Direct Bottle Roll Leach Test Results

Sample	Crush size, mm	% Recovery, Au	% Recovery, Ag	NaCN, kg/t	Lime, kg/t
A-Zapote Saddle	- 12.7	37.5	13.8	0.14	1.3
	- 2	59.6	25.2	0.14	1.5
	- 9.53	40.7	23.6	0.14	1.5
	- 6.35	47.6	16.8	0.23	1.4
C-Gaitan Footwall	- 12.7	57.5	12.6	0.07	1.2
	- 2	73	25.2	0.16	1.2
	- 9.53	59.6	13.1	0.16	1.2
	- 6.35	64.1	17.8	0.16	1.2
D-Gaitan Stringer	- 12.7	57.5	22.2	0.06	1.6
	- 2	72	35.7	0.09	1.8
	- 9.53	62.4	23.4	0.14	1.5
	- 6.35	65	29.4	0.22	1.5
Composite ZPF-01	- 2	60.5	25.3	0.23	2.1
Composite ZPF-02	- 2	64.2	27	0.29	2.7
Composite ZPF-03	- 2	58.2	21.8	0.3	2.6
Composite ZPF-04	- 2	47.5	22.9	0.4	2.2
Composite ZPF-05	- 2	57.5	20.1	0.15	2
Composite ZPF-06	- 2	60.5	23.5	0.22	1.9
Composite ZPF-07	- 2	43	12	0.16	1
Composite ZPF-08	- 2	75.4	27.4	0.37	1.4

Similar to the column leach tests, the bottle roll tests showed improved recoveries with finer crushing with notably lower recoveries and cyanide consumption as compared to the column leach tests at the same crush sizes. KCA believes this discrepancy is likely due to the bottle roll tests being limited to 24-hours.

Overall, the samples tested show that they are amenable to cyanide leaching and that gold recovery by heap leaching could be viable.

13.3.2 *RDi Test Program 2012*

Variability bottle roll leach tests were performed by RDi in 2012 on drill core reject samples from Guadelupe West, Guadelupe Vein Zone, and the Zapote deposits. Additional details are available in the RDi Report.

The variability program initially evaluated material grind size vs. recovery in order to determine the grind size to use for the remaining variability testing. Based on the results presented in Table 13-16, a grind size of 150 mesh was selected.

Table 13-16 2012 RDi Grind Size Variability Bottle Roll Leach Test Results

Test No.	Composite	Composite Description	Grind P_{80} mesh	Extraction % (48 hrs.)		Residue, g/t		Calculated Head, g/t		NaCN Consumption kg/t
				Au	Ag	Au	Ag	Au	Ag	
1	1	GLW	65	70.7	34.7	0.69	92.8	2.30	142.19	0.169
2	1	GLW	100	57.7	36.2	1.30	89.4	3.08	140.03	0.538
3	1	GLW	150	79.8	31.4	0.45	104.0	2.03	151.67	1.138
4	1	GLW	200	84.7	38.1	0.31	81.3	2.02	131.26	1.259
10	2	GL Vein Zone	65	87.0	48.4	0.41	106.4	3.13	206.12	0.597
11	2	GL Vein Zone	100	87.9	43.1	0.37	118.2	3.05	207.77	1.258
12	2	GL Vein Zone	150	89.3	44.3	0.34	116.0	3.16	208.17	1.380
13	2	GL Vein Zone	200	92.6	47.5	0.24	107.9	3.25	205.42	1.318
19	3	El Zapote	65	83.0	28.5	0.52	21.3	3.04	29.79	0.109
20	3	El Zapote	100	89.4	34.1	0.33	18.7	3.11	28.39	0.170
21	3	El Zapote	150	93.0	37.9	0.20	19.3	2.80	31.09	1.139
22	3	El Zapote	200	92.8	38.9	0.22	17.2	3.02	28.17	1.198

Additional parameters evaluated during the variability program included cyanide concentration, pulp density, and the effect of direct leaching vs. CIL leaching vs. CIL leaching with lead nitrate addition. Results from these tests are presented in Table 13-17 through Table 13-19, respectively.

Table 13-17 2012 RDi Variable Cyanide Concentration Bottle Roll Leach Test Results

Test No.	Composite	Composite Description	NaCN Concentration g/L	Extraction % (48 hrs.)		Residue, g/t		Calculated Head, g/t		NaCN Consumption, kg/t
				Au	Ag	Au	Ag	Au	Ag	
5	1	GLW	0.5	78.3	16.8	0.45	105.9	2.07	127.23	0.511
6	1	GLW	0.75	81.3	25.7	0.41	106.6	2.20	143.57	0.930
3	1	GLW	1.0	79.8	31.4	0.45	104.0	2.23	151.67	1.138
14	2	GL Vein Zone	0.5	78.6	26.4	0.69	147.6	3.22	200.61	0.631
15	2	GL Vein Zone	0.75	86.8	34.3	0.44	140.3	3.34	213.65	0.990
12	2	GL Vein Zone	1.0	89.3	44.3	0.34	116.0	3.16	208.17	1.380
23	3	El Zapote	0.5	88.8	47.2	0.35	11.5	3.08	21.77	0.480
24	3	El Zapote	0.75	92.4	38.3	0.24	16.5	3.19	26.74	0.993
21	3	El Zapote	1.0	93.0	37.9	0.20	19.3	2.80	31.09	1.139

Table 13-18 2012 RDi Variable Pulp Density Bottle Roll Leach Test Results

Test No.	Composite	Composite Description	Leach Pulp Density, % Solids	Extraction % (48 hrs.)		Residue, g/t		Calculated Head, g/t		NaCN Consumption, kg/t
				Au	Ag	Au	Ag	Au	Ag	
3	1	GLW	40	79.8	31.4	0.45	104.0	2.23	151.67	1.138
7	1	GLW	45	83.1	35.0	0.34	81.5	2.02	125.47	0.979
8	1	GLW	50	76.8	27.3	0.55	102.0	2.37	140.31	0.756
12	2	GL Vein Zone	40	89.3	44.3	0.34	116.0	3.16	208.17	1.380
16	2	GL Vein Zone	45	88.7	41.1	0.38	125.2	3.38	212.45	1.175
17	2	GL Vein Zone	50	92.0	39.6	0.23	117.6	2.93	194.54	0.960
21	3	El Zapote	40	93.0	37.9	0.20	19.3	2.80	31.09	1.139
25	3	El Zapote	45	92.1	41.9	0.29	14.9	3.00	25.63	1.029
26	3	El Zapote	50	89.4	38.6	0.33	17.9	308	29.14	0.839

Table 13-19 2012 RDi Direct vs. CIL vs. CIL with Lead Nitrate Bottle Roll Leach Test Results

Test No.	Composite	Composite Description	Process Parameters	Extraction % (48 hrs.)		Residue, g/t		Calculated Head, g/t		NaCN Consumption kg/t
				Au	Ag	Au	Ag	Au	Ag	
3	1	GLW	Leach	79.8	31.4	0.45	104.0	2.23	151.67	1.138
9	1	GLW	CIL	93.3	68.7	0.14	46.0	2.08	146.88	1.047
28	1	GLW	CIL/Lead Nitrate	96.8	87.3	0.06	15.0	1.84	117.98	0.566
12	2	GL Vein Zone	Leach	89.3	44.3	0.34	116.0	3.16	208.17	1.380
18	2	GL Vein Zone	CIL	96.0	68.5	0.13	64.7	3.32	205.58	1.640
29	2	GL Vein Zone	CIL/Lead Nitrate	97.1	89.2	0.09	22.7	3.06	210.12	0.749
21	3	El Zapote	Leach	93.0	37.9	0.20	19.3	2.80	31.09	1.139
27	3	El Zapote	CIL	95.4	38.9	0.14	18.2	3.00	29.79	1.287
30	3	El Zapote	CIL/Lead Nitrate	96.5	37.8	0.09	21.1	2.67	33.92	0.510
31	5	Noche Buena	Leach	88.4	72.0	0.07	6.2	0.62	22.17	1.440
32	5	Noche Buena	CIL	91.1	87.7	0.07	3.1	0.77	25.28	1.237
33	5	Noche Buena	CIL/Lead Nitrate	93.1	90.4	0.06	2.4	0.79	25.12	0.394
34	6	El Zapote	Leach	93.5	27.3	0.28	37.6	4.31	51.70	0.888
35	6	El Zapote	CIL	95.0	32.1	0.25	34.9	4.94	51.36	0.815
36	6	El Zapote	CIL/Lead Nitrate	96.3	31.3	0.18	35.7	4.89	51.79	0.517
37	7	El Zapote	Leach	94.2	34.1	0.15	28.7	2.60	43.58	1.020
38	7	El Zapote	CIL	95.8	39.9	0.12	28.0	2.90	46.60	0.755
39	7	El Zapote	CIL/Lead Nitrate	96.3	42.0	0.12	27.2	3.24	46.93	0.460
40	8	San Miguel	Leach	91.3	53.7	0.42	33.2	4.82	71.77	1.379
41	8	San Miguel	CIL	96.8	77.5	0.15	17.4	4.81	77.41	1.470
42	8	San Miguel	CIL/Lead Nitrate	98.9	87.0	0.05	9.0	4.22	69.15	0.695
43	9	San Miguel	Leach	84.9	46.3	2.12	68.3	14.07	127.07	1.197
44	9	San Miguel	CIL	97.1	76.7	0.47	31.9	16.22	136.80	0.986
45	9	San Miguel	CIL/Lead Nitrate	98.8	83.4	0.15	20.3	13.08	122.02	0.806

The following parameters were recommended by RDi to be used for future test programs based on the results from the initial variability testing:

- Grind size of 150 mesh or finer;
- Cyanide concentration of 1 g/L;
- Pulp density of 40% (very little effect on recovery between 40 and 50%); and
- CIL with lead nitrate addition.

It is noted that the recommendations were focused on gold recoveries only and additional variability testing for silver are recommended.

13.3.3 *RDi/Forte Analytical Test Program 2021-2023*

A total of 59 CIL bottle roll leach tests were conducted by RDi/Forte between 2021 and 2023 on drill hole composites from the Guadalupe East, Noche Buena, San Miguel East, San Miguel West, Zapote and Tahonitas deposits. The test work is an extension of the work completed in 2012 and tested different material grind sizes and lead nitrate additions. Results are presented in Table 13-20.

Additional details are available in the Forte Analytical Report.

Table 13-20 2021-2023 RDi/Forte CIL Bottle Roll Leach Test Results

Test	Dhole	Grind P80 mesh	Pb(NO3)2 Kg/t	Head, calc Au, g/t	Head, calc Ag, g/t	Cyanide, NaCN kg/t	Lime, CaOH2 kg/t	Tail assay Au, g/t	Tail assay Ag, g/t	Au% Extraction 48hr Au	Ag% Extraction 48hr Ag
BR1	21GE-19	325	0.20	1.62	64.34	1.379	5.326	0.01	1.80	99.1	97.2
BR2	21GE-19	200	0.20	0.97	30.00	1.195	3.183	0.02	1.20	98.4	96.0
BR3	21NB-17	325	0.20	1.26	12.04	1.018	3.488	0.01	0.60	99.0	95.0
BR4	21NB-19	325	0.20	0.24	14.03	1.007	3.747	0.02	0.40	93.8	97.1
BR5	21ZAP-01	325	0.20	0.16	13.68	0.834	3.564	0.01	8.60	96.8	37.1
BR6	22SME-11	325	0.20	2.57	144.15	0.917	6.484	0.03	17.40	98.9	87.9
BR7	21ZAP-02	325	0.20	0.89	29.50	1.022	3.600	0.04	13.80	95.5	53.2
BR8	22GE-38	400	0.20	0.78	28.53	1.062	4.115	0.01	1.60	98.2	94.4
BR9	22TA-30	400	0.20	0.36	20.18	0.891	3.720	0.02	2.20	94.4	89.1
BR10	22SME-12	400	0.20	0.38	3.95	0.832	4.149	0.01	1.10	98.2	72.2
BR11	22NB-26	400	0.20	0.64	74.87	0.880	5.090	0.02	7.60	97.3	89.8
BR12	22SMW-10	400	0.20	1.31	126.60	1.192	4.931	0.03	6.20	97.9	95.1
BR13	22SMW-10	6	none	0.27	3.62	0.509	6.532	0.11	2.00	96.8	38.1
BR14	22GE-38	200	0.20	0.98	30.10	0.837	3.976	0.01	1.60	98.6	94.7
BR15	22GE-38	270	0.20	0.74	28.42	1.194	3.979	0.02	1.70	97.2	94.0
BR16	21TA-14	6	none	0.86	39.80	0.864	3.587	0.63	19.30	23.6	48.9
BR17	21TA-14	400	0.20	0.41	44.70	1.191	3.564	0.04	4.90	90.8	89.0
BR18	21ZAP-43	6	none	0.95	22.10	0.361	3.567	0.36	17.60	52.7	24.4
BR19	21ZAP-43	400	0.20	0.96	24.40	1.019	3.499	0.04	10.60	96.0	56.5
BR20	21TA-14	200	0.20	0.39	39.90	1.007	3.197	0.05	7.10	87.4	82.3
BR21	21TA-14	270	0.20	0.46	33.60	1.240	3.010	0.04	3.70	91.0	89.1
BR22	21ZAP-36	400	0.20	2.11	11.10	1.178	3.073	0.03	7.90	98.6	29.2
BR23	21ZAP-36	6	none	2.13	12.40	0.530	3.339	0.65	10.90	51.2	24.9
BR24	22GE-70	400	0.20	0.80	19.30	1.257	2.979	0.02	0.20	97.1	99.2
BR25	21ZAP-32	6	none	0.32	47.20	0.265	3.275	0.09	32.30	66.5	5.8
BR26	21ZAP-32	400	0.20	0.31	34.20	0.961	3.465	0.03	26.60	93.6	22.0
BR27	21ZAP-32	6	none	1.01	38.20	0.380	3.333	0.64	35.60	30.6	6.7
BR28	21ZAP-32	400	0.20	0.66	35.80	1.069	3.242	0.03	25.30	97.0	29.2
BR29	22NB-27	400	0.20	1.41	33.90	1.970	3.477	0.03	10.20	98.6	70.0
BR30	21ZAP-41	400	0.20	0.32	3.10	0.898	6.523	0.02	1.20	93.7	61.7
BR31	21ZAP-41	6	none	0.26	7.00	0.383	6.120	0.07	6.10	67.2	12.6
BR32	22ZAP-85	400	0.20	0.93	12.00	0.960	6.778	0.02	6.30	97.8	48.0
BR33	22ZAP-85	400	0.20	0.40	13.80	0.898	7.233	0.02	10.00	95.1	27.5
BR34	22ZAP-85	400	0.20	0.24	9.00	0.963	6.335	0.01	5.40	95.9	39.3
BR35	22ZAP-85	400	0.20	1.23	10.40	0.902	6.743	0.03	3.80	97.6	63.6
BR36	22GE-33	400	0.20	1.27	31.90	1.086	5.518	0.03	2.80	97.6	91.3
BR37	22GE-33	400	0.20	1.02	35.00	1.441	5.727	0.04	1.50	96.1	95.6
BR38	22GE-33	400	0.20	4.98	118.80	1.202	6.377	0.04	3.40	99.2	97.1
BR39	22NB-25	400	0.20	0.32	24.70	1.375	4.141	0.03	1.50	90.6	93.8
BR40	22NB-25	6	0.20	0.50	0.90	0.504	3.532	0.02	0.30	72.0	136.2
BR41	22NB-29	400	0.20	0.28	19.70	1.364	6.363	0.02	5.50	92.8	72.1
BR42	22NB-29	400	0.20	0.31	66.80	1.017	4.193	0.02	2.70	96.7	96.0
BR43	22GE-44	400	0.20	0.20	14.00	1.966	2.972	0.02	0.30	90.2	97.8
BR44	22GE-44	400	0.20	0.18	9.30	2.376	3.415	0.02	0.25	94.5	98.4
BR45	22GE-46	400	0.20	0.57	40.70	1.613	4.122	0.02	0.25	96.5	99.6
BR46	22GE-46	400	0.20	0.20	13.50	1.551	4.632	0.02	1.70	90.1	87.7
BR47	22GE-33	6	0.20	0.22	7.80	0.406	3.924	0.02	3.70	34.3	60.7
BR48	22GE-33	400	0.20	2.19	153.50	1.023	4.142	0.14	2.10	99.1	98.7
BR49	22GE-53	400	0.20	0.84	30.50	1.196	4.155	0.02	0.25	97.6	99.5
BR50	22GE-53	400	0.20	0.44	29.90	2.200	8.126	0.02	1.90	95.5	93.5
BR51	22GE-53	400	0.20	23.78	451.20	1.791	4.749	0.07	48.50	99.7	89.3
BR54	21GE-21	6	0.20	0.30	5.40	0.328	3.508	0.09	2.60	71.8	65.8
BR55	22TA-38	6	0.20	0.15	39.40	0.444	3.345	0.02	2.40	62.9	60.0
BR56	22TA-38	6	0.20	0.08	21.00	0.563	3.257	0.03	10.70	65.0	61.5
BR57	22TA-38	400	0.20	0.31	53.80	1.320	5.104	0.02	6.60	96.8	87.7
BR58	22TA-38	6	0.20	0.19	39.70	0.623	3.374	0.06	19.60	79.2	51.8
BR59	22TA-38	270	0.20	11.23	24.30	1.082	4.883	0.02	1.60	99.9	93.6
BR60	22TA-38	6	0.20	0.13	37.00	0.564	4.137	0.03	24.20	68.4	36.5
BR61	22TA-38	270	0.20	0.15	39.40	1.023	4.685	0.02	13.60	93.4	65.5

Results from the program are largely consistent with previous results. Some of the samples showed improved recoveries with finer grinding to 0.037 mm (400 mesh) with silver recoveries benefiting more from the finer grinding. Overall incremental recovery improvements for gold on average were very minor between the 0.053 mm (270 mesh) and 0.037 mm (400 mesh) grind sizes.

Head grades for gold for the test work were generally low, with 44 of the 59 tests having a gold grade of less than 1 g/t and approximately half of the tests having a grade of less than 0.5 g/t. There does not appear to be a strong correlation between gold head grade and gold recovery; however, it is recommended that future test work be performed on more grade-representative material.

13.3.4 *Forte Analytical 2024 Test Program*

Cyanide leach tests were completed on drill core reject samples left over from previous test programs. In total, twelve samples were evaluated with head analyses for gold and silver presented in Table 13-21.

Table 13-21 2024 Forte Composite Sample Head Analyses

Sample Name	Gold g/t	Silver g/t
1 - 22GE-38: 22867-22913	0.578	21.837
2 - 21GE-21: 28172-28192	0.28	6.229
3 - 22GE-46: 32712-32717	0.369	30.283
4 - 21GE-19: 11936-11945	1.389	62.142
5 - 22GE-33: 22757-27764	6.232	142.951
6 - 22GE-53: 42728-42737	15.015	325.11
7 - 22SME-12: 47614-47622	0.334	2.513
8 - 21ZAP-32: 24206-24231	0.477	23.891
9 - 21ZAP-43: 31100-31114	1.451	24.203
9 - 21ZAP-43: 31100-31114 dup	1.136	27.219
10 - 21ZAP-36: 24719-24720	2.645	11.509
11 - 22SMW-10: 62101	7.065	478.287
12 - 21GE-03: 4338-4340	11.872	705.063
13 - 22TA-39: 45645-45666	0.387	54.18
14 - 22NB-27: 48773-48775	4.717	102.263

Notes:

The test results indicate the following:

- Gold assays for the 14 samples varied from 0.28 g/t Au to 15 g/t Au.
- Silver assays varied from 6.2 g/t Ag to 705 g/t Ag.

The cyanide leach testing was developed in two phases. The first phase of the test work evaluated different lead nitrate (“PbNO3”) additions ranging from 0 mg/kg to 500 mg/kg on a sample from Guadalupe East with results presented in Table 13-22. Samples were ground to 80% passing 200 mesh and leached for 48 hours with carbon added after 24 hours of leaching. The results showed the optimal lead nitrate addition at 200 mg/kg which was used for the second phase of testing.

The second phase of the leach test work included CIL bottle roll leach tests on each of the 12 composite samples. Each sample was ground to 80% passing 200 mesh and leached at 2 g/L NaCN and 200 mg/kg of lead nitrate. Results from the CIL bottle roll leach tests are presented in Table 13-23.

Additional details are available in the Forte Analytical Report titled "Prime Mining Corp. Los Reyes Phase II Metallurgical Testing" dated 2 July 2024.

Table 13-22 2024 Forte Lead Nitrate Optimization Test Results

Test #	PbNO3 Addition (mg/kg)	% Recovery Gold	Assayed Head Grade Au (g/t)	Calc. Head Grade Au (g/t)	Residue Grade Au (g/t)	% Recovery Silver	Assayed Head Grade Ag (g/t)	Calc. Head Grade Ag (g/t)	Residue Grade Ag (g/t)	NaCN Consumption (kg/t)	Lime Consumption (kg/t)
PBR-1	0	89.4	0.58	0.72	0.08	87.6	22	22	BD	1.376	2.026
PBR-2	100	94.1	0.58	0.68	0.04	88.9	22	24	BD	1.324	1.995
PBR-3	200	95.4	0.58	0.66	0.03	96.4	22	20	BD	1.165	3.284
PBR-4	500	95.3	0.58	0.64	0.03	96.2	22	21	BD	1.447	2.193

Table 13-23 2024 Forte Bottle Roll Leach Tests

Sample #	Test #	% Recovery Gold	Assayed Head Grade Au (g/t)	Calc. Head Grade Au (g/t)	Residue Grade Au (g/t)	% Recovery (Ag)	Assayed Head Grade Ag (g/t)	Calc. Head Grade Ag (g/t)	Residue Grade Ag (g/t)	NaCN Consumption (kg/t)	Lime Consumption (kg/t)
2 - 21GE-21	PBR-16	91.1	0.28	0.34	0.03	84.3	BD	<7	BD	1.662	2.524
3 - 22GE-46	PBR-15	92.4	0.37	0.39	0.03	96.1	30	25	BD	1.602	2.433
4 - 21GE-19	PBR-17	97.8	1.39	1.81	0.04	94.6	62	56	BD	1.482	2.347
5 - 22GE-33	PBR-12	98.6	6.23	6.32	0.09	95.2	143	125	BD	1.565	2.518
6 - 22GE-53	PBR-10	98.8	15	14.7	0.17	89.8	325	303	31	2.187	1.213
7 - 22SME-12	PBR-9	93.9	0.33	0.33	0.03	56.9	BD	<7	BD	1.168	2.862
8 - 21ZAP-32	PBR-13	95.3	0.48	0.64	0.03	28.4	24	24	17	1.121	1.72
9 - 21ZAP-43	PBR-14	95	1.45	1.19	0.06	47.1	24	23	12	1.298	1.917
10 - 21ZAP-36	PBR-11	98.9	2.65	5.24	0.06	38.7	12	16	10	1.659	1.224
11 - 22SMW-10	PBR-7	95.2	7.07	6.67	0.32	79.2	478	451	94	1.97	4.253
12 - 21GE-03	PBR-8	96.6	11.9	11.9	0.41	73.7	705	660	174	1.968	5.07
13 - 22TA-39	PBR-6	90.6	0.39	0.42	0.04	70.2	54	50	15	1.18	3.026
14 - 22NB-27	PBR-5	97.3	4.72	4.38	0.12	96.9	102	97	BD	1.878	5.141

Notes:

Conditions: Grind (P80): 200 Mesh, PbNO3 200 kg/t, Leach Time: 48 Hours.

The results from the CIL bottle roll leach tests were consistent with previous test work with high recoveries for gold, ranging from 90.6% to 98.9% and variable recoveries for silver ranging from 28.4% to 96.9%. Overall recoveries averaged 95.5% for gold and 73% for silver. NaCN consumption averaged 1.6 kg/t and lime averaged 2.8 kg/t.

13.3.5 *KCA Test Program 2024*

Variability bottle roll leach tests were completed by KCA in 2024 on 16 composite samples generated from drill core. Head assays for gold and silver for each composite sample are presented in Table 13-24.

Table 13-24 2024 KCA Composite Sample Head Analyses

KCA Sample No.	Description	Assay 1, Au g/t	Assay 2, Au g/t	Assay 3, Au g/t	Average Assay, Au g/t
99401 A	ZS_HG-VHG	7.200	6.994	7.543	7.246
99402 A	ZN_HG-VHG_2	5.091	5.006	5.331	5.143
99403 A	TA_HG-VHG	1.733	1.587	1.793	1.705
99404 A	NB_HG-VHG	1.226	1.519	1.402	1.382
99405 A	SME_HG-VHG	1.502	1.666	1.485	1.551
99406 A	ZN_HG-VHG_1	0.705	0.823	0.778	0.769
99407 A	ZN_LG-MG	0.511	0.614	0.513	0.546
99408 A	NB_LG-MG	0.207	0.165	0.182	0.185
99409 A	TA_LG-MG	0.233	0.216	0.233	0.227
99410 A	GE_HG-VHG_1	8.040	8.674	8.811	8.509
99411 A	GE_HG-VHG_2	5.074	5.623	5.554	5.417
99412 A	GE_HG-VHG_4	2.727	2.763	3.099	2.863
99413 A	GE_HG-VHG_3	1.783	2.013	2.349	2.048
99414 A	GE_LG-MG_2	0.394	0.274	0.326	0.331
99415 A	GW_LG-MG_1	0.497	0.511	0.521	0.510
99416 A	GE_LG-MG_1	0.415	0.387	0.415	0.406
KCA Sample No.	**Description**	**Assay 1, Ag g/t**	**Assay 2, Ag g/t**	**Assay 3, Ag g/t**	**Average Assay, Ag g/t**
99401	ZS_HG-VHG	59.34	58.01	57.22	58.19
99402	ZN_HG-VHG_2	24.99	25.82	25.70	25.50
99403	TA_HG-VHG	104.21	100.80	111.02	105.34
99404	NB_HG-VHG	59.01	72.31	79.30	70.21
99405	SME_HG-VHG	69.62	74.19	78.41	74.07
99406	ZN_HG-VHG_1	17.90	19.41	23.42	20.24
99407	ZN_LG-MG	14.30	15.60	15.50	15.13
99408	NB_LG-MG	5.11	6.00	6.00	5.70
99409	TA_LG-MG	19.82	19.20	17.01	18.67
99410	GE_HG-VHG_1	724.08	648.07	726.07	699.41
99411	GE_HG-VHG_2	176.11	158.81	160.01	164.98
99412	GE_HG-VHG_4	391.85	334.83	462.45	396.38
99413	GE_HG-VHG_3	79.20	58.59	48.00	61.93
99414	GE_LG-MG_2	20.40	17.59	21.81	19.93
99415	GW_LG-MG_1	19.41	18.99	18.79	19.06
99416	GE_LG-MG_1	30.41	18.62	26.61	25.21

Notes:

The detection limit for silver with FAAS finish is 0.5 g/t. For the purpose of calculation, a value of 1/2 the detection limit is utilized for assays less than the detection limit.

Direct bottle roll tests were conducted on each composite sample at varying material sizes ranging from 80% passing 1.7 mm to 80% passing 0.075 mm (200 mesh). Lead nitrate was added to each sample at 200 g/t based on results from the Forte Analytical lead nitrate optimization test work. Coarse bottle roll tests (0.3 mm and 1.7 mm) were leached for 96 hours to ensure the samples were completely leached vs. 24 hours for the milled samples. The goal of the variability test work was to confirm the material grind size requirements and to determine whether a direct agitated leach circuit would be viable instead of the CIL process. Results are presented in Table 13-25.

Table 13-25 2024 KCA Direct Bottle Roll Leach Tests Summary

KCA Sample No.	Description	Target p80 Size, mm	Calculated Head, Au g/t	Extracted, Au g/t	Au Extracted, %	Calculated Head, Ag g/t	Extracted, Ag g/t	Ag Extracted, %	Leach Time, hours	Consumption NaCN, kg/t	Addition $Ca(OH)_2$, kgt
99401 B	ZS_HG-VHG	1.70	7.163	4.192	59%	54.55	11.92	22%	96	0.11	0.50
99401 B	ZS_HG-VHG	0.300	6.879	5.960	87%	61.88	20.62	33%	96	0.03	0.75
99401 B	ZS_HG-VHG	0.150	6.069	5.715	94%	62.99	23.72	38%	24	0.07	0.50
99401 B	ZS_HG-VHG	0.106	6.344	6.115	96%	61.43	24.33	40%	24	0.15	0.50
99401 B	ZS_HG-VHG	0.075	6.781	6.630	98%	66.14	31.60	48%	24	0.23	0.50
99402 B	ZN_HG-VHG_2	1.70	5.261	3.614	69%	24.59	4.66	19%	96	0.11	1.25
99402 B	ZN_HG-VHG_2	0.300	5.208	4.676	90%	25.31	7.58	30%	96	0.12	1.00
99402 B	ZN_HG-VHG_2	0.150	4.554	4.155	91%	24.78	8.17	33%	24	0.07	1.00
99402 B	ZN_HG-VHG_2	0.106	4.681	4.508	96%	25.25	9.52	38%	24	0.31	0.75
99402 B	ZN_HG-VHG_2	0.075	5.088	4.958	97%	26.05	11.04	42%	24	0.53	0.75
99403 B	TA_HG-VHG	1.70	1.808	1.104	61%	113.41	39.87	35%	96	0.18	0.50
99403 B	TA_HG-VHG	0.300	1.926	1.743	91%	116.62	82.90	71%	96	0.26	0.75
99403 B	TA_HG-VHG	0.150	1.667	1.533	92%	113.03	69.69	62%	24	0.15	0.50
99403 B	TA_HG-VHG	0.106	1.620	1.534	95%	110.08	73.71	67%	24	0.38	0.50
99403 B	TA_HG-VHG	0.075	1.747	1.668	95%	118.65	78.21	66%	24	0.38	0.50
99404 B	NB_HG-VHG	1.70	1.240	0.888	72%	92.93	61.03	66%	96	0.49	0.50
99404 B	NB_HG-VHG	0.300	1.460	1.326	91%	92.64	77.46	84%	96	0.34	0.75
99404 B	NB_HG-VHG	0.150	1.224	1.118	91%	75.86	66.23	87%	24	0.22	0.50
99404 B	NB_HG-VHG	0.106	1.242	1.181	95%	69.91	60.27	86%	24	0.45	0.50
99404 B	NB_HG-VHG	0.075	1.284	1.225	95%	67.88	60.46	89%	24	0.38	0.50
99405 B	SME_HG-VHG	1.70	1.568	1.204	77%	89.74	41.54	46%	96	0.26	1.50
99405 B	SME_HG-VHG	0.300	1.977	1.823	92%	81.66	66.93	82%	96	0.27	1.50
99405 B	SME_HG-VHG	0.150	1.616	1.531	95%	83.16	60.16	72%	24	0.31	1.25
99405 B	SME_HG-VHG	0.106	1.637	1.579	96%	81.03	63.29	78%	24	0.38	1.25
99405 B	SME_HG-VHG	0.075	1.519	1.472	97%	93.09	71.07	76%	24	0.61	0.75
99406 B	ZN_HG-VHG_1	1.70	0.866	0.410	47%	19.05	2.65	14%	96	0.03	0.50
99406 B	ZN_HG-VHG_1	0.300	0.733	0.667	91%	25.07	4.74	19%	96	0.03	0.50
99406 B	ZN_HG-VHG_1	0.150	0.780	0.691	89%	20.59	6.37	31%	24	0.15	0.50
99406 B	ZN_HG-VHG_1	0.106	0.751	0.706	94%	20.01	6.95	35%	24	0.30	0.50
99406 B	ZN_HG-VHG_1	0.075	0.852	0.813	95%	20.70	8.44	41%	24	0.37	0.50
99407 B	ZN_LG-MG	1.70	0.575	0.335	58%	13.61	1.68	12%	96	0.34	1.75
99407 B	ZN_LG-MG	0.300	0.588	0.523	89%	16.45	3.51	21%	96	0.19	1.50
99407 B	ZN_LG-MG	0.150	0.543	0.491	91%	16.82	4.59	27%	24	0.30	1.00
99407 B	ZN_LG-MG	0.106	0.517	0.491	95%	17.15	5.35	31%	24	0.38	1.25
99407 B	ZN_LG-MG	0.075	0.570	0.537	94%	16.30	5.76	35%	24	0.76	0.75
99408 B	NB_LG-MG	1.70	0.231	0.174	75%	6.25	3.82	61%	96	0.26	0.75
99408 B	NB_LG-MG	0.300	0.274	0.252	92%	7.21	6.01	83%	96	0.11	0.75
99408 B	NB_LG-MG	0.150	0.250	0.215	86%	7.19	6.16	86%	24	0.07	0.75
99408 B	NB_LG-MG	0.106	0.195	0.183	94%	7.03	6.14	87%	24	0.30	0.50
99408 B	NB_LG-MG	0.075	0.181	0.168	93%	7.76	6.87	89%	24	0.38	0.50
99409 B	TA_LG-MG	1.70	0.269	0.175	65%	19.80	2.67	13%	96	0.03	0.50
99409 B	TA_LG-MG	0.300	0.294	0.254	86%	21.78	4.98	23%	96	0.03	0.75
99409 B	TA_LG-MG	0.150	0.232	0.200	86%	22.06	6.39	29%	24	0.15	0.50
99409 B	TA_LG-MG	0.106	0.240	0.214	90%	22.43	7.36	33%	24	0.22	0.50
99409 B	TA_LG-MG	0.075	0.259	0.245	95%	21.85	8.46	39%	24	0.38	0.50
99410 B	GE_HG-VHG_1	1.70	8.751	5.767	66%	692.74	374.44	54%	96	0.74	0.75
99410 B	GE_HG-VHG_1	0.300	7.760	6.788	87%	684.33	449.37	66%	96	0.86	0.75
99410 B	GE_HG-VHG_1	0.150	7.595	6.317	83%	669.12	241.74	36%	24	0.60	0.75
99410 B	GE_HG-VHG_1	0.106	7.611	6.651	87%	641.13	241.52	38%	24	1.13	0.75
99410 B	GE_HG-VHG_1	0.075	8.117	7.095	87%	710.68	318.62	45%	24	1.51	0.50
99411 B	GE_HG-VHG_2	1.70	5.725	3.854	67%	221.11	138.71	63%	96	0.26	0.50
99411 B	GE_HG-VHG_2	0.300	5.146	4.705	91%	198.17	156.17	79%	96	0.42	0.50
99411 B	GE_HG-VHG_2	0.150	4.450	3.862	87%	176.95	111.01	63%	24	0.30	0.50
99411 B	GE_HG-VHG_2	0.106	5.079	4.815	95%	185.81	121.64	65%	24	0.53	0.50
99411 B	GE_HG-VHG_2	0.075	5.278	5.118	97%	204.37	139.73	68%	24	0.68	0.50
99412 B	GE_HG-VHG_4	1.70	2.537	1.915	76%	395.33	214.67	54%	96	0.49	0.50
99412 B	GE_HG-VHG_4	0.300	2.800	2.674	96%	419.47	305.13	73%	96	0.64	0.50
99412 B	GE_HG-VHG_4	0.150	2.583	2.447	95%	389.72	180.44	46%	24	0.45	0.50
99412 B	GE_HG-VHG_4	0.106	2.654	2.548	96%	368.85	165.50	45%	24	0.75	0.50
99412 B	GE_HG-VHG_4	0.075	2.787	2.709	97%	390.08	213.70	55%	24	0.98	0.50
99413 B	GE_HG-VHG_3	1.70	1.980	1.313	66%	67.36	44.62	66%	96	0.19	0.50
99413 B	GE_HG-VHG_3	0.300	2.023	1.851	92%	71.71	60.98	85%	96	0.19	0.50
99413 B	GE_HG-VHG_3	0.150	1.979	1.788	90%	68.57	53.46	78%	24	0.15	0.50
99413 B	GE_HG-VHG_3	0.106	2.036	1.955	96%	65.98	54.78	83%	24	0.37	0.50
99413 B	GE_HG-VHG_3	0.075	2.098	2.040	97%	71.90	56.24	78%	24	0.30	0.50
99414 B	GE_LG-MG_2	1.70	0.328	0.252	77%	21.17	12.98	61%	96	0.19	0.50
99414 B	GE_LG-MG_2	0.300	0.435	0.409	94%	24.86	21.72	87%	96	0.26	0.50
99414 B	GE_LG-MG_2	0.150	0.373	0.334	90%	23.53	19.69	84%	24	0.30	0.50
99414 B	GE_LG-MG_2	0.106	0.364	0.333	92%	22.24	18.89	85%	24	0.75	0.50
99414 B	GE_LG-MG_2	0.075	0.439	0.408	93%	24.09	21.15	88%	24	0.83	0.50

KCA Sample No.	Description	Target p80 Size, mm	Calculated Head, Au g/t	Extracted, Au g/t	Au Extracted, %	Calculated Head, Ag g/t	Extracted, Ag g/t	Ag Extracted, %	Leach Time, hours	Consumption NaCN, kg/t	Addition $Ca(OH)_2$, kgt
99415 B	GW_LG-MG_1	1.70	0.462	0.254	55%	18.40	8.98	49%	96	0.46	1.50
99415 B	GW_LG-MG_1	0.300	0.519	0.461	89%	19.59	12.92	66%	96	0.27	1.50
99415 B	GW_LG-MG_1	0.150	0.509	0.444	87%	18.91	12.85	68%	24	0.31	1.25
99415 B	GW_LG-MG_1	0.106	0.510	0.475	93%	19.29	12.87	67%	24	0.38	1.25
99415 B	GW_LG-MG_1	0.075	0.523	0.491	94%	20.21	14.54	72%	24	0.53	0.75
99416 B	GE_LG-MG_1	1.70	0.400	0.253	63%	21.16	12.52	59%	96	0.14	0.50
99416 B	GE_LG-MG_1	0.300	0.447	0.395	88%	23.79	20.06	84%	96	0.26	0.50
99416 B	GE_LG-MG_1	0.150	0.401	0.366	91%	22.71	18.88	83%	24	0.30	0.50
99416 B	GE_LG-MG_1	0.106	0.379	0.350	92%	21.37	17.83	83%	24	0.53	0.50
99416 B	GE_LG-MG_1	0.075	0.377	0.350	93%	24.47	21.32	87%	24	0.68	0.50

The bottle roll tests showed that recoveries for gold and silver were strongly dependent on grind size, as shown in Figure 13-3 for gold and Figure 13-4 for silver.

Figure 13-3 KCA 2024 Particle Size vs. Recovery, Gold

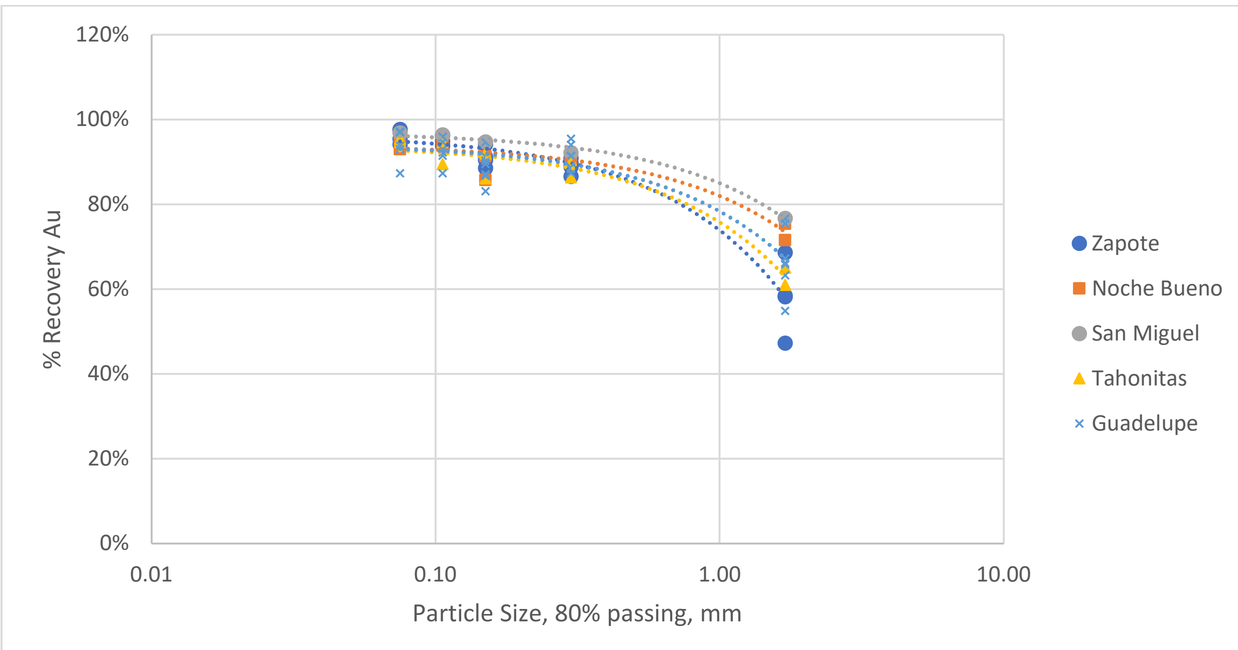
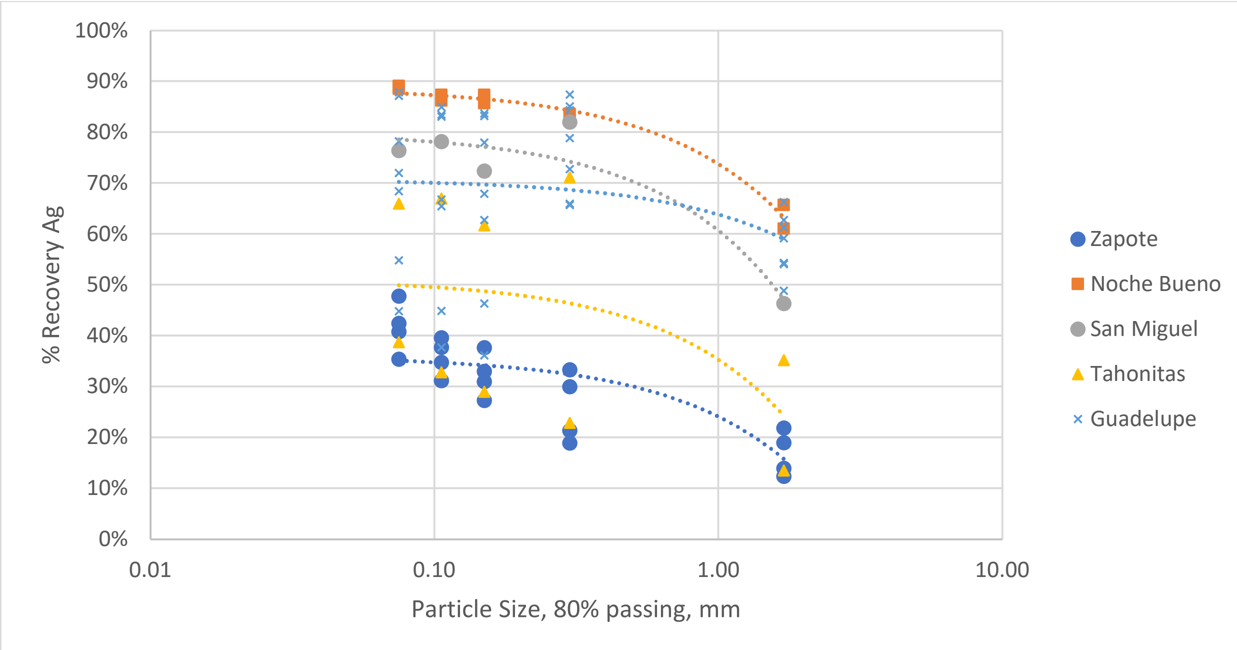


Figure 13-4 KCA 2024 Particle Size vs. Recovery, Silver



Gold recoveries at 80% passing 150 and 200 mesh for all material types were generally high ranging from 87% to 98% with an overall average of 94%. Silver recoveries varied significantly by material type ranging from 31% to 89% with an overall average of 62%. The results indicate that direct leaching is viable achieving similar recoveries compared to CIL bottle roll leach tests from previous test work programs, with the exception of silver recoveries for the Tahonitas samples which were significantly lower than previous work.

13.4 Metallurgical Test Work Results and Conclusions

Based on the metallurgical test work results, KCA recommends the following design parameters, which are discussed in the following sections:

- Heap Parameters:
  - Three-stage crushing to 80% passing 6.3 mm for heap leach material
  - 90-day leach cycle
  - Average gold recovery of 73% and silver recovery of 25%
  - Cyanide Consumption of 0.19 kg/t and lime addition of 1.1 kg/t
- Mill Parameters:
  - Target grind size of 80% passing 0.037 mm (400 mesh)
  - Gravity concentration with agitated leach on gravity tails
  - Overall mill recoveries and reagent requirements as per Table 13-26 (overall weighted average recovery of 95.6% for gold and 81% for silver)

Table 13-26 Agitated Leach Recovery and Reagent Requirements by Deposit

	Agitated Leach			
	% Au	% Ag	NaCN, Kg/t	CaO, kg/t
Zapote	96%	42%	0.5	2.2
Tahonitas	94%	89%	0.6	2.1
San Miguel	98%	84%	0.7	2.9
Noche Buena	95%	91%	0.7	2.1
Guadalupe W	89%	55%	0.7	1.9
Guadalupe E	96%	96%	0.9	1.9

In general, the various deposits at the Property show amenability to cyanide leaching for the recovery of gold and silver values, with improved recoveries with fine crushing/grinding. Although most of the test work has been conducted on CIL bottle roll leach tests, high recoverable silver values make use of a carbon circuit impractical and a direct agitated leach plant with Merrill-Crowe plant for recovery is recommended – results from the 2024 KCA test program indicate similar recoveries can be achieved by direct leaching of the material.

The potential for preg-robbing has been suggested as part of previous test campaigns; however, at this time this is considered to be anecdotal with no conclusive evidence of preg robbing. Levels of known preg robbing constituents, such as organic carbon and some swelling clays, are low. Preg-robbing tests with spiked and non-spiked tests should be considered in future programs to test the preg-robbing potential of the various material types.

13.4.1 *Gold and Silver Recoveries vs. Material Size*

In order to determine the recommended heap and agitated leach material product size and resulting recoveries, the recoveries by product size were analyzed. Heap leach recovery curves for gold and silver are presented in Figure 13-5 and Figure 13-6, respectively. Agitated leach recovery curves for gold and silver are presented in Figure 13-7 and Figure 13-8, respectively.

Recoveries were also evaluated by head grade at different grind sizes. At grind sizes of 150 mesh and finer, there did not appear to be any appreciable correlation between head grade and final recovery for gold. Silver recoveries by head grade varied somewhat by deposit but were generally unaffected or slightly improved with increasing silver grade.

Figure 13-5 Heap Gold Recovery vs. Crush Size

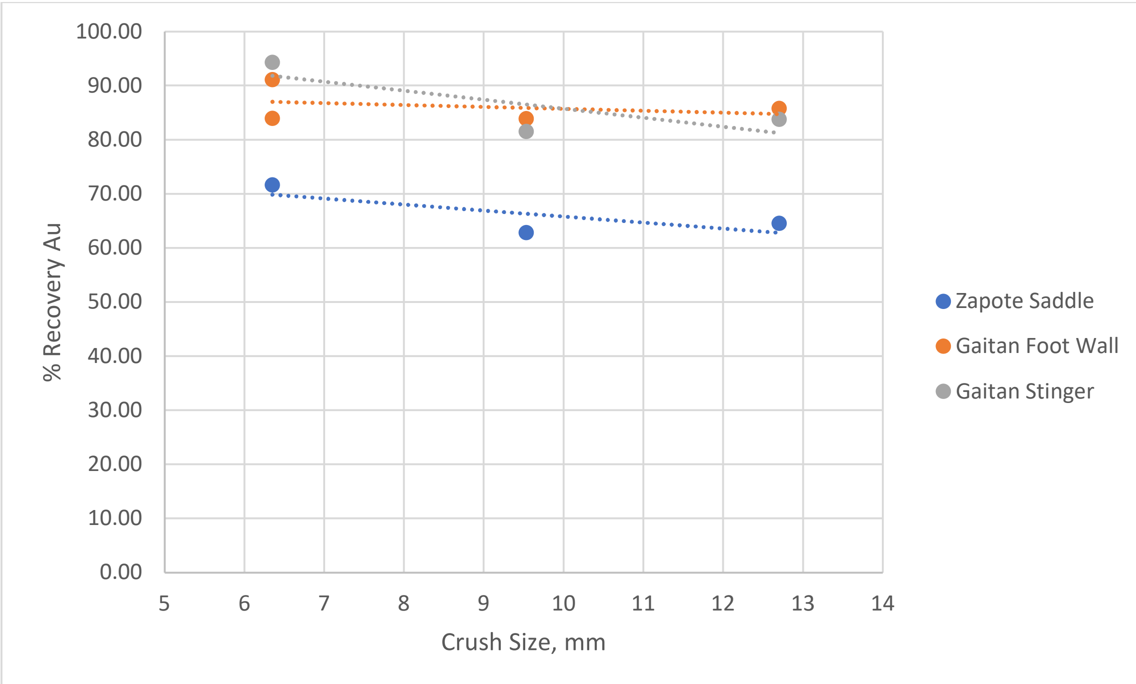


Figure 13-6 Heap Silver Recovery vs. Crush Size

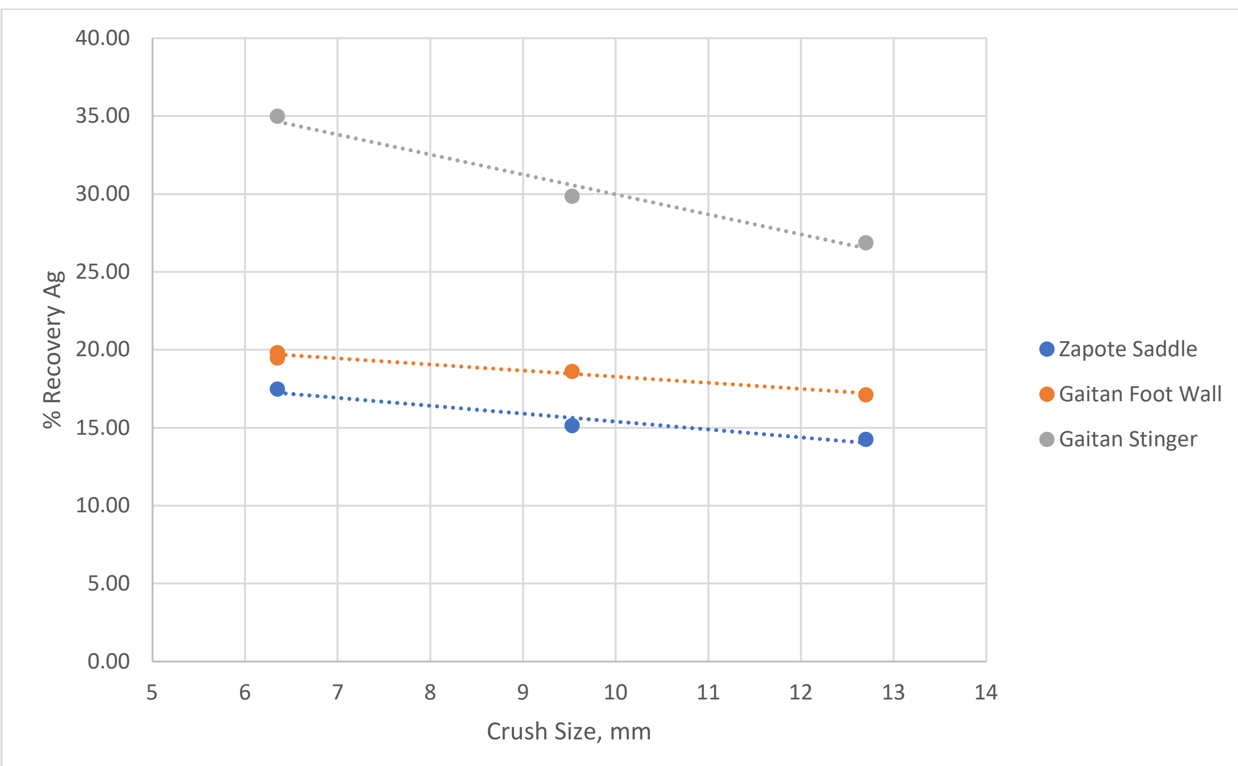


Figure 13-7 Agitated Leach Gold Recovery vs. Grind Size

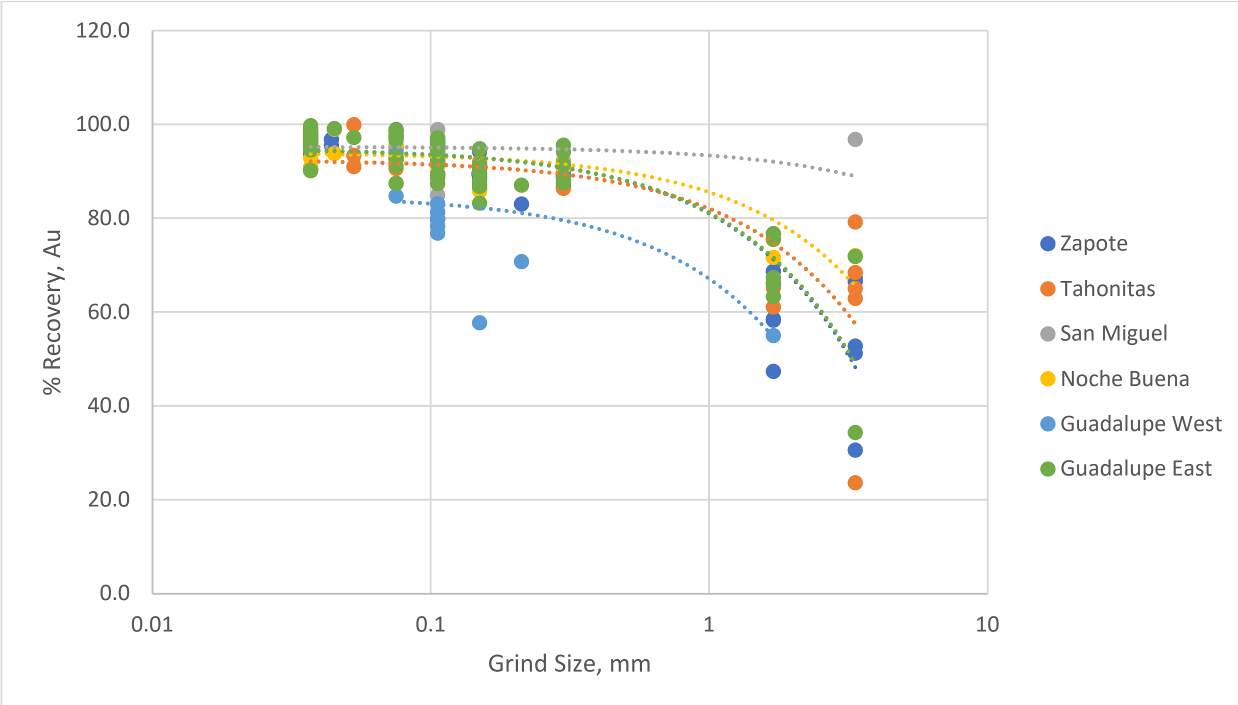
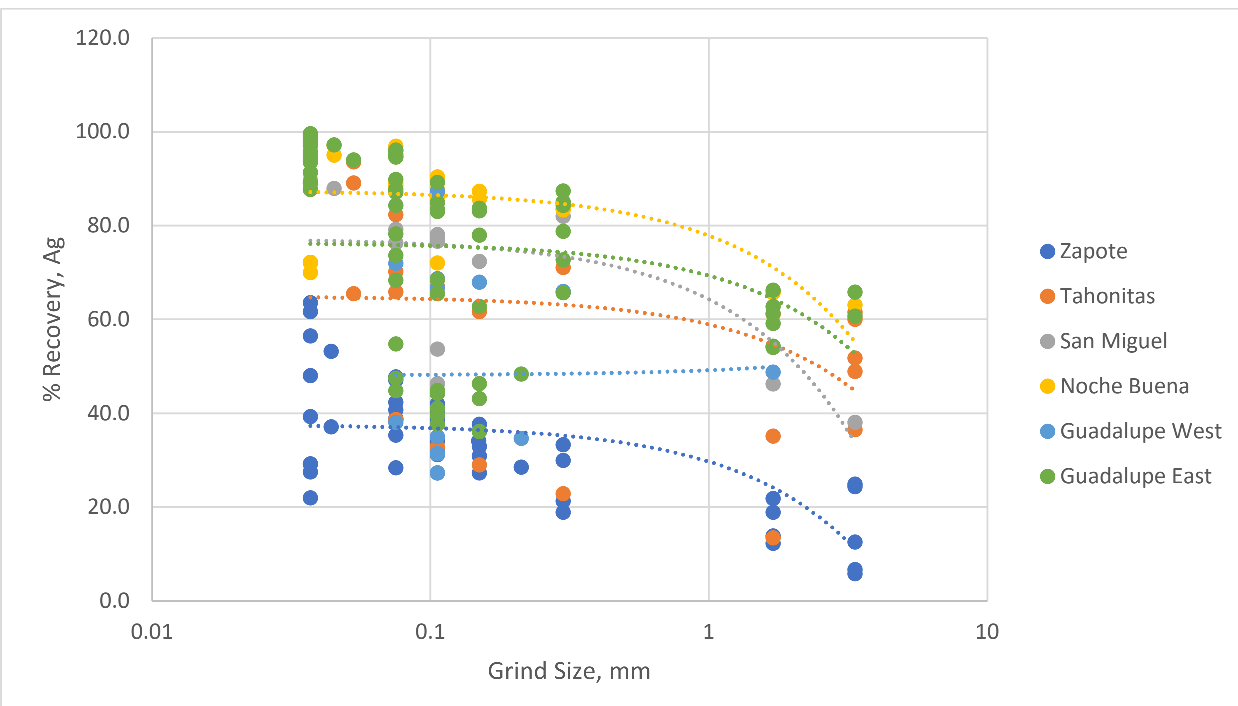


Figure 13-8 Agitated Leach Silver Recovery vs. Grind Size



Heap leach gold and silver recoveries are both directly related to material crush size with improved recoveries with finer crushing. A crush size of 80% passing 6.3 mm has been selected as this can generally be achieved with a modest conventional three-stage crushing circuit. For the purposes of resource estimation, KCA recommends using an average gold recovery of 73% and silver recovery of 25% based on the limited data available. Additional columns are currently in progress and will help to better define the heap recoveries.

Agitated leach recoveries generally improve with finer grinding with silver recoveries benefitting more at grind sizes finer than 0.106 to 0.075 mm (150 to 200 mesh) compared to gold which shows declining incremental recovery improvements. A grind size of 0.037 mm (400 mesh) is recommended to maximize the silver recoveries. Recoveries by deposit have been estimated by taking the average of the gold and silver recoveries for all tests at 0.037 mm. No discount for recovery has been applied to the agitated leach material. The weighted average recovery based on total contained ounces is estimated at 95.6% for gold and 81% for silver.

13.4.2 *Reagent Consumptions*

Reagent consumptions for the heap and agitated leach plants, respectively, have been estimated based on the average consumptions by material type from all available test work. Heap leach cyanide and lime consumptions have been estimated based on the bottle roll test consumptions, with heap cyanide consumption being estimated at 33% of the lab consumption based on KCA's experience. Cyanide and lime requirements for the agitated leach have been taken at a 1:1 ratio with the average lab results.

13.5 Preg-Robbing Discussion

Preg-robbing has been presented as a potential concern in some of the lab programs, which is a potential explanation for the improved recoveries for CIL leach tests. A program was completed by KCA in 2012 to evaluate preg-robbing potential of several materials. The program showed very high preg-robbing potential with some material types; however, many of the samples were contaminated with an organic emulsion which may have impacted the results making the program inconclusive.

Typical preg-robbing constituents, such as organic carbon and some clays, are not present in significant quantities in the Project materials and it is unknown what could be contributing to the preg-robbing effect. Preg-robbing potential should be further evaluated as preg-robbing could significantly impact the overall Project economics if present.

14. MINERAL RESOURCE ESTIMATE

14.1 Mineral Resource Statement

The Mineral Resource statement for the Project includes estimates for three principal mineralized trends on the property - (1) Z-T, which includes the Tahonitas, Zapote North, and Zapote South deposits; (2) Central, which includes the Noche Buena, San Miguel East, and San Miguel West deposits; and (3) Guadalupe, which includes the Guadalupe East and Guadalupe West deposits (Figures 10-3, 10-7, and 10-11). Three additional generative exploration targets adjacent to the principal trends, Fresnillo, Mariposa, and Las Primas, are also included in the Mineral Resource statement under 'Generative Areas'. All stated Resource estimates are expressed in contained ounces.

The Mineral Resources are stated in accordance with CIM Definition Standards in NI 43-101 and were estimated using drillholes completed on or before July 17, 2024. The Mineral Resource update presented here was prepared to support continued exploration and project work on the Property.

Mineral Resources were reported below the most recent LiDAR topographic surface and are contained within economically constrained pit shells generated using the Hochbaum Pseudoflow algorithm implemented in Datamine's Studio NPVS or underground stope shapes generated using Datamine's MSO. Open pit Mineral Resources are reported using a 0.17 g/t gold-only cutoff grade, and underground Mineral Resources are reported from stopes which meet or exceed an NSR value of US$80.81/tonne. The Mineral Resources are classified as Indicated or Inferred based on drill spacing and geological continuity. Tables 14-1 through 14-3 show the classified Mineral Resources for the Property.

Table 14-1 Mineral Resource Statement

Mining Method and Process	Class	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
Open Pit – Mill	Indicated	24,657	1.13	899	35.7	28,261
	Inferred	7,211	0.89	207	42.8	9,916
Underground – Mill	Indicated	4,132	3.02	402	152.4	20,243
	Inferred	4,055	2.10	273	78.6	10,247
Total Mill	**Indicated**	**28,789**	**1.41**	**1,301**	**52.4**	**48,504**
	Inferred	**11,266**	**1.33**	**480**	**55.7**	**20,163**
Open Pit - Heap Leach	Indicated	20,254	0.29	190	8.4	5,492
	Inferred	5,944	0.30	58	7.3	1,398
Total	**Indicated**	**49,042**	**0.95**	**1,491**	**34.2**	**53,995**
	Inferred	**17,210**	**0.97**	**538**	**39.0**	**21,561**

Notes for tables 14-1 through 14-3:

1. Open Pit Resource estimates are based on economically constrained open pits generated using the Hochbaum Pseudoflow algorithm in Datamine's Studio NPVS and the following optimization parameters (all dollar values are in US dollars):
    - $1,950/ounce gold price and $25.24/ounce silver price.
    - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
    - Heap leach recoveries of 73% and 25% for gold and silver, respectively.
    - Pit slopes by area ranging from 42-47 degrees overall slope angle.
    - 5% ore loss and 5% dilution factor applied to the 5 x 5 x 5m open pit resource block models.
    - Mining costs of $2.00 per tonne of waste mined and $2.50 per tonne of ore mined.
    - Milling costs of $16.81 per tonne processed.
    - Heap Leach costs of $5.53 per tonne processed.
    - G&A cost of $2.00 per tonne of material processed.
    - 3% royalty costs and 1% selling costs were also applied.
    - A 0.17 g/t gold only cutoff was applied to ex-pit processed material (which is above the heap-leaching NSR cutoff).
2. Underground Resource estimates are based on economically constrained stopes generated using Datamine's Mineable Shape Optimizer (MSO) algorithm and the following optimization parameters (all dollar values are in US dollars):
    - $1,950/ounce gold price and $25.24/ounce silver price.
    - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
    - Mechanized cut and fill mining with a $60.00 per tonne cost.
    - Diluted to a minimum 4m stope width with a 98% mining recovery.
    - G&A cost of $4.00 per tonne of material processed.
    - Milling costs of $16.81 per tonne processed.
    - 3% royalty costs and 1% selling costs were also applied.
3. Where mentioned, "residual open pits" assumes that any underground stopes are backfilled with zero grade material at two-thirds of the original rock density. Economic-constrained open pits are then estimated with this mined-out, backfilled material in the open pit block selective mining unit ("SMU") model and assuming the resource parameters above.
4. Mineral Resources are not Mineral Reserves (as that term is defined in the CIM Definition Standards) and do not have demonstrated economic viability.

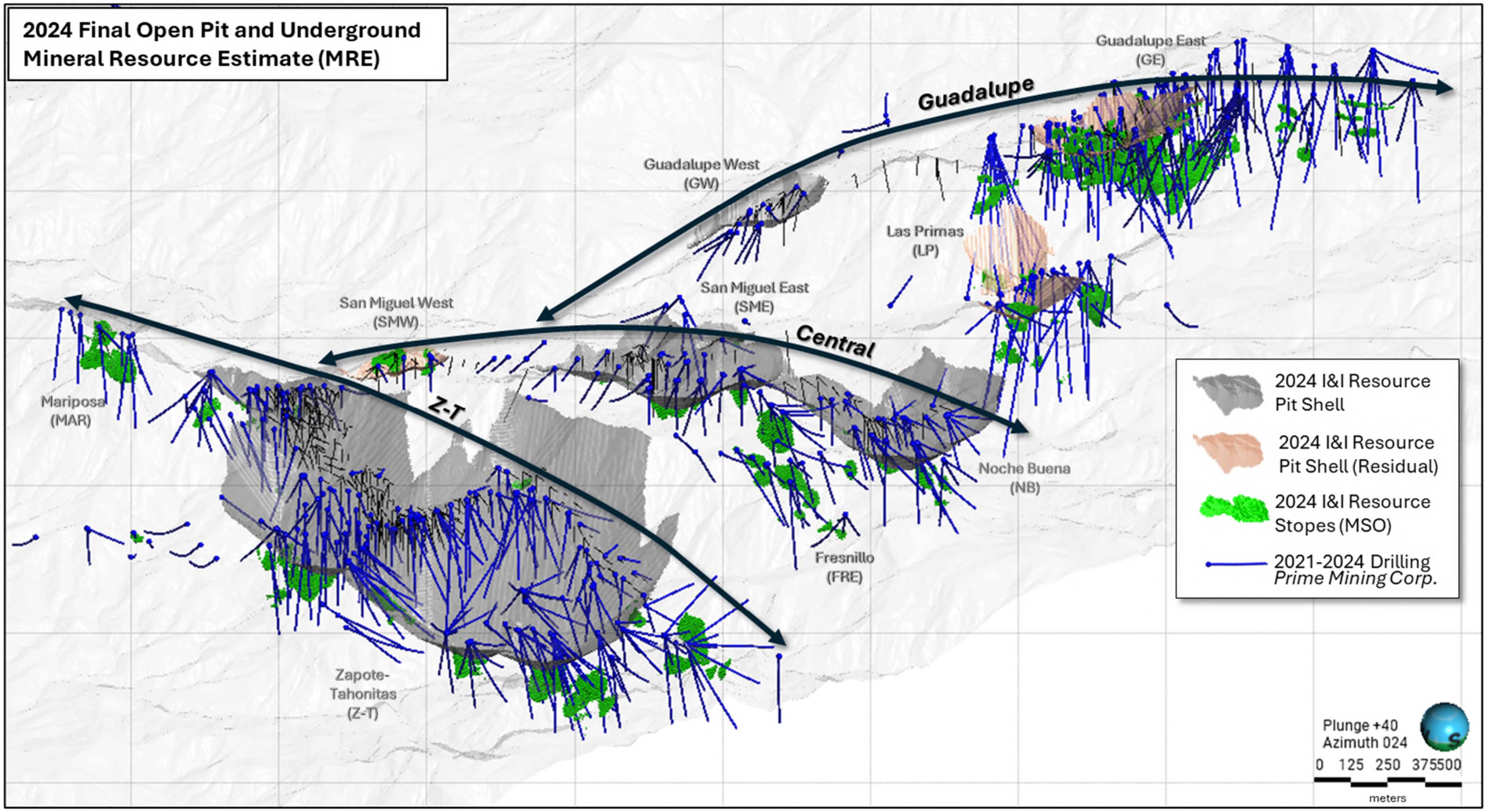
Table 14-2 Mineral Resource Statement by Mining Method and Area

Area	Mining Method	Classification	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
Z-T Trend	Open Pit	Indicated	29,183	0.78	734	21.7	20,316
		Inferred	9,322	0.68	205	29.9	8,957
	Underground	Indicated	2	1.26	0	24.6	2
		Inferred	1,624	1.98	103	78.7	4,110
Guadalupe Trend	Open Pit	Indicated	3,907	0.72	90	24.6	3,094
		Inferred	333	0.40	4	21.5	230
	Underground	Indicated	3,813	2.95	362	158.7	19,452
		Inferred	854	2.34	64	152.9	4,195
Central Trend	Open Pit	Indicated	10,972	0.71	251	28.3	9,977
		Inferred	3,069	0.48	48	20.4	2,018
	Underground	Indicated	135	6.63	29	72.6	316
		Inferred	397	1.44	18	36.3	463
Generative Areas	Open Pit	Indicated	849	0.49	13	13.4	366
		Inferred	431	0.55	8	7.9	110
	Underground	Indicated	182	1.83	11	81.0	473
		Inferred	1,180	2.31	88	39.0	1,479
Total	Open Pit	Indicated	44,910	0.75	1,089	23.4	33,753
		Inferred	13,155	0.63	265	26.8	11,314
	Underground	Indicated	4,132	3.02	402	152.4	20,243
		Inferred	4,055	2.10	273	78.6	10,247
	Total	**Indicated**	**49,042**	**0.95**	**1,491**	**34.2**	**53,995**
		Inferred	**17,210**	**0.97**	**538**	**39.0**	**21,561**

Table 14-3 Description of Resource Components for Tables 14-1 and 14-2, and Figure 14-1

Area	Deposit	Resource Description
Z-T Trend	Zapote-Tahonitas	Revenue Factor 1.0 Open Pits @0.17 g/t Au only cutoff plus remaining economic stopes
Guadalupe Trend	Guadalupe East	Economic underground stopes plus residual economic open pits above @0.17 g/t Au only cutoff
	Guadalupe West	Revenue Factor 1.0 Open Pits @0.17 g/t Au only cutoff
Central Trend	Noche Buena	Revenue Factor 1.0 Open Pits @0.17 g/t Au only cutoff plus remaining economic stopes
	San Miguel East	Revenue Factor 1.0 Open Pits @0.17 g/t Au only cutoff plus remaining economic stopes
	San Miguel West	Economic underground stopes plus residual economic open pits above @0.17 g/t Au only cutoff
Generative Areas	Mariposa	Economic underground stopes
	Las Primas	Economic underground stopes plus residual economic open pits above @0.17 g/t Au only cutoff
	Fresnillo	Economic underground stopes

Figure 14-1 Oblique view showing pit shells and stopes which comprise the 2024 Los Reyes Mineral Resource Estimate



Notes:

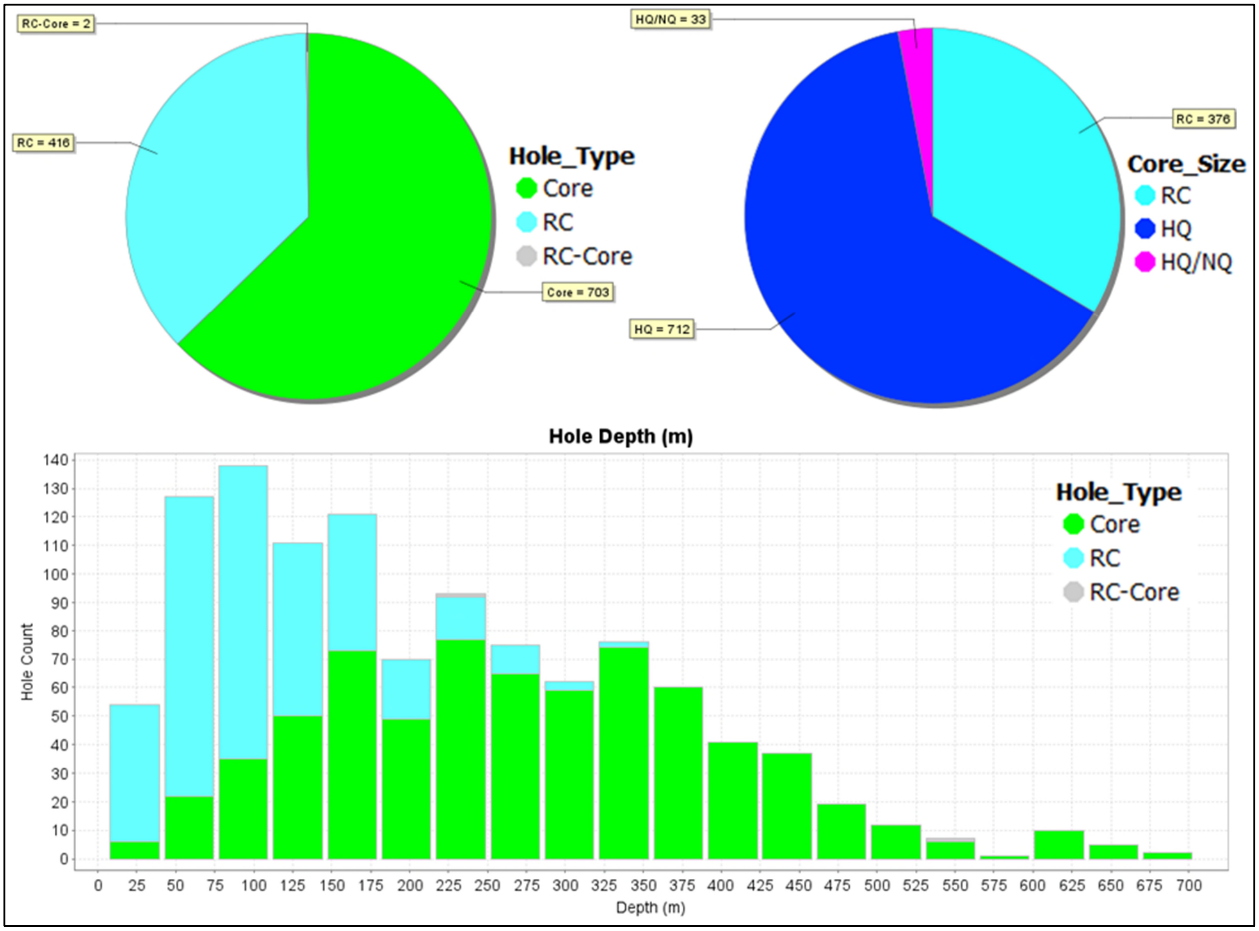
'Residual' pits at Guadalupe East, Las Primas, and San Miguel West assume that underground stopes are mined and then backfilled with zero-grade material at two-thirds of the original rock density. Economically constrained open pits are then generated with this mined-out, backfilled material flagged to the open pit SMU (5x5x5m) block models (see Table 14-3 and the section titled 'Residual Open Pit Optimization – 5x5x5m Block Models with Stopes Backfilled'). Underground Mineral Resources are otherwise only reported for stopes which fall outside Indicated and Inferred (I&I) Resource pit shell volumes.

14.2 Database

The Project database is maintained in a Microsoft SQL database management system, which contains collar locations, downhole survey data, qualitative logging information, and assay and multielement geochemical data, among other items. Data for geologic modelling and resource estimation purposes were exported as .csv files and then imported into Leapfrog Geo v.2023.2.3 and ioGAS v.8.2 for analysis. The database used for this report includes all drillholes on the property completed on or before July 17, 2024.

The full database export contains 1,180 drillholes, of which 62.2% are diamond drill holes comprising 80.9% of the total metreage, 37.6% are RC holes comprising 19.1% of the total metreage, and 0.2% are RC pre-collars with core tails comprising 0.002% of the total metreage. 59 holes were excluded from the MRE, either due to uncertainty in assay, survey, or collar information for historical holes, due to abandonment prior to achieving targeted depth, or due to the drillhole location falling outside the resource model extents. The resulting final estimation dataset contains 373 drillholes completed by NCM between 1993 and 1997, five completed by Meridian in 2001, 48 completed by Vista Gold in 2011 and 2012, 41 completed by Great Panther in 2015, and 654 completed by the Company between December 2020 and July 17, 2024, for a total of 240,172m in 1,121 holes. All Company drilling included in this estimate was completed after the April 2020 Los Reyes resource estimate and technical report (Turner and Hunter, 2020). Drilling statistics for the final estimation dataset are presented in Figure 14-2 and Table 14-4.

Figure 14-2 Hole type, core size, and hole depth statistics for the Los Reyes final estimation dataset



Notes:

Statistics do not consider information from drillholes excluded from the estimation.

Table 14-4 Final resource estimation dataset breakdown by area, company, and year

Company		NCM					Meridian	Vista			Great Panther	Prime					Total
Year		**1993**	**1994**	**1996**	**1997**	**sub-total**	**2001**	**2011**	**2012**	**sub-total**	**2015**	**2021** [1]	**2022** [2]	**2023**	**2024** [3]	**sub-total**	
Guadalupe	drill holes			49	30	79		10	8	18	9	42	105	23	11	181	**287**
	meters			5,333	5,216	0,549		1,470	1,482	2,952	1,494	11,297	36,973	8,031	3,911	60,211	**75,205**
Z-T	drill holes	28	38	55	113	234	5		15	15	11	58	94	80	40	272	**537**
	meters	2,337	3,376	4,249	8,025	17,986	829		1,886	1,886	1,156	11,726	21,692	27,234	14,173	74,824	**96,682**
Central	drill holes		4	9	46	59			15	15	21	31	50	29	6	116	**211**
	meters		247	1,017	5,003	6,267			2,582	2,582	2,855	6,769	11,759	8,751	1,937	29,215	**40,918**
Other	drill holes				1	1				0		10	11	39	25	85	**86**
	meters				166	166				0		1,901	3,033	11,642	10,625	27,200	**27,366**
Total	drill holes	28	42	113	190	373	5	10	38	48	41	141	260	171	82	654	**1,121**
	meters	2,337	3,623	10,599	18,410	34,968	829	1,470	5,950	7,420	5,505	31,692	73,457	55,658	30,645	191,451	**240,172**

Notes:

1. Two drill holes were started in December, 2020, one of which was completed in 2020.
2. 22FRE-09 (351.0m) was not completed in 2022 and was not included in the 2023 MRE.
3. Only holes completed prior to July 17, 2024 are included in the current October 2024 MRE.

14.3 Mineral Resource Estimate

The Project MRE was prepared by Prime with detailed review completed by, and under the supervision of Sims Resources LLC (John Sims, Independent QP). Geologic and estimation domains were constructed using Leapfrog Geo v.2023.2.3, including input from geochemical analyses completed in ioGAS v.8.2. Geostatistical evaluations and EDA, including topcut selection, declustering, variography, and SGS were completed using Snowden Supervisor v.9.0. Resource estimation was prepared using Leapfrog EDGE v.2023.2.3.

Two sets of block models were prepared for this MRE - (1) 5x5x5m block models were generated for use in open pit optimization, and (2) 2.5x2.5x2.5m block models were generated for use in underground MSO. The 5x5x5m and 2.5x2.5x2.5m models are estimated independently, and employ distinct compositing, domaining, and estimation strategies which are suitable for their respective mining methods and SMU. Parameters for each set of block models are described in detail below.

14.3.1 *Data Preparation*

Drillhole data used in the MRE were checked for overlapping sample intervals, negative or invalid values, and irregular downhole survey deviation in Leapfrog Geo. All errors were assessed and corrected prior to completing statistical analysis and estimation.

Drillhole collars were also visually checked against the most current topographic surface. Most collars are set to the topographic surface, with minor deviations (<1 meter) in some collars attributed to local variations in the topography.

Gold and silver assay values less than the detection limit were assigned a value equal to half of the detection limit value, which, depending on the analysis date and laboratory, was 0.001ppm, 0.005ppm, or 0.03ppm for Au and 0.1ppm, 0.5ppm, or 0.7ppm for Ag**.** Null values for Au and Ag were assigned for all intervals with no recovery or where historical mine workings, voids, or backfill material were encountered.

14.3.2 *Wireframes*

<u>Topography</u>

Topography data for the Project was gathered by Pioneer Exploration Consultants Ltd. in March 2021. No significant disturbance (mining) has occurred in the Project area since. Data were collected by airborne LiDAR survey and were processed using Green Valley LiDAR 360 software, and the resulting 1 m-resolution bare earth surface was used to define the topographic limits for the Project geologic model and MRE block models discussed below.

Historical Underground Workings

Historical mine workings solids were constructed in AutoCAD using a combination of underground LiDAR scans, digitized plan maps and long sections, and logged working intervals intercepted in drilling (Lindstrom, 2023). LiDAR scans were collected and processed by Unmanned Aerial Services Incorporated ("**Unmanned Aerial Services**") in April 2022 for accessible underground workings on the Property. The output wireframes from this work were then used in conjunction with intercepted workings intervals from surveyed drillholes to georeferenced historical map data, particularly in areas where collapse, backfill, or other conditions prevented full access to scan the workings. Additional data were gathered by Unmanned Aerial Services in 2024 and were used to supplement the 2023 dataset.

The proportion of a block which lies within the historical workings wireframes was calculated for model depletion and reporting purposes. Final block density was then determined by considering the weighted average of the in-situ portion of the block, at its original density according to lithology and estimation domain, and the historically mined portion of the block, at an assigned density of 0.0 g/cm^3. Logged workings intervals encountered in drilling outside the wireframes were also depleted in the model using an indicator estimate, in which logged workings were assigned a value of 1 and all other lithology codes were assigned a value of 0. Blocks with estimated indicator values greater than 0.5 were then flagged to the model as 100% mined (Mined_Pct = 1, Figures 14-3 and 14-4).

Sensitivity work assuming a mined-out halo around mapped or inferred workings was also performed. The overall resource was not materially sensitive to these estimates.

Figure 14-3 Upper – Underground workings wireframes and logged workings intervals in the Guadalupe East area. Lower – Model filtered for blocks with mined proportion greater than 0 (Mined_Pct >0)

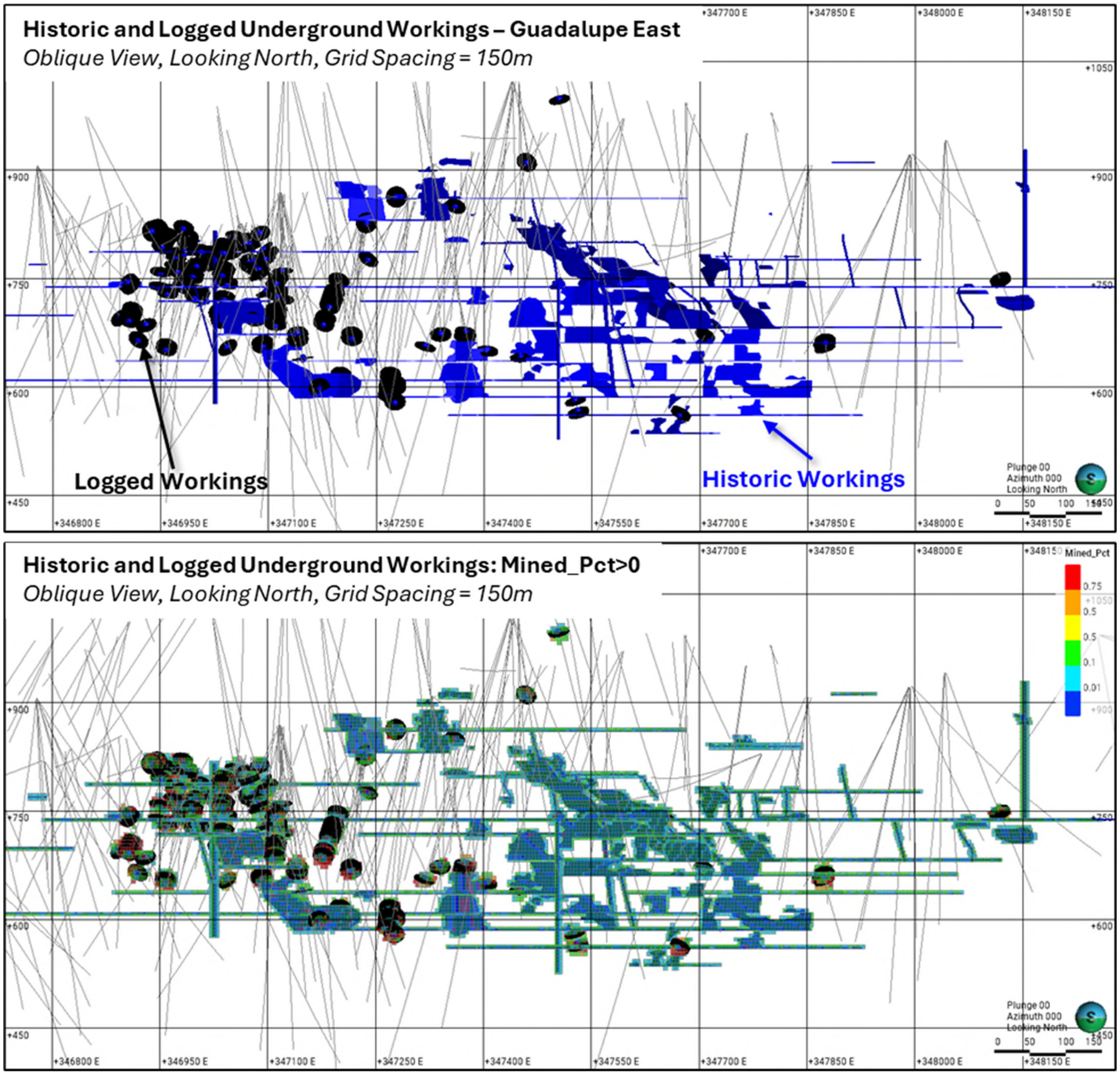
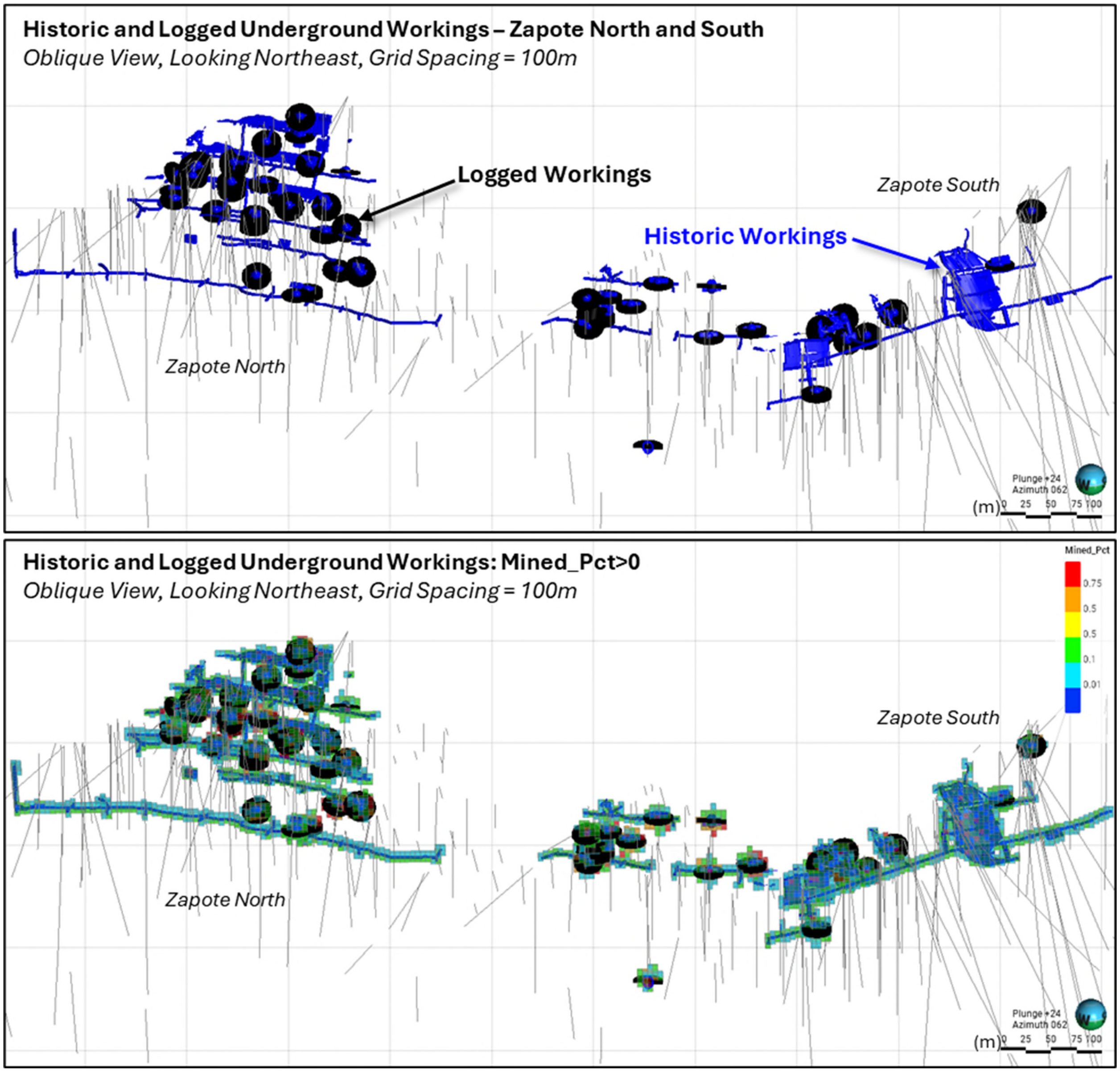


Figure 14-4 Upper – Underground workings wireframes and logged workings intervals in the Zapote North and South areas. Lower – Model filtered for blocks with mined proportion greater than 0 (Mined_Pct >0)



Lithology and Faults

Lithology and fault wireframes were generated in Leapfrog Geo using interval selection based on a merged table containing qualitative logging data (lithology, alteration, structure), Au and Ag assays, multi-element geochemistry, and geotechnical data (RQD, recovery). Structural measurements from oriented core were used to influence modeled surfaces where available. Geographic Information Systems (GIS) data from 1:5,000 and 1:2,000 scale geologic mapping, including lithologic contacts and structural point data, were also applied as direct inputs to the modeled surfaces. All lithology and fault wireframes were manually edited based on geologic interpretations by the Company geologists and were validated against hand-drawn cross sections completed in key areas across the various deposits before use in MRE.

Three faults were activated in the geologic model where major offsets in lithology are apparent; (1) the Z-T fault places rhyolitic intrusives in the hanging wall against andesite and granodiorite in the footwall, (2) the NB-SME fault places dacitic intrusives in the hanging wall against andesites in the footwall, and (3) the Estaca fault places rhyolitic intrusives, dacitic intrusives, and andesites in the hanging wall against granodiorite in the footwall (Figures 14-5 and 14-6). These three fault zones are pre-syn mineral and are key district-scale controlling structures for quartz veining and Au-Ag mineralization. Several minor, generally northeast-striking post-mineral faults were also built but were not activated in the model because they do not show appreciable offset. All fault and lithology wireframes were snapped to drillhole data and were checked for closure and consistency prior to resource estimation. Six major lithologies were modeled and are outlined in Table 14-5.

Figure 14-5 Los Reyes Fault Model

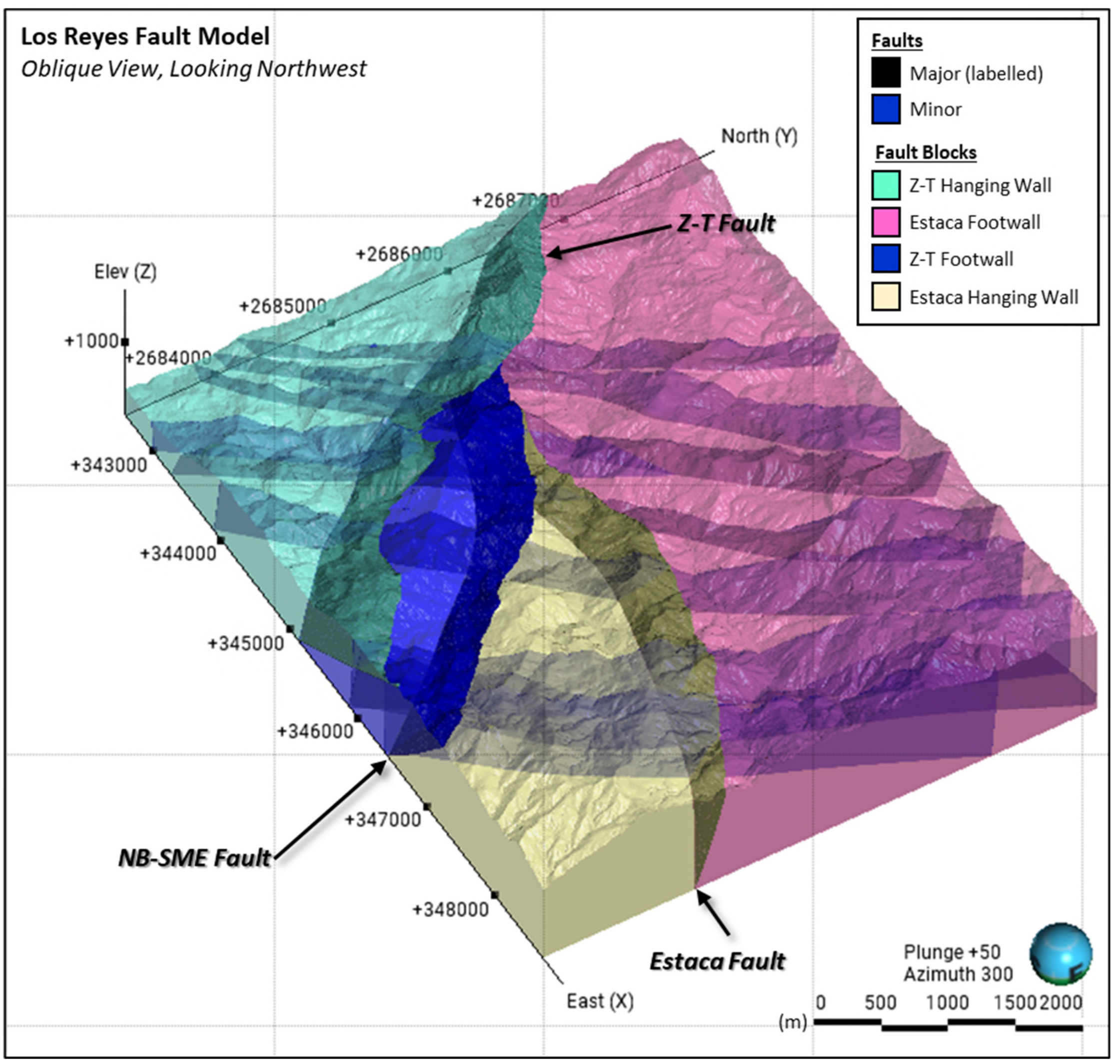
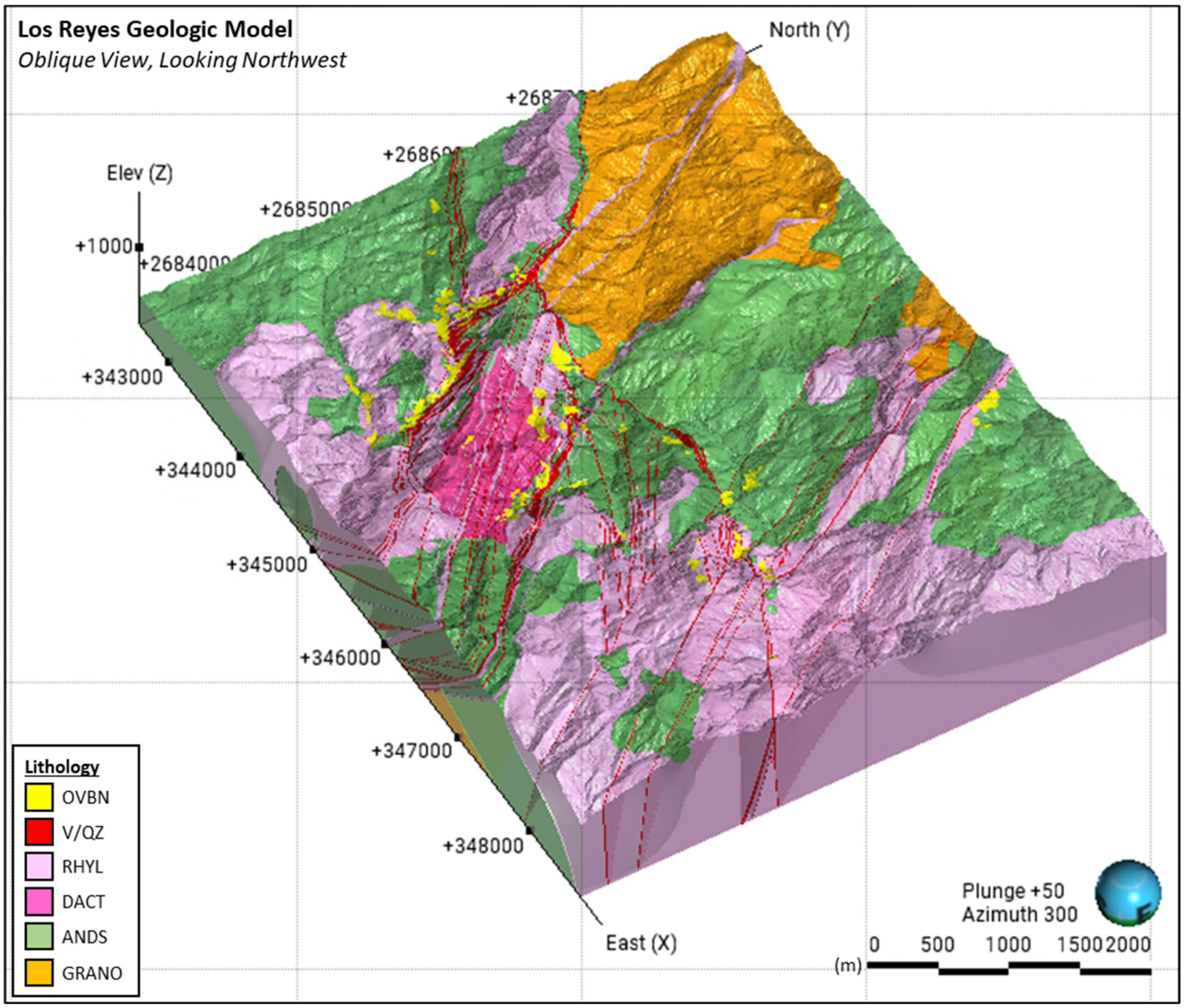


Table 14-5 Lithology Codes

Code	Lithology	Description
1	V/QZ	Quartz vein/stockwork and silicified breccias
2	RHYL	Rhyolitic intrusive domes and dikes
3	DACT	Dacitic intrusive domes and dikes
4	ANDS	Andesites and andesitic tuffs
5	GRANO	Granodiorite
6	OVBN	Overburden

Figure 14-6 Los Reyes Lithology Model

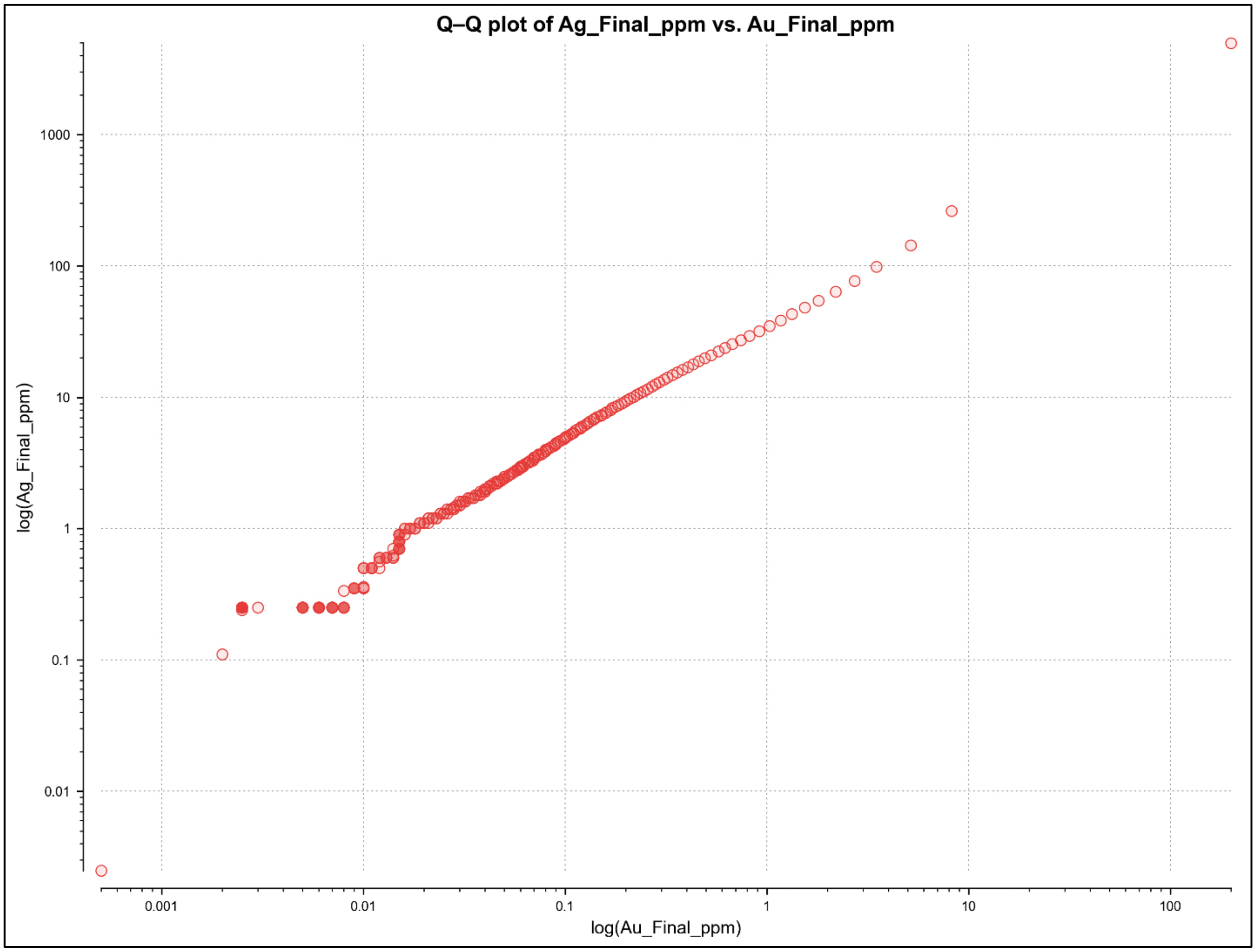


Mineralization

Gold and silver mineralization are spatially and genetically associated with low-sulphidation epithermal quartz veins at the Property, with a strong positive correlation observed between concentrations of the two metals across all deposits (Figure 14-7). Given this relationship between Au and Ag, mineralized domain wireframes were constructed based on gold-equivalent (AuEq) grades, using the formula: AuEq = Au (g/t) + (Ag (g/t) x $25.24/$1,950), where $25.24/oz and $1,950/oz are the assumed metals prices for silver and gold, respectively. Gold-equivalent grades calculated in this manner are used only to define mineralized envelopes for estimation domain construction and at no point are used as an input for open pit optimization, underground Mineable Shape Optimization (MSO), or resource reporting. Gold and silver are estimated independently in all domains, with unique topcut selection, variography, and estimation parameters determined for each metal in each domain. Metals price assumptions and metallurgical recoveries are similarly assessed independently for gold and silver when calculating block revenues for pit optimization and stope optimization (see section 14.3.11).

A cutoff grade of 0.2 g/t AuEq was selected for mineralized domains in the 5x5x5m set of block models, and a 1.0 g/t AuEq cutoff grade was selected for mineralized domains in the 2.5x2.5x2.5m set of block models described below. Grade shells were generated for both cutoff grades using the Indicator Interpolant tool and spherical interpolant function in Leapfrog Geo, with geometry and continuity controlled by a structural trend generated from vein midpoint surfaces in the quartz vein and breccia model ("V/QZ"). Manual edits to the grade shell volumes were also completed where necessary to reflect the interpreted continuity of mineralization as determined by Company geologists. Grade shell volumes were restricted to the V/QZ solid and were subsequently divided based on changes in orientation to generate the final mineralized domains for estimation (Figures 14-8 and 14-9; Tables 14-6 and 14-7).

Figure 14-7 Q-Q plot showing Au vs. Ag in assays at Los Reyes



5x5x5m Block Models

The domain strategy for the 5x5x5m block models used in Open Pit optimization follows a nested approach, with three major domain groups – (1) Mineralized domains, with the prefix '02AuEQ', represent volumes inside the V/QZ solid that are also inside the grade shells generated at a 0.2 g/t AuEq cutoff grade (Figure 14-8). (2) Quartz vein and breccia envelope domains with the prefix QV_BX, represent volumes which are inside the V/QZ solid, but fall outside the 0.2 g/t AuEq grade shells. (3) Background domains with the prefix BACKGROUND, represent volumes outside the grade shells and outside the V/QZ solid. Table 14-6 lists all domains estimated in the 5x5x5m block models.

Figure 14-8 Mineralized domains for Au and Ag grade estimation in 5x5x5m block models used for open pit optimization

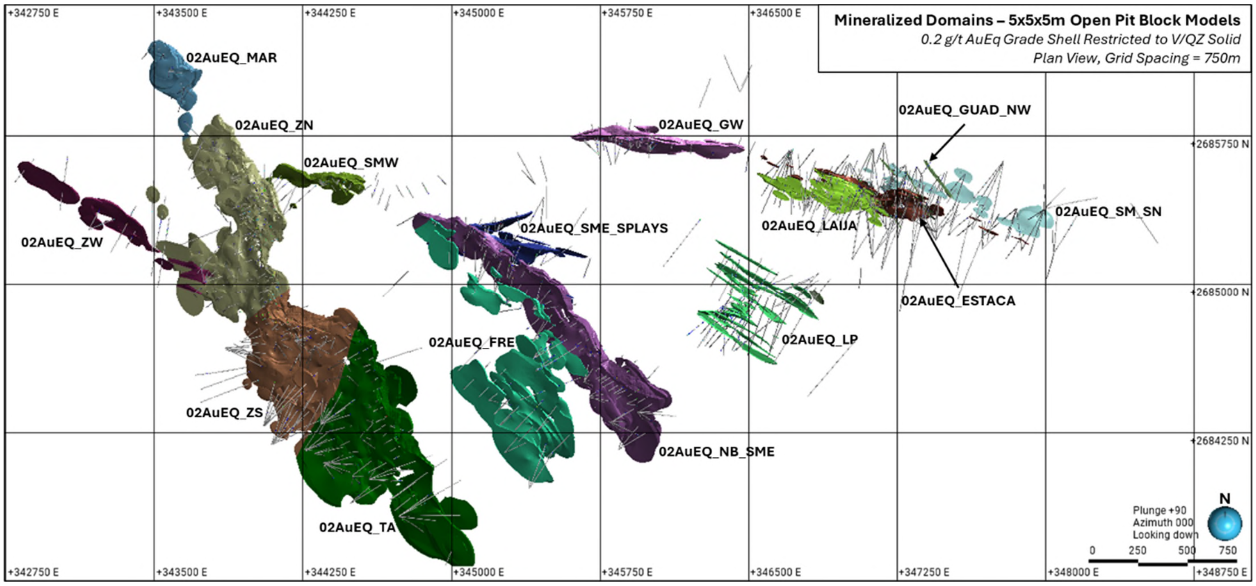


Table 14-6 Los Reyes estimation domains for Au and Ag grade estimation in the 5x5x5m block models used for open pit optimization

Domain Group	Block Model	Code	Domain	Description
QV_BX mineralized	ZTM_NB_SM_5x5x5_Rotated	100	02AuEQ_MAR	Mariposa mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		101	02AuEQ_ZN	Zapote North mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		102	02AuEQ_ZS	Zapote South mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		103	02AuEQ_TA	Tahonitas mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		104	02AuEQ_SMW	San Miguel West mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		105	02AuEQ_NB_SME	Noche Buena/San Miguel East mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		106	02AuEQ_SME_SPLAYS	San Miguel East Splays mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		114	02AuEQ_ZW	Zapote West mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
	GUAD_LP_5x5x5_Rotated	107	02AuEQ_GW	Guadalupe West mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		108	02AuEQ_LAIJA	Laija mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		109	02AuEQ_ESTACA	Estaca mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		110	02AuEQ_SM_SN	San Manuel and San Nicolas quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		111	02AuEQ_LP	Las Primas mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		112	02AuEQ_FRE	Fresnillo mineralized quartz vein/bx (inside 0.2 gpt AuEq grade shell)
		113	02AuEQ_GUAD_NW	NW-striking Guadalupe mineralized quartz vein/bx (inside 0.2gpt AuEq grade shell)
QV_BX non-mineralized	ZTM_NB_SM_5x5x5_Rotated	200	QV_BX_ZTM	ZTM structure non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
		201	QV_BX_FRE	Fresnillo non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
		202	QV_BX_NB_SME	Noche Buena/San Miguel East non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
		203	QV_BX_SME_SPLAYS	San Miguel East Splays non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
		210	QV_BX_ZW	Zapote West non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
	GUAD_LP_5x5x5_Rotated	204	QV_BX_LP	Las Primas non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
		205	QV_BX_GW	Guadalupe West non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
		206	QV_BX_LAIJA	Laija non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
		207	QV_BX_ESTACA	Estaca non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
		208	QV_BX_SM_SN	San Manuel and San Nicolas non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
		209	QV_BX_GUAD_NW	NW-striking Guadalupe structures non-mineralized quartz vein/bx (outside 0.2gpt AuEq grade shell)
Background	ZTM_NB_SM_5x5x5_Rotated	301	BACKGROUND_ZTM_NB_SM	ZTM_NB_SM_5x5x5 model background domain (outside vein/bx solid)
	GUAD_LP_5x5x5_Rotated	302	BACKGROUND_GUAD_LP	GUAD_LP_5x5x5 model background domain (outside vein/bx solid)

2.5x2.5x2.5m Block Models

The domain strategy for the 2.5x2.5x2.5m block models used in underground MSO follows a nested approach, with three major domain groups – (1) Mineralized domains, with the prefix '1AuEQ', represent volumes inside the V/QZ solid that are also inside the grade shells generated at a 1.0 g/t AuEq cutoff grade (Figure 14-9). (2) Quartz vein and breccia envelope domains with the prefix QV_BX, represent volumes which are inside the V/QZ solid, but fall outside the 1.0 g/t AuEq grade shells. (3) Background domains with the prefix BACKGROUND, represent volumes outside the grade shells and outside the V/QZ solid. Table 14-7 lists all domains estimated in the 2.5x2.5x2.5m block models.

Figure 14-9 Mineralized domains for Au and Ag grade estimation in 2.5x2.5x2.5m block models used for MSO

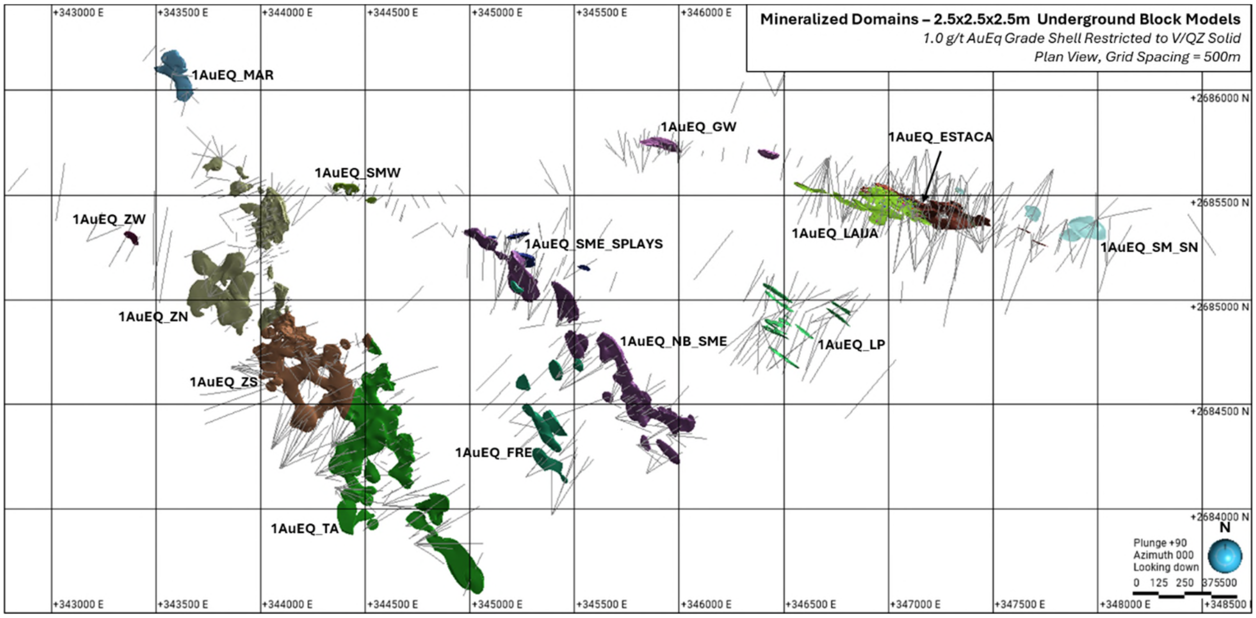


Table 14-7 Los Reyes estimation domains for Au and Ag grade estimation in the 2.5x2.5x2.5m block models used for underground optimization

Domain Group	Model	Domain Code	Domain	Description
QV_BX mineralized	ZTM_NB_SM_5x5x5_Rotated	100	1AuEQ_MAR	Mariposa mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		101	1AuEQ_ZN	Zapote North mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		102	1AuEQ_ZS	Zapote South mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		103	1AuEQ_TA	Tahonitas mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		104	1AuEQ_SMW	San Miguel West mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		105	1AuEQ_NB_SME	Noche Buena/San Miguel East mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		106	1AuEQ_SME_SPLAYS	San Miguel East Splays mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		114	1AuEQ_ZW	Zapote West mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
	GUAD_LP_5x5x5_Rotated	107	1AuEQ_GW	Guadalupe West mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		108	1AuEQ_LAIJA	Laija mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		109	1AuEQ_ESTACA	Estaca mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		110	1AuEQ_SM_SN	San Manuel and San Nicolas quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		111	1AuEQ_LP	Las Primas mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		112	1AuEQ_FRE	Fresnillo mineralized quartz vein/bx (inside 1.0 gpt AuEq grade shell)
		113	1AuEQ_GUAD_NW	NW-striking Guadalupe mineralized quartz vein/bx (inside 1.0gpt AuEq grade shell)
QV_BX non-mineralized	ZTM_NB_SM_5x5x5_Rotated	200	QV_BX_ZTM	ZTM structure non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
		201	QV_BX_FRE	Fresnillo non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
		202	QV_BX_NB_SME	Noche Buena/San Miguel East non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
		203	QV_BX_SME_SPLAYS	San Miguel East Splays non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
		210	QV_BX_ZW	Zapote West non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
	GUAD_LP_5x5x5_Rotated	204	QV_BX_LP	Las Primas non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
		205	QV_BX_GW	Guadalupe West non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
		206	QV_BX_LAIJA	Laija non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
		207	QV_BX_ESTACA	Estaca non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
		208	QV_BX_SM_SN	San Manuel and San Nicolas non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
		209	QV_BX_GUAD_NW	NW-striking Guadalupe structures non-mineralized quartz vein/bx (outside 1.0gpt AuEq grade shell)
Background	ZTM_NB_SM_5x5x5_Rotated	301	BACKGROUND_ZTM_NB_SM	ZTM_NB_SM_5x5x5 model background domain (outside vein/bx solid)
	GUAD_LP_5x5x5_Rotated	302	BACKGROUND_GUAD_LP	GUAD_LP_5x5x5 model background domain (outside vein/bx solid)

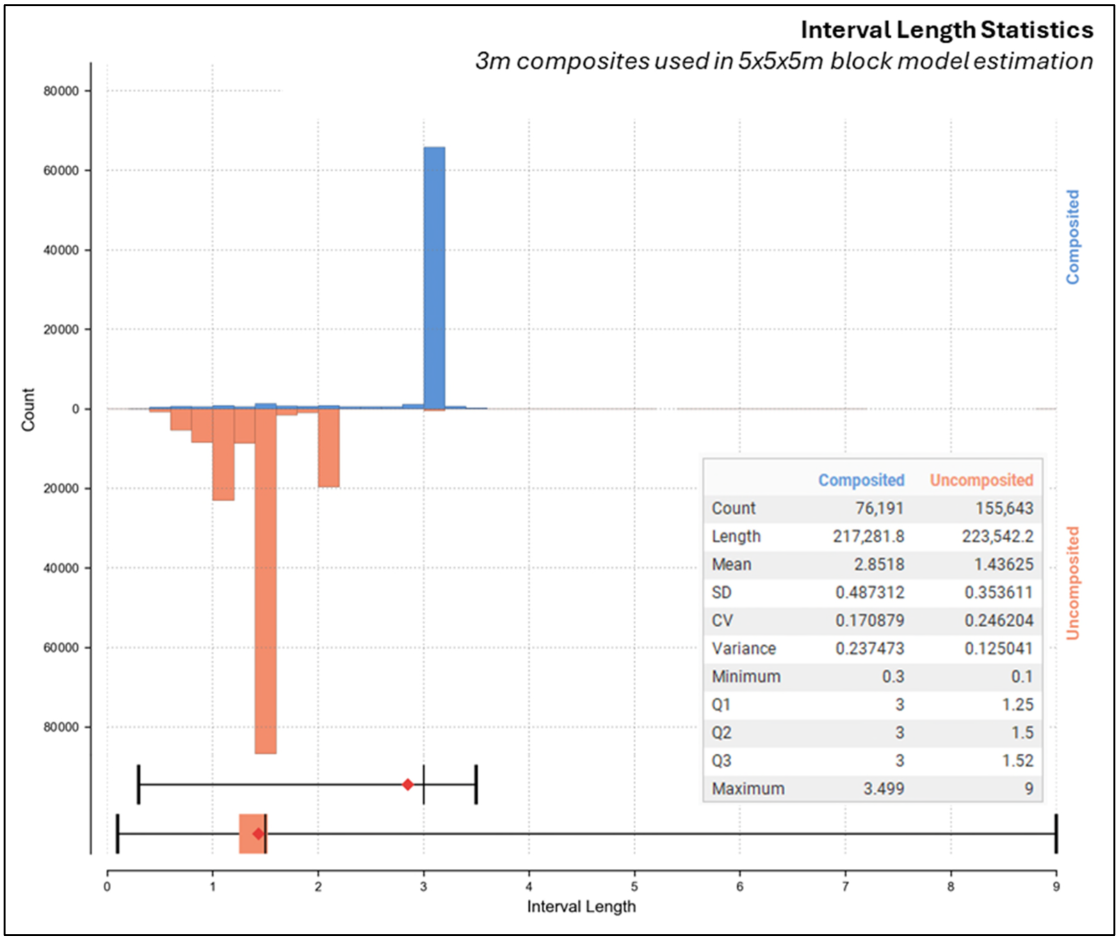
14.3.3 *Composites*

The most frequent sample interval in the assay data table is 1.5 metre, with sample intervals 1.5 ± 0.05 metre in length representing 51.7% of the total dataset. Compositing strategies for the 5x5x5m and 2.5x2.5x2.5m block models are distinct, given the difference in SMU, and are outlined individually below.

5x5x5m Block Models

To reduce variability and ensure the same support for estimation, a 3 metre compositing interval was selected for gold and silver estimation in the 5x5x5m block models. The 3 metre compositing length was selected because it is a multiple of the most frequent, 1.5 metre sample length in the assay table, is more appropriate for the 5x5x5m SMU, and because it maintains the same composite interval to SMU ratio as applied for the 2.5x2.5x2.5m block models (0.6). Composites were generated to respect the domain boundaries presented in table 14-6. Figure 14-10 shows a global comparison between raw assay interval lengths and composited data used for estimation in the 5x5x5m block models.

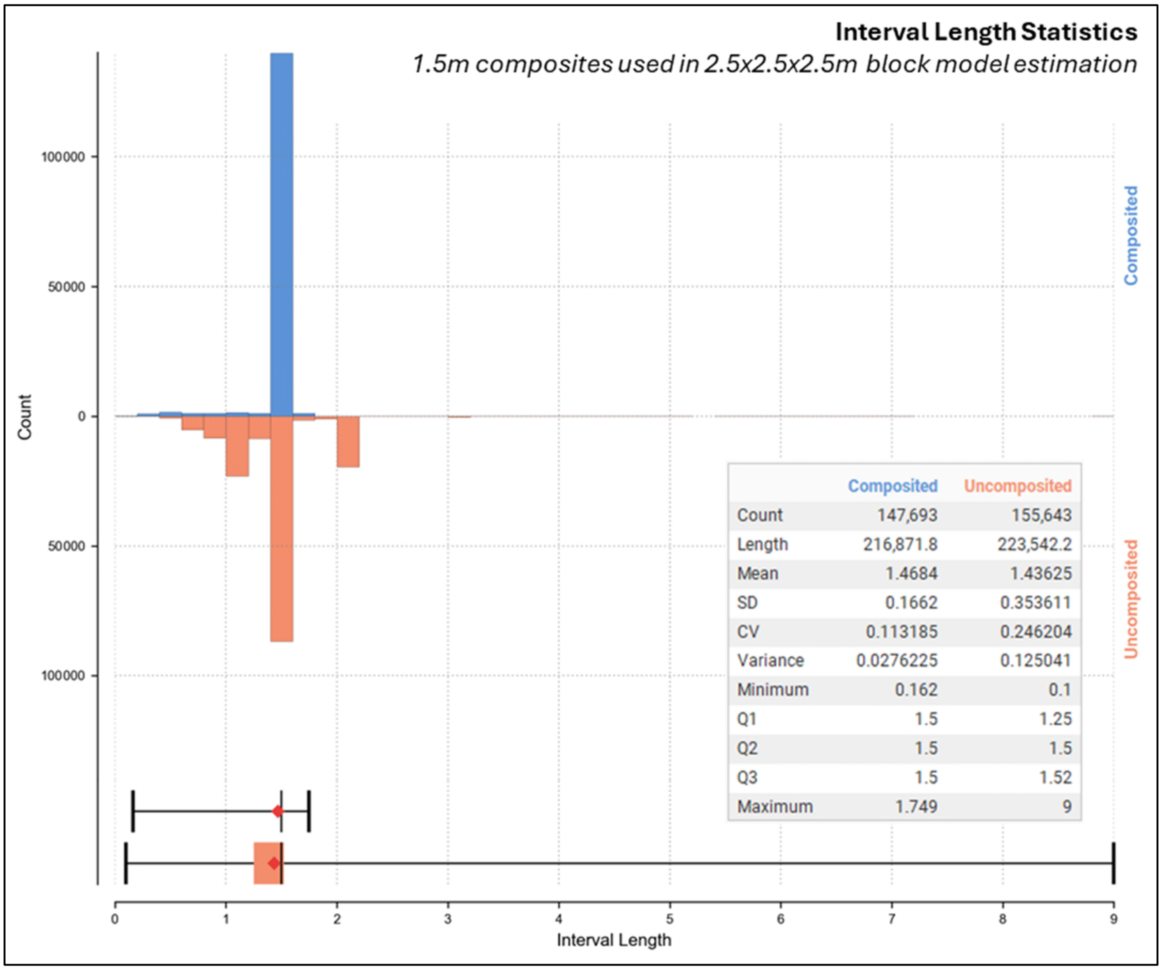
Figure 14-10 Global compositing interval length statistics for 3m composites used for estimation in 5x5x5m block models



<u>2.5x2.5x2.5m Block Models</u>

Gold and silver assays were composited using a 1.5 metre composite length for estimation in the 2.5x2.5x2.5m SMU block models, consistent with the most frequent sample interval in the assay data table. Composites were generated to respect the domain boundaries presented in table 14-7. Figure 14-11 shows a global comparison between raw assay interval lengths and composited data used for estimation in the 2.5x2.5x2.5m block models.

Figure 14-11 Global compositing interval length statistics for 1.5m composites used for estimation in 2.5x2.5x2.5m block models



	Composited	Uncomposited
Count	147,693	155,643
Length	216,871.8	223,542.2
Mean	1.4684	1.43625
SD	0.1662	0.353611
CV	0.113185	0.246204
Variance	0.0276225	0.125041
Minimum	0.162	0.1
Q1	1.5	1.25
Q2	1.5	1.5
Q3	1.5	1.52
Maximum	1.749	9

14.3.4 *Exploratory Data Analysis*

Contact Analysis

Contact profiles were generated for Au and Ag across all estimation domains to assess grade interpolation limits between adjacent domains. Methodology for both sets of block models is described below.

5x5x5m Block Models

Based on the analysis of 3 metre Au and Ag composited data across contacting domains in the 5x5x5m models (Table 14-6), all contacts between mineralized domains (02AuEQ prefix) and other domain groups (QV_BX and BACKGROUND prefixes) were treated as hard, and a hard boundary was similarly applied between the QV_BX and BACKGROUND domain groups. Soft boundaries were applied between contacting mineralized domains of different structural orientations (ex: 02AuEQ_Estaca and 02AuEQ_LAIJA in Figure 14-12), with a maximum soft boundary search distance set to half the first pass search dimensions of the primary domain. No boundary was applied between domains belonging to the main Zapote-Tahonitas (Z-T) structure because mineralization is continuous between the Tahonitas (TA), Zapote South (ZS), and Zapote North (ZN) areas. These domains were separated solely to isolate changes in orientation of the Z-T structure for variography. Contact analysis summaries for domains estimated in the 5x5x5m block models are shown in Table 14-8.

Figure 14-12 Contact plot examples from the 02AuEQ_ESTACA domain, showing soft boundaries (left) and hard boundaries (right) for Au (upper) and Ag (lower)

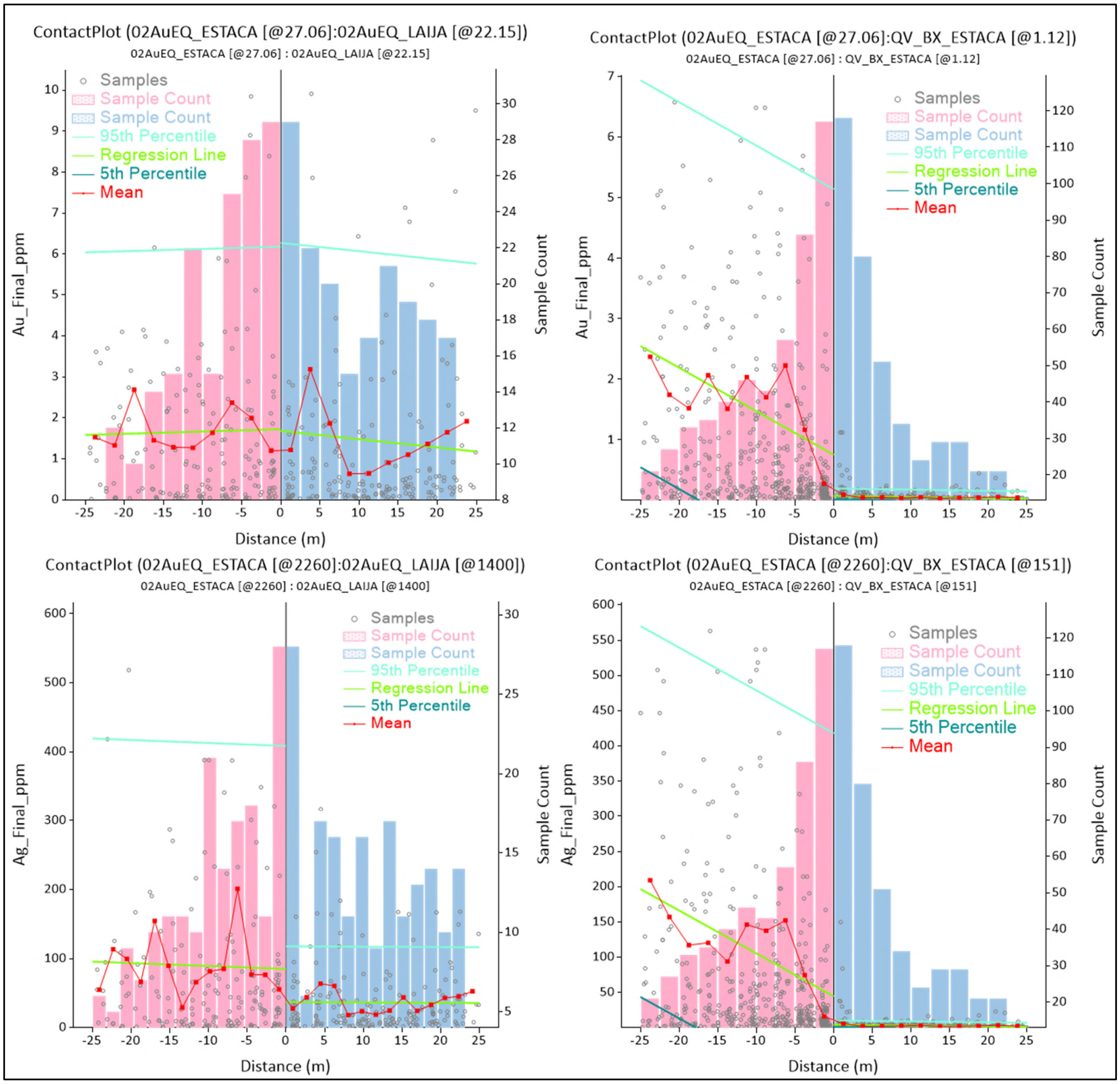


Table 14-8 Contact analysis summary for domains in 5x5x5m block models used for open pit optimization

Domain Group	Au_Domain	Soft Boundary	Soft Boundary search max. (m)	Comment
QV_BX Mineralized	02AuEQ_ESTACA	02AuEQ_LAIJA, 02AuEQ_SM_SN	30	Laija and SM/SN are antithetic to Estaca but part of the same vein system. Half pass 1 search dir1 distance used.
	02AuEQ_FRE	-	N/A	Hard boundary
	02AuEQ_GUAD_NW	-	N/A	Hard boundary
	02AuEQ_GW	-	N/A	Hard boundary
	02AuEQ_LAIJA	02AuEQ_Estaca	30	Laija veins are antithetic to Estaca but part of same system. Half pass 1 search dir1 used.
	02AuEQ_MAR	-	N/A	Hard boundary
	02AuEQ_NB_SME	02AuEQ_SME_SPLAYS	30	SME footwall splays off main NB_SME structure. Half pass 1 search dir1 distance used.
	02AuEQ_SM_SN	02AuEQ_Estaca	30	SM/SN veins are antithetic to Estaca but part of same system. Half pass 1 search dir1 distance used.
	02AuEQ_SME_SPLAYS	02AuEQ_NB_SME	30	SME footwall splays off main NB_SME structure. Half pass 1 search dir1 distance used.
	02AuEQ_SMW	-	N/A	Hard boundary
	02AuEQ_TA	02AuEQ_ZS	120	Full search pass 2 search direction 1 distance used (no boundary). Very few samples available for contact analysis but TA, ZS, and ZN are part of the same structure and are only separated for estimation due to changes in the strike/dip of the ZT structure.
	02AuEQ_ZN	02AuEQ_ZS	120	
	02AuEQ_ZS	02AuEQ_TA, 02AuEQ_ZS	120	
QV_BX Non-Mineralized	QV_BX_ESTACA	-	N/A	Hard boundary
	QV_BX_FRE	-	N/A	Hard boundary
	QV_BX_GUAD_NW	-	N/A	Hard boundary
	QV_BX_GW	-	N/A	Hard boundary
	QV_BX_LAIJA	-	N/A	Hard boundary
	QV_BX_LP	-	N/A	Hard boundary
	QV_BX_NB_SME	-	N/A	Hard boundary
	QV_BX_SM_SN	-	N/A	Hard boundary
	QV_BX_SME_SPLAYS	-	N/A	Hard boundary
	QV_BX_ZTM	-	N/A	Hard boundary
Background	BACKGROUND_GUAD_LP	-	N/A	Hard boundary
	BACKGROUND_ZTM_NB_SM	-	N/A	Hard boundary

2.5x2.5x2.5m Block Models

Based on the analysis of 1.5 metre Au and Ag composited data across contacting domains in the 2.5x2.5x2.5m models (Table 14-7), all contacts between mineralized domains (1AuEQ prefix) and other domain groups (QV_BX and BACKGROUND prefixes) were treated as hard, and a hard boundary was similarly applied between the QV_BX and BACKGROUND domain groups. Soft boundaries were applied between contacting mineralized domains of different structural orientations (ex: 1AuEQ_Estaca and 1AuEQ_LAIJA in Figure 14-13), with a maximum soft boundary search distance set to half the first pass search dimensions of the primary domain. No boundary was applied between domains belonging to the main Zapote-Tahonitas (Z-T) structure because mineralization is continuous between the Tahonitas (TA), Zapote South (ZS), and Zapote North (ZN) areas. These domains were separated solely to isolate changes in orientation of the Z-T structure for variography. Contact analysis summaries for domains estimated in the 2.5x2.5x2.5m block models are shown in Table 14-9.

Figure 14-13 Contact plot examples from the 1AuEQ_LAIJA domain, showing soft boundaries (left) and hard boundaries (right) for Au (upper) and Ag (lower)

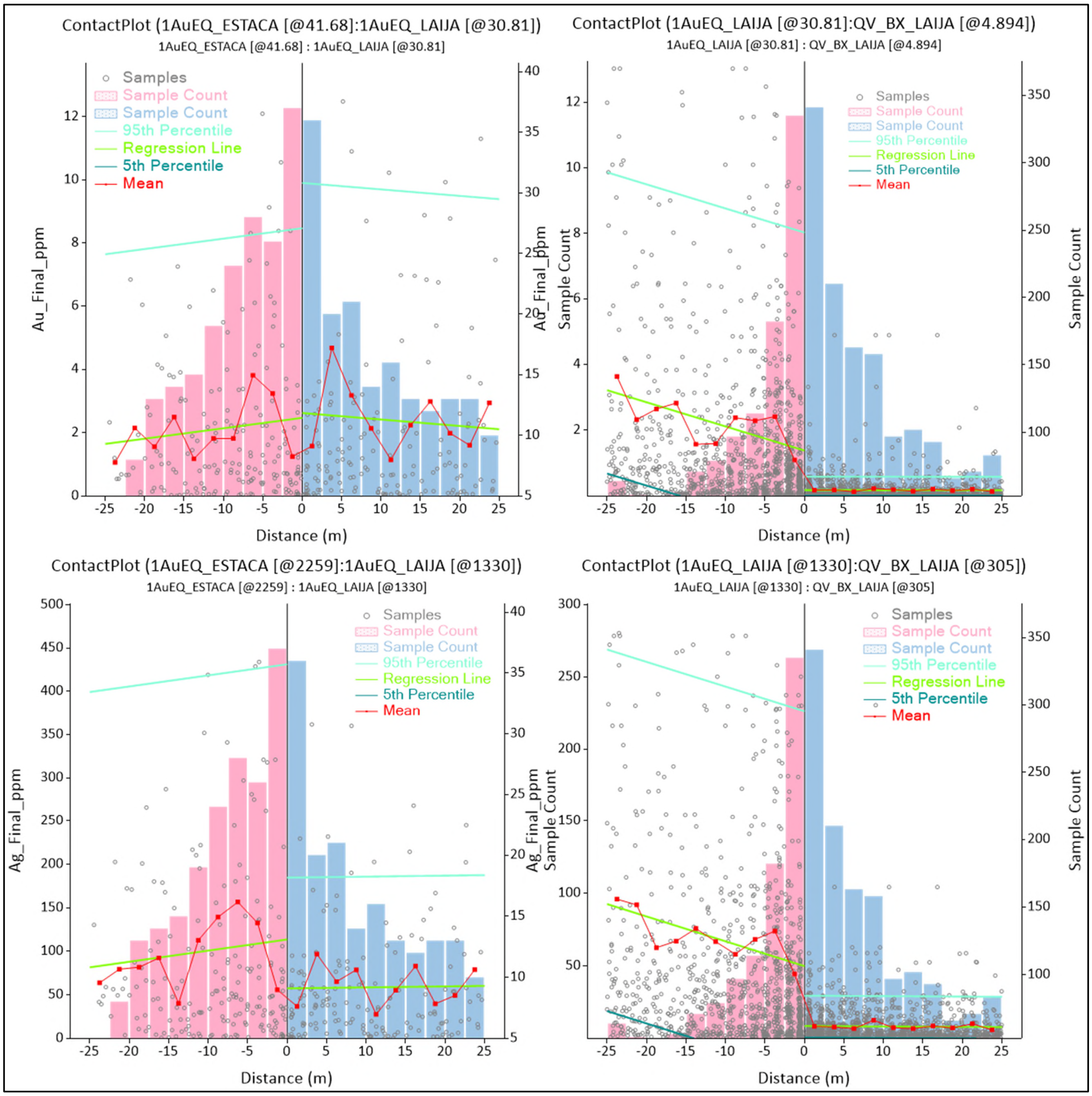


Table 14-9 Contact analysis summary for domains in 2.5x2.5x2.5m block models used for underground optimization

Domain Group	Au_Domain	Soft Boundary	Soft Boundary search max. (m)	Comment
QV_BX Mineralized	1AuEQ_ESTACA	1AuEQ_LAIJA, 1AuEQ_SM_SN	30	Laija and SM/SN are antithetic to Estaca but part of the same vein system. Half pass 1 search dir1 distance used.
	1AuEQ_FRE	-	N/A	Hard boundary
	1AuEQ_GUAD_NW	-	N/A	Hard boundary
	1AuEQ_GW	-	N/A	Hard boundary
	1AuEQ_LAIJA	1AuEQ_Estaca	30	Laija veins are antithetic to Estaca but part of same system. Half pass 1 search dir1 distance used.
	1AuEQ_MAR	-	N/A	Hard boundary
	1AuEQ_NB_SME	1AuEQ_SME_SPLAYS	30	SME footwall splays off main NB_SME structure. Half pass 1 search dir1 distance used.
	1AuEQ_SM_SN	1AuEQ_Estaca	30	SM/SN veins are antithetic to Estaca but part of same system. Half pass 1 search dir1 distance used.
	1AuEQ_SME_SPLAYS	1AuEQ_NB_SME	30	SME footwall splays off main NB_SME structure. Half pass 1 search dir1 distance used.
	1AuEQ_SMW	-	N/A	Hard boundary
	1AuEQ_TA	1AuEQ_ZS	120	Full search pass 2 search direction 1 distance used (no boundary). Very few samples available for contact analysis but TA, ZS, and ZN are part of the same structure and are only separated for estimation due to changes in the strike/dip of the ZT structure.
	1AuEQ_ZN	1AuEQ_ZS	120	
	1AuEQ_ZS	1AuEQ_TA, 1AuEQ_ZS	120	
QV_BX Non-Mineralized	QV_BX_ESTACA	-	N/A	Hard boundary
	QV_BX_FRE	-	N/A	Hard boundary
	QV_BX_GUAD_NW	-	N/A	Hard boundary
	QV_BX_GW	-	N/A	Hard boundary
	QV_BX_LAIJA	-	N/A	Hard boundary
	QV_BX_LP	-	N/A	Hard boundary
	QV_BX_NB_SME	-	N/A	Hard boundary
	QV_BX_SM_SN	-	N/A	Hard boundary
	QV_BX_SME_SPLAYS	-	N/A	Hard boundary
	QV_BX_ZTM	-	N/A	Hard boundary
Background	BACKGROUND_GUAD_LP	-	N/A	Hard boundary
	BACKGROUND_ZTM_NB_SM	-	N/A	Hard boundary

Outlier Management and Topcut Strategy

Capping analysis was completed for Au and Ag across all estimation domains in the 5x5x5m and 2.5x2.5x2.5m block models, using histograms, mean-variance plots, cumulative metal plots, and disintegration analysis considering step changes of 10% and 15% between the assay values of adjacent data points on log-probability plots. Specific methodology for each block model set is described below.

5x5x5m Block Models

Capping analysis was completed on 3 metre composited data for each estimation domain in the 5x5x5m block models, using the methods described above (Figures 14-14 and 14-15). Capped samples were then evaluated in 3D within each domain to ensure that the samples were not clustered and represented true outliers. ID3 estimates were also completed within each mineralized domain (02AuEQ prefix), using both the capped and uncapped datasets to assess the impact to average grade and contained metal (Tables 14-10 and 14-11).

2.5x2.5x2.5m Block Models

Capping analysis was completed on 1.5 metre composited data for each estimation domain in the 2.5x2.5x2.5m block models, using the same methods as for the 5x5x5m models (Figures 14-16 and 14-17). Capped samples were then evaluated in 3D within each domain to ensure that the samples were not clustered and represented true outliers. ID3 estimates were also completed within each mineralized domain (1AuEQ prefix), using both the capped and uncapped datasets to assess the impact to average grade and contained metal (Tables 14-12 and 14-13).

Figure 14-14 Gold topcut analysis for the 02AuEQ_ESTACA estimation domain

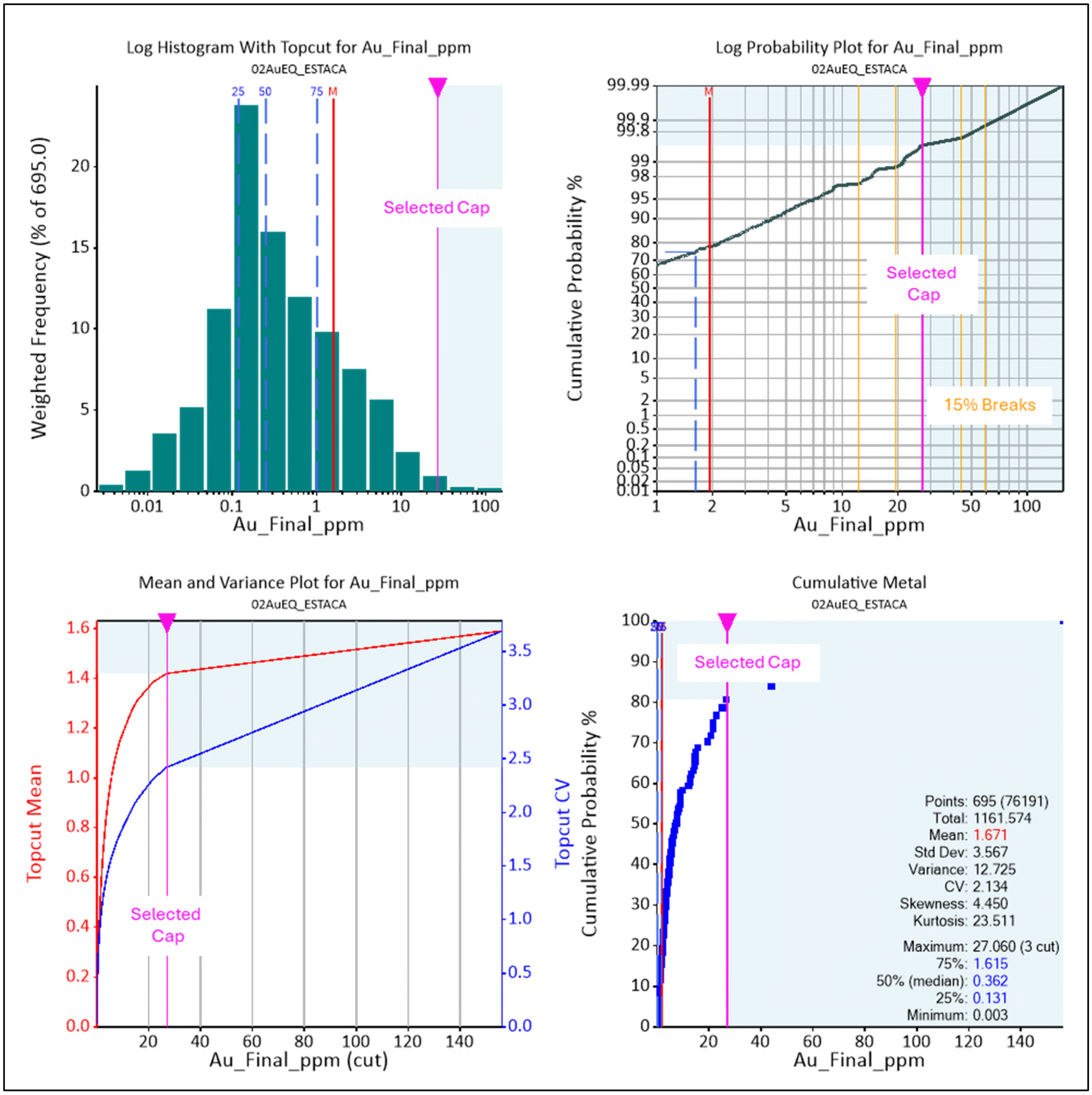


Figure 14-15 Silver topcut analysis for the 02AuEQ_NB_SME estimation domain

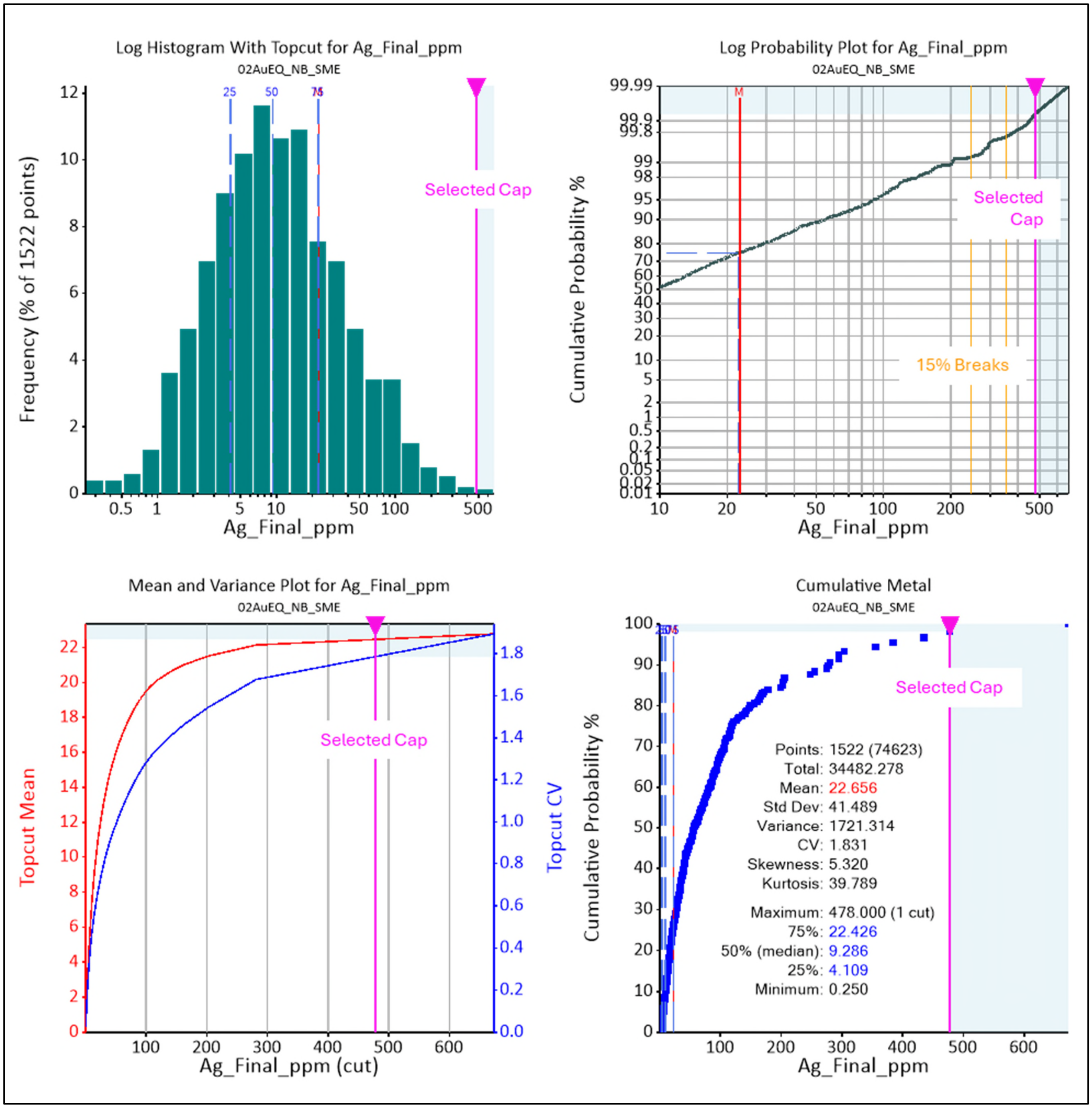


Table 14-10 Gold topcut statistics for mineralized domains used for estimation in 5x5x5m block models

Domain	3m Composite Statistics: Au (g/t)									Au (g/t) ID3 Estimate Mean Comparison (Block Model)			
	Max Uncapped (g/t)	Cap (g/t)	Percentile	Total samples	Capped samples	Mean Uncapped	Mean Capped	CV Uncapped	CV Capped	Capped (g/t)	Uncapped (g/t)	Lost (%)	Total Domain Tonnes
02AuEQ_ESTACA	156.29	27.06	99.6%	695	3	1.93	1.67	3.73	2.13	1.72	2.00	-16.0%	4,617,637
02AuEQ_FRE	5.29	5.29	100.0%	385	0	0.37	0.37	1.24	1.24	0.36	0.36	0.0%	12,292,862
02AuEQ_GUAD_NW	12.97	10.76	98.8%	86	1	0.59	0.56	3.14	3.00	0.28	0.28	0.0%	373,632
02AuEQ_GW	14.70	12.60	99.5%	433	2	0.57	0.57	1.99	1.91	0.39	0.39	-0.3%	3,467,924
02AuEQ_LAIJA	39.63	22.15	99.8%	843	2	1.40	1.37	2.24	2.07	1.12	1.15	-2.5%	4,747,290
02AuEQ_LP	22.81	5.00	99.7%	351	1	0.50	0.45	2.75	1.58	0.39	0.41	-6.5%	7,405,638
02AuEQ_MAR	16.22	14.63	99.5%	201	1	0.65	0.64	2.71	2.64	0.63	0.64	-1.1%	3,298,861
02AuEQ_NB_SME	32.61	15.65	99.9%	1549	2	0.54	0.53	2.54	2.22	0.43	0.44	-0.9%	17,259,106
02AuEQ_SM_SN	8.35	7.41	98.8%	165	2	0.55	0.54	2.08	2.03	0.82	0.82	0.0%	1,589,349
02AuEQ_SME_SPLAYS	7.21	5.00	99.2%	245	2	0.41	0.40	2.20	2.10	0.38	0.40	-3.9%	1,766,573
02AuEQ_SMW	44.95	20.63	97.2%	143	4	1.22	1.01	4.05	3.41	0.69	0.79	-15.1%	1,402,616
02AuEQ_TA	19.85	14.57	99.8%	1097	2	0.46	0.46	2.65	2.53	0.43	0.44	-0.5%	16,836,605
02AuEQ_ZN	57.58	29.06	99.9%	2647	3	0.77	0.76	2.76	2.47	0.57	0.58	-0.9%	19,192,879
02AuEQ_ZS	17.85	15.77	99.9%	1685	1	0.82	0.82	2.12	2.10	0.62	0.62	0.0%	15,257,969
02AuEQ_ZW	4.42	4.42	100.0%	33	0	0.41	0.41	1.80	1.80	0.40	0.40	-0.8%	1,826,828

Table 14-11 Silver topcut statistics for mineralized domains used for estimation in 5x5x5m block models

Domain	3m Composite Statistics: Ag (g/t)									Ag (g/t) ID3 Estimate Mean Comparison (Block Model)			
	Max Uncapped (g/t)	Cap (g/t)	Percentile	Total samples	Capped samples	Mean Uncapped	Mean Capped	CV Uncapped	CV Capped	Capped (g/t)	Uncapped (g/t)	Lost (%)	Total Domain Tonnes
02AuEQ_ESTACA	3001.87	2260.00	99.9%	695	1	107.07	106.00	2.35	2.28	110.37	110.98	-0.5%	4,617,637
02AuEQ_FRE	168.54	67.40	99.7%	385	1	7.04	6.78	1.72	1.38	7.03	7.16	-1.9%	12,292,862
02AuEQ_GUAD_NW	407.69	261.80	98.8%	86	1	23.44	21.75	2.40	2.12	14.77	14.77	0.0%	373,632
02AuEQ_GW	405.70	405.70	100.0%	433	0	19.90	19.90	1.48	1.48	19.17	19.16	0.0%	3,467,924
02AuEQ_LAIJA	2461.49	1400.00	99.8%	843	2	47.57	45.73	2.99	2.55	45.05	46.37	-2.9%	4,747,290
02AuEQ_LP	857.41	615.00	99.1%	351	3	23.40	22.44	3.06	2.74	16.98	17.01	-0.2%	7,405,638
02AuEQ_MAR	142.60	142.60	100.0%	201	0	10.49	10.49	1.08	1.08	10.55	10.55	0.0%	3,298,861
02AuEQ_NB_SME	673.37	478.00	99.9%	1522	1	22.78	22.66	1.89	1.83	20.64	20.73	-0.5%	17,259,106
02AuEQ_SM_SN	641.92	388.50	99.4%	165	1	30.34	28.80	2.56	2.34	47.75	50.44	-5.6%	1,589,349
02AuEQ_SME_SPLAYS	584.08	523.00	99.6%	245	1	32.76	32.51	2.13	2.09	29.19	29.60	-1.4%	1,766,573
02AuEQ_SMW	431.90	376.00	99.3%	143	1	21.56	21.16	2.56	2.47	14.89	15.06	-1.1%	1,402,616
02AuEQ_TA	1076.72	538.00	99.8%	1097	2	27.71	26.96	2.21	1.90	25.75	27.13	-5.4%	16,836,605
02AuEQ_ZN	332.85	332.85	100.0%	2327	0	13.56	13.56	0.92	0.92	12.78	12.78	0.0%	19,192,879
02AuEQ_ZS	281.20	281.20	100.0%	1478	0	20.61	20.61	1.11	1.11	18.82	18.83	-0.1%	15,257,969
02AuEQ_ZW	41.88	41.88	100.0%	33	0	5.65	5.65	1.26	1.26	5.07	5.07	-0.1%	1,826,828

Figure 14-16 Gold topcut analysis for the 1AuEQ_ZS estimation domain

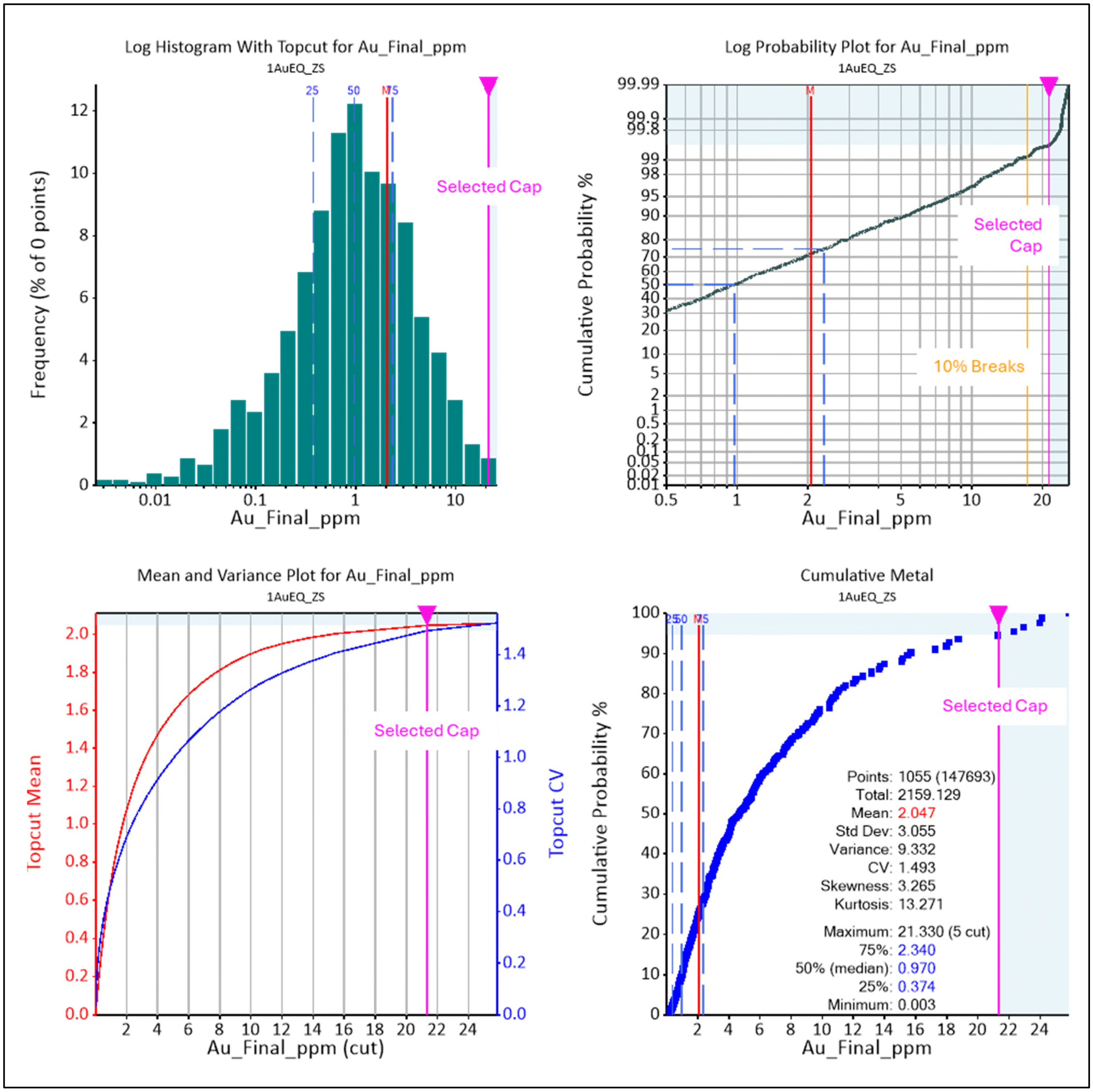


Figure 14-17 Silver topcut analysis for the 1AuEQ_LAIJA estimation domain

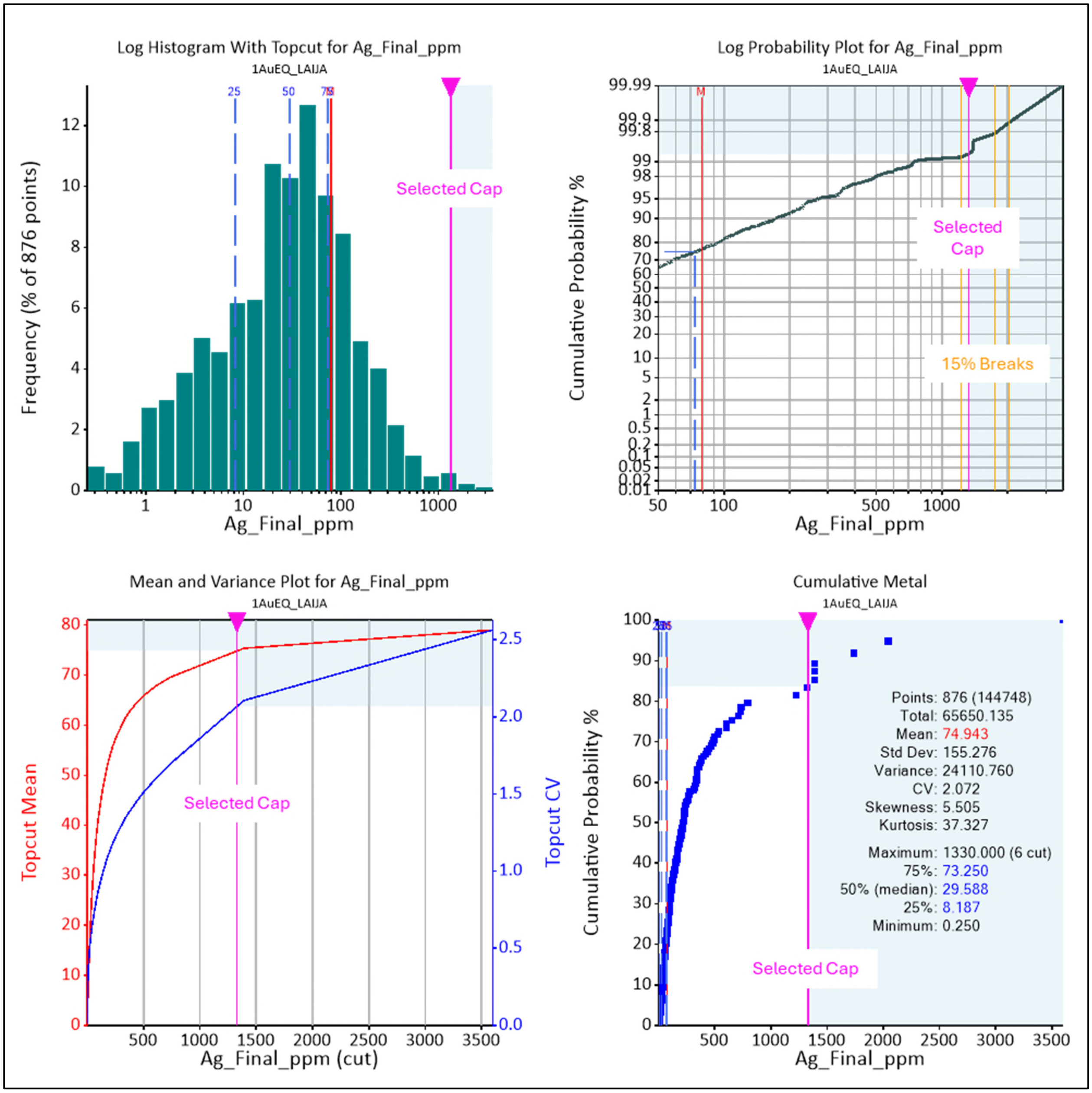


Table 14-12 Gold topcut statistics for mineralized domains used for estimation in 2.5x2.5x2.5m block models

Domain	1.5m Composite Statistics: Au (g/t)									Au (g/t) ID3 Estimate Mean Comparison (Block Model)			
	Max Uncapped (g/t)	Cap (g/t)	Percentile	Total samples	Capped samples	Mean Uncapped	Mean Capped	CV Uncapped	CV Capped	Capped (g/t)	Uncapped (g/t)	Lost (%)	Total Domain Tonnes
1AuEQ_ESTACA	156.29	41.68	99.6%	733	3	3.04	2.75	2.86	1.88	2.73	3.03	-11.2%	3,661,777
1AuEQ_GW	29.17	15.18	99.1%	213	2	1.43	1.36	1.77	1.41	1.23	1.28	-4.3%	677,077
1AuEQ_LAIJA	48.23	30.81	99.3%	876	6	2.36	2.30	1.95	1.81	2.02	2.09	-3.8%	2,981,499
1AuEQ_GUAD_NW	2.21	2.21	100.0%	5	0	0.51	0.51	1.67	1.67	0.39	0.39	-0.3%	88,677
1AuEQ_MAR	37.10	20.28	97.5%	79	2	2.23	1.98	2.35	1.94	1.81	2.05	-13.1%	1,122,359
1AuEQ_NB_SME	36.66	28.16	99.8%	802	2	1.44	1.43	1.95	1.87	1.24	1.24	-0.5%	5,182,339
1AuEQ_LP	32.64	13.00	99.4%	166	1	1.16	1.04	2.58	1.89	0.92	1.00	-9.1%	1,957,599
1AuEQ_FRE	5.79	5.79	100.0%	70	0	0.98	0.98	1.26	1.26	0.89	0.89	0.0%	1,310,731
1AuEQ_SM_SN	14.56	11.56	95.5%	44	2	1.90	1.77	1.79	1.66	1.58	1.64	-3.8%	542,463
1AuEQ_SME_SPLAYS	13.03	8.42	99.0%	98	1	1.37	1.32	1.50	1.38	1.43	1.52	-6.5%	385,872
1AuEQ_SMW	46.46	31.56	91.7%	36	3	7.68	6.79	1.67	1.55	7.70	8.70	-12.9%	117,826
1AuEQ_TA	38.78	18.61	99.8%	538	1	1.26	1.22	2.22	1.96	1.04	1.06	-1.4%	7,509,531
1AuEQ_ZN	60.23	37.03	99.8%	1264	3	2.30	2.27	1.86	1.74	1.80	1.81	-1.1%	5,475,724
1AuEQ_ZS	25.84	21.33	99.5%	1055	5	2.06	2.05	1.52	1.49	1.73	1.74	-0.6%	5,512,418
1AuEQ_ZW	6.68	6.68	100.0%	5	0	2.13	2.13	1.11	1.11	1.68	1.68	0.0%	46,866

Table 14-13 Silver topcut statistics for mineralized domains used for estimation in 2.5x2.5x2.5m block models

Domain	1.5m Composite Statistics: Ag (g/t)									Ag (g/t) ID3 Estimate Mean Comparison (Block Model)			
	Max Uncapped (g/t)	Cap (g/t)	Percentile	Total samples	Capped samples	Mean Uncapped	Mean Capped	CV Uncapped	CV Capped	Capped (g/t)	Uncapped (g/t)	Lost (%)	Total Domain Tonnes
1AuEQ_ESTACA	3189.53	2259.00	99.3%	733	5	173.54	170.09	2.00	1.89	170.66	172.98	-1.4%	3,661,777
1AuEQ_GW	169.20	169.20	100.0%	70	0	23.99	23.99	1.33	1.33	18.60	18.60	0.0%	677,077
1AuEQ_LAIJA	256.00	256.00	99.5%	213	1	32.31	31.84	1.24	1.15	39.82	40.19	-0.9%	2,981,499
1AuEQ_GUAD_NW	3599.28	1330.00	99.3%	876	6	79.02	74.94	2.56	2.07	80.97	84.08	-3.8%	88,677
1AuEQ_MAR	37.20	37.20	100.0%	5	0	15.75	15.75	0.87	0.87	21.41	21.41	0.0%	1,122,359
1AuEQ_NB_SME	1019.81	868.00	98.8%	166	2	55.50	54.58	2.10	2.00	38.82	39.88	-2.7%	5,182,339
1AuEQ_LP	267.50	267.50	100.0%	79	0	20.96	20.96	1.42	1.42	20.96	20.96	0.0%	1,957,599
1AuEQ_FRE	1210.96	575.00	99.7%	788	2	58.99	58.15	1.46	1.34	57.69	58.80	-1.9%	1,310,731
1AuEQ_SM_SN	1282.59	399.00	97.7%	44	1	106.98	86.90	2.00	1.45	74.08	83.83	-13.2%	542,463
1AuEQ_SME_SPLAYS	1055.71	561.00	99.0%	98	1	104.53	99.48	1.47	1.29	106.34	116.23	-9.3%	385,872
1AuEQ_SMW	648.86	386.00	97.2%	36	1	89.79	82.49	1.40	1.19	87.68	95.05	-8.4%	117,826
1AuEQ_TA	1399.32	730.00	99.3%	538	4	74.90	73.60	1.56	1.43	74.67	76.59	-2.6%	7,509,531
1AuEQ_ZN	174.20	174.20	100.0%	1147	0	23.77	23.77	0.65	0.65	24.38	24.38	0.0%	5,475,724
1AuEQ_ZS	377.95	377.95	100.0%	877	0	40.39	40.39	0.87	0.87	42.96	42.96	0.0%	5,512,418
1AuEQ_ZW	67.00	67.00	100.0%	5	0	21.76	21.76	1.05	1.05	17.29	17.29	0.0%	46,866

14.3.5 *Variography*

Variography was completed for Au and Ag within mineralized estimation domains using Snowden Supervisor v.8.15 and was completed independently for domains estimated in the 5x5x5m and 2.5x2.5x2.5m block models. Variogram modelling was completed on normal scores-transformed data and variograms were modeled using as few structures as possible, with a nugget obtained from down hole variograms and generally 2 spherical structures used. The back-transformation of normal scores variograms to original units was then completed for Au and Ag variograms in each domain using 90 Hermite polynomials, and the orientation of the variograms were checked against the mineralization orientation for each domain in 3D prior to use in estimation. Search orientations determined from variography were used in both the OK estimates and in the final ID3 estimates used for resource reporting.

5x5x5m Block Models

Experimental variograms were calculated from capped 3 metre composites for mineralized domains (02AuEQ prefix) estimated in the 5x5x5m block models. Examples from several domains are shown in Figures 14-18 and 14-19, with results for all domains presented in Tables 14-12 through 14-13.

2.5x2.5x2.5m Block Models

Experimental variograms were calculated from capped 1.5 metre composites for Au and Ag in mineralized domains (1AuEQ prefix) estimated in the 2.5x2.5x2.5m block models. Examples from several domains are shown in Figures 14-20 through 14-21, with results for all domains presented in Tables 14-13 through 14-14.

Figure 14-18 Normal scores variography and backtransform model for gold estimation in the 02AuEQ_ZS domain

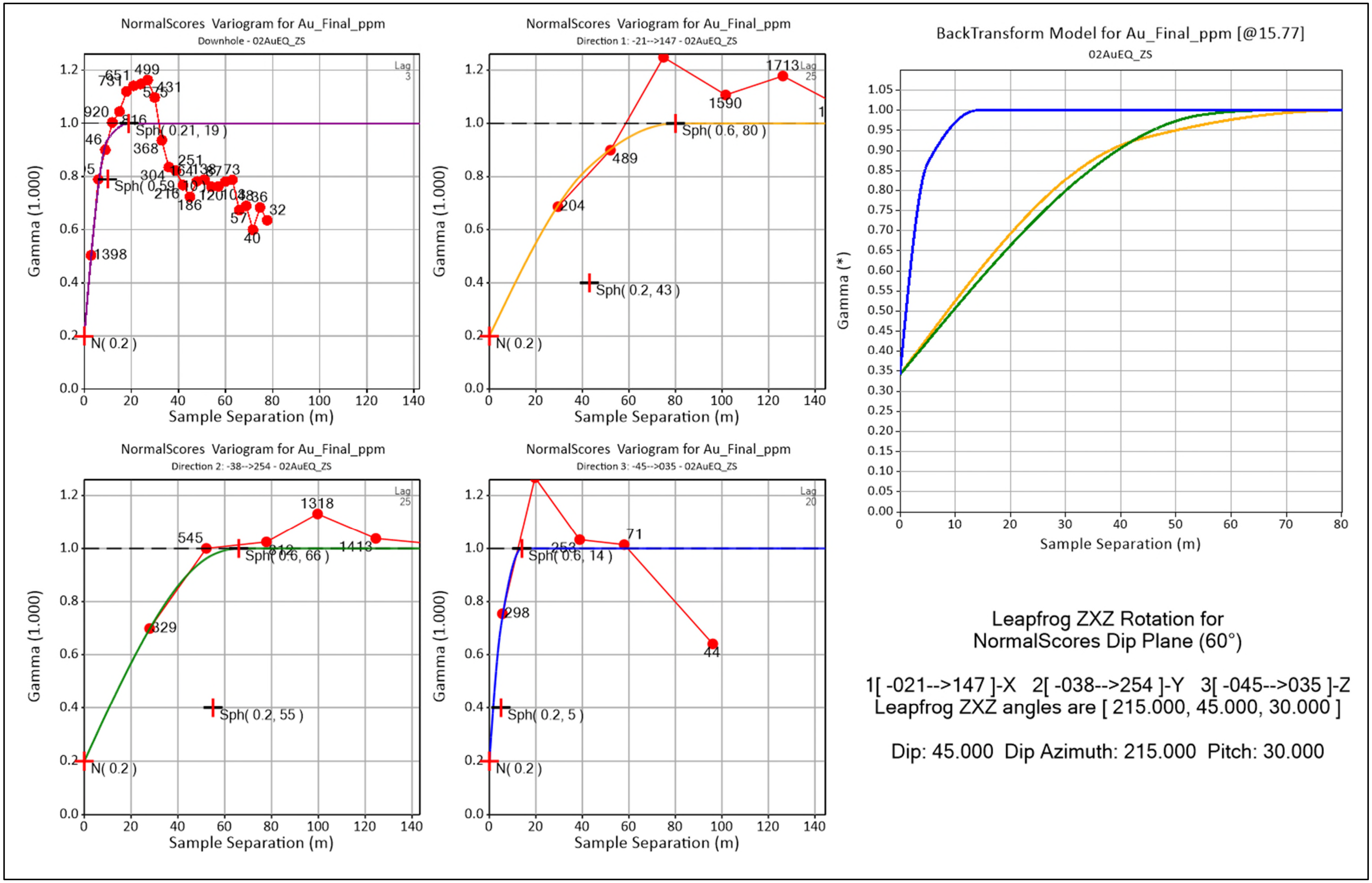


Figure 14-19 Normal scores variography and backtransform model for silver estimation in the 02AuEQ_ESTACA domain

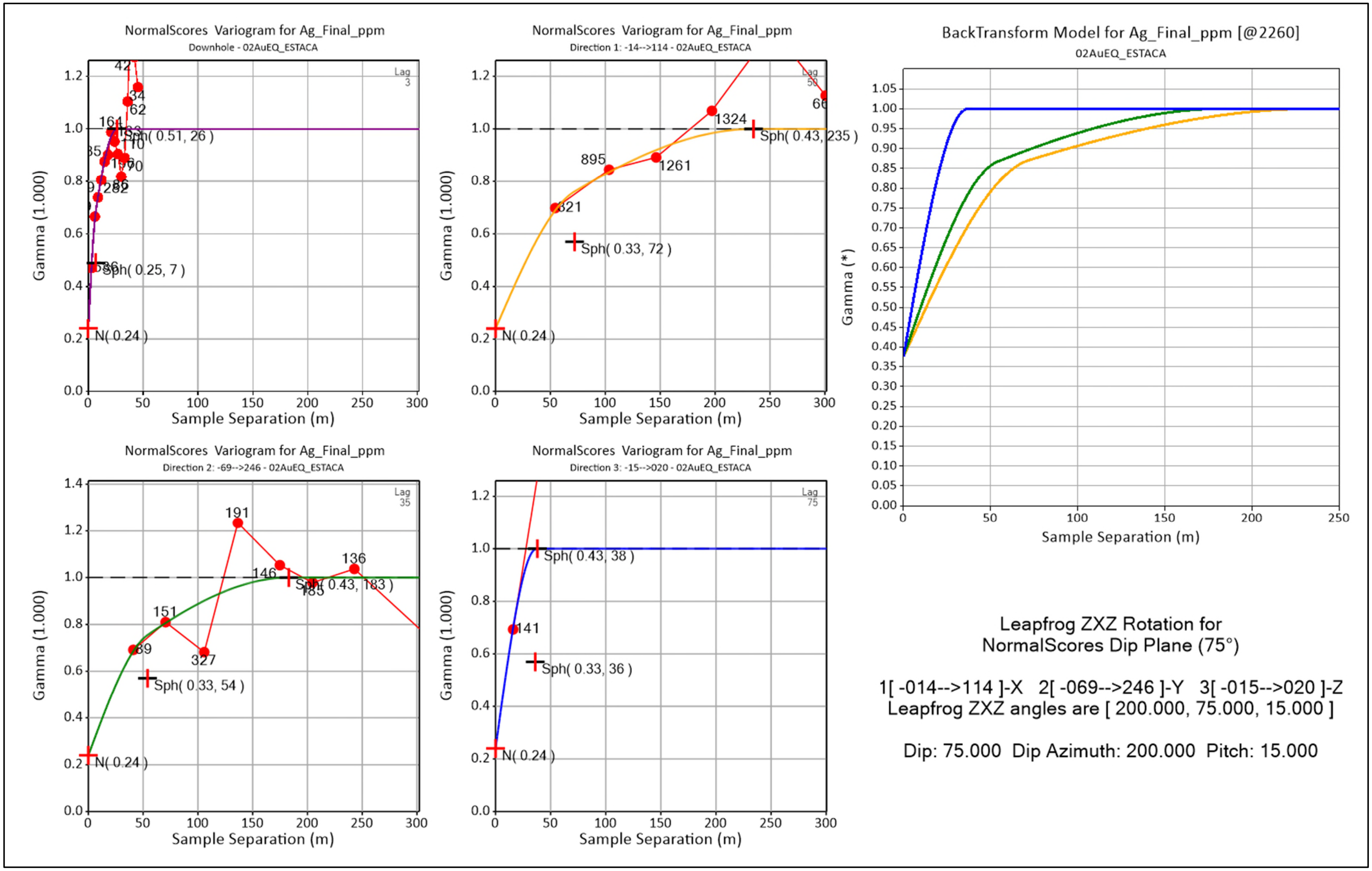


Table 14-14 Gold variogram parameters for mineralized domains used for estimation in 5x5x5m block models

	Rotation – Snowden Supervisor				Structure 1					Structure 2				
Domain	**Horizontal**	**Across Strike**	**Dip Plane**	**Nugget**	**Type**	**Normalized Sill**	**Major (m)**	**Semi-Major (m)**	**Minor (m)**	**Type**	**Normalized Sill**	**Major (m)**	**Semi-Major (m)**	**Minor (m)**
02AuEQ_ESTACA	110	195	75	0.372	Spherical	0.389	89	72	25	Spherical	0.239	145	164	33
02AuEQ_FRE	135	215	70	0.313	Spherical	0.437	120	129	12	Spherical	0.25	216	262	13
02AuEQ_GW	100	30	100	0.351	Spherical	0.417	53	36	13	Spherical	0.232	107	44	35
02AuEQ_LAIJA	305	200	310	0.377	Spherical	0.391	26	29	21	Spherical	0.233	64	45	22
02AuEQ_GUAD_NW	325	180	90	0.434	Spherical	0.566	132	132	20	-	-	-	-	-
02AuEQ_LP	310	190	150	0.326	Spherical	0.356	154	81	51	Spherical	0.319	189	82	85
02AuEQ_MAR	310	135	315	0.405	Spherical	0.595	97	52	40	-	-	-	-	-
02AuEQ_NB_SME	145	210	50	0.343	Spherical	0.563	78	69	16	Spherical	0.0942	120	75	25
02AuEQ_SM_SN	305	225	270	0.33	Spherical	0.67	120	120	13	-	-	-	-	-
02AuEQ_SME_SPLAYS	285	145	105	0.349	Spherical	0.651	50	50	7	-	-	-	-	-
02AuEQ_SMW	100	210	70	0.533	Spherical	0.467	86	86	10	-	-	-	-	-
02AuEQ_TA	150	220	55	0.318	Spherical	0.521	95	53	3	Spherical	0.162	111	128	10
02AuEQ_ZN	165	220	55	0.31	Spherical	0.531	27	36	7	Spherical	0.159	60	38	20
02AuEQ_ZS	125	225	60	0.318	Spherical	0.371	43	55	5	Spherical	0.311	80	66	14
02AuEQ_ZW	120	210	90	0.411	Spherical	0.589	40	40	10	-	-	-	-	-

Notes:

Nugget and normalized sill values from back-transformed normal scores variograms.

Table 14-15 Silver variogram parameters for mineralized domains used for estimation in 5x5x5m block models

	Rotation – Snowden Supervisor				Structure 1					Structure 2				
Domain	Horizontal	Across Strike	Dip Plane	Nugget	Type	Normalized Sill	Major (m)	Semi-Major (m)	Minor (m)	Type	Normalized Sill	Major (m)	Semi-Major (m)	Minor (m)
02AuEQ_ESTACA	110	195	75	0.375	Spherical	0.392	72	54	36	Spherical	0.233	235	183	38
02AuEQ_FRE	130	215	60	0.346	Spherical	0.382	118	176	9	Spherical	0.272	416	224	24
02AuEQ_GW	100	30	100	0.4	Spherical	0.435	47	68	26	Spherical	0.164	151	180	44
02AuEQ_LAIJA	305	200	310	0.454	Spherical	0.378	26	40	29	Spherical	0.168	92	56	31
02AuEQ_GUAD_NW	325	180	90	0.335	Spherical	0.665	40	40	20	-	-	-	-	-
02AuEQ_LP	310	190	150	0.413	Spherical	0.421	83	51	147	Spherical	0.165	144	96	148
02AuEQ_MAR	310	135	315	0.236	Spherical	0.447	75	49	20	Spherical	0.317	82	56	43
02AuEQ_NB_SME	145	210	50	0.196	Spherical	0.543	66	72	11	Spherical	0.261	335	159	60
02AuEQ_SM_SN	305	225	270	0.352	Spherical	0.648	102	102	13	-	-	-	-	-
02AuEQ_SME_SPLAYS	285	145	105	0.331	Spherical	0.669	65	70	18	-	-	-	-	-
02AuEQ_SMW	100	210	70	0.191	Spherical	0.809	110	137	18	-	-	-	-	-
02AuEQ_TA	150	220	55	0.19	Spherical	0.609	48	41	10	Spherical	0.201	135	79	30
02AuEQ_ZN	165	220	55	0.239	Spherical	0.312	19	47	9	Spherical	0.449	113	121	35
02AuEQ_ZS	130	225	40	0.194	Spherical	0.576	73	76	9	Spherical	0.23	351	199	13
02AuEQ_ZW	120	210	90	0.351	Spherical	0.649	40	40	20	-	-	-	-	-

Notes:

Nugget and normalized sill values from back-transformed normal scores variograms.

Figure 14-20 Normal scores variography and backtransform model for gold estimation in the 1AuEQ_NB_SME domain

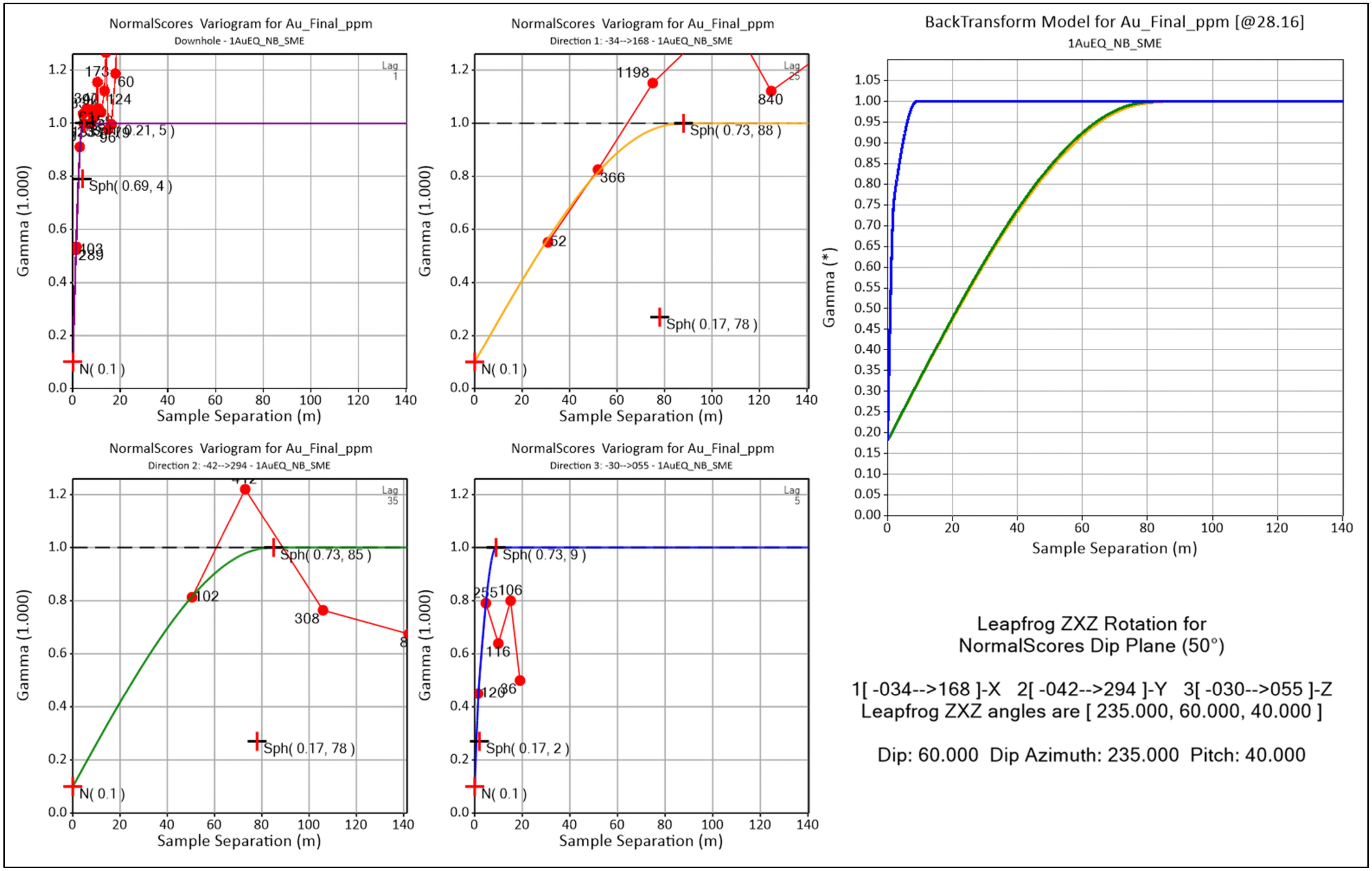


Figure 14-21 Normal scores variography and backtransform model for silver estimation in the 1AuEQ_TA domain

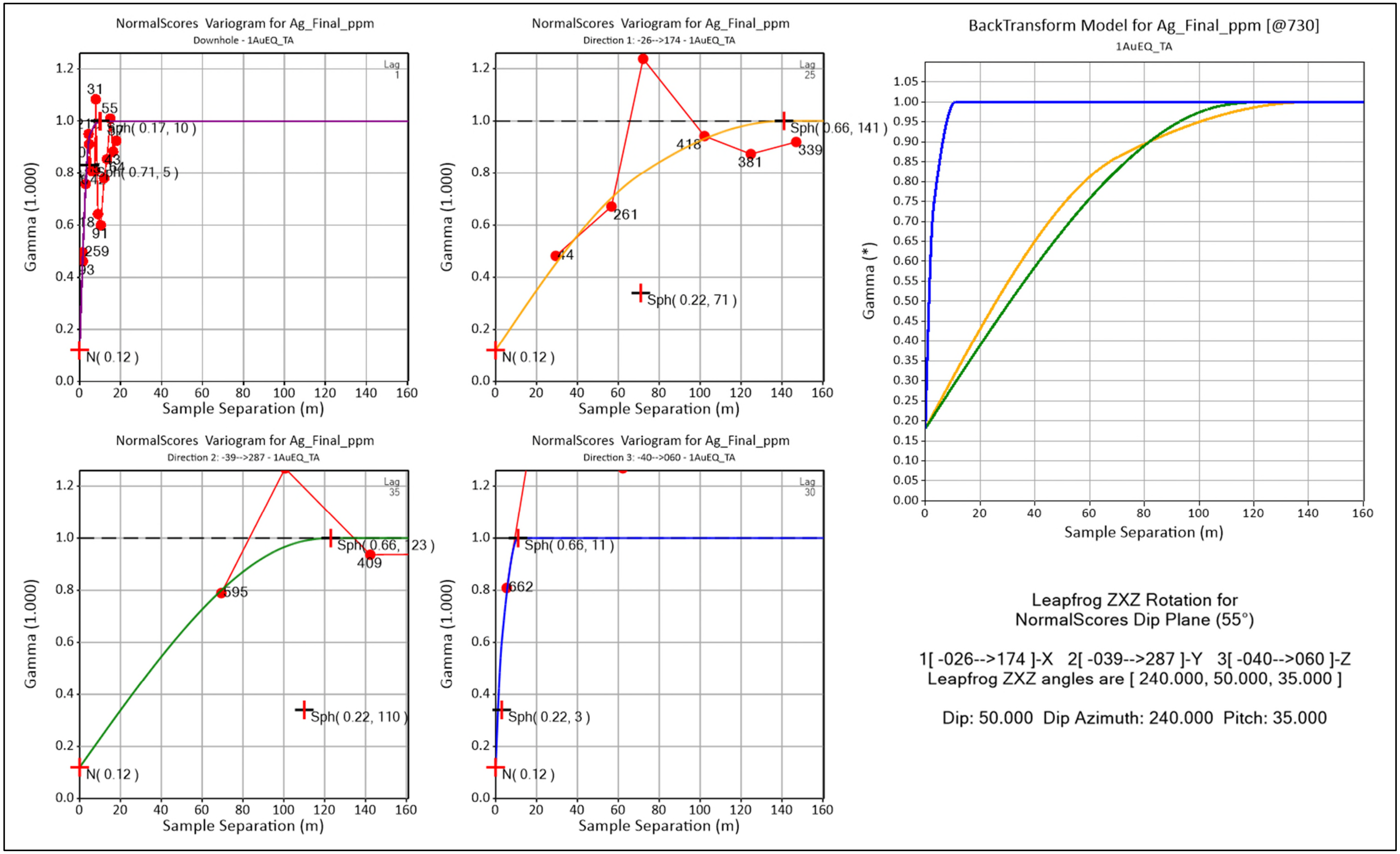


Table 14-16 Gold variogram parameters for mineralized domains used for estimation in 2.5x2.5x2.5m block models

	Rotation – Snowden Supervisor				Structure 1					Structure 2				
Domain	Horizontal	Across Strike	Dip Plane	Nugget	Type	Normalized Sill	Major (m)	Semi-Major (m)	Minor (m)	Type	Normalized Sill	Major (m)	Semi-Major (m)	Minor (m)
1AuEQ_ESTACA	110	195	75	0.28	Spherical	0.464	52	60	27	Spherical	0.257	111	65	28
1AuEQ_FRE	135	215	70	0.24	Spherical	0.76	183	183	10	-	-	-	-	-
1AuEQ_GW	100	30	100	0.265	Spherical	0.735	79	52	17	-	-	-	-	-
1AuEQ_LAIJA	300	200	310	0.295	Spherical	0.534	34	42	19	Spherical	0.171	59	43	20
1AuEQ_GUAD_NW	325	180	90	0.3	Spherical	0.7	40	40	10	-	-	-	-	-
1AuEQ_LP	310	190	150	0.349	Spherical	0.651	140	140	15	-	-	-	-	-
1AuEQ_MAR	310	135	315	0.326	Spherical	0.674	80	80	15	-	-	-	-	-
1AuEQ_NB_SME	145	210	50	0.181	Spherical	0.472	78	78	2	Spherical	0.347	88	85	9
1AuEQ_SM_SN	305	225	270	0.3	Spherical	0.7	40	40	10	-	-	-	-	-
1AuEQ_SME_SPLAYS	285	145	105	0.236	Spherical	0.764	50	50	5	-	-	-	-	-
1AuEQ_SMW	100	210	70	0.3	Spherical	0.7	40	40	10	-	-	-	-	-
1AuEQ_TA	150	220	55	0.267	Spherical	0.452	61	61	6	Spherical	0.281	81	102	9
1AuEQ_ZN	165	220	55	0.254	Spherical	0.468	43	25	3	Spherical	0.277	47	29	7
1AuEQ_ZS	125	225	60	0.198	Spherical	0.533	34	18	4	Spherical	0.269	80	40	10
1AuEQ_ZW	120	210	90	0.411	Spherical	0.589	40	40	10	-	-	-	-	-

Notes:

Nugget and normalized sill values from back-transformed normal scores variograms.

Table 14-17 Silver variogram parameters for mineralized domains used for estimation in 2.5x2.5x2.5m block models

	Rotation – Snowden Supervisor				Structure 1					Structure 2				
Domain	Horizontal	Across Strike	Dip Plane	Nugget	Type	Normalized Sill	Major (m)	Semi-Major (m)	Minor (m)	Type	Normalized Sill	Major (m)	Semi-Major (m)	Minor (m)
1AuEQ_ESTACA	110	195	75	0.23	Spherical	0.545	54	54	12	Spherical	0.225	194	66	14
1AuEQ_FRE	135	215	70	0.246	Spherical	0.754	170	170	11	-	-	-	-	-
1AuEQ_GW	100	30	100	0.216	Spherical	0.409	46	63	7	Spherical	0.375	96	65	25
1AuEQ_LAIJA	300	200	310	0.369	Spherical	0.551	25	35	25	Spherical	0.0797	61	60	26
1AuEQ_GUAD_NW	325	180	90	0.3	Spherical	0.7	40	40	10	-	-	-	-	-
1AuEQ_LP	310	190	150	0.276	Spherical	0.724	97	97	15	-	-	-	-	-
1AuEQ_MAR	310	135	315	0.359	Spherical	0.641	127	127	20	-	-	-	-	-
1AuEQ_NB_SME	145	210	50	0.197	Spherical	0.423	72	28	8	Spherical	0.38	80	77	20
1AuEQ_SM_SN	305	225	270	0.3	Spherical	0.7	40	40	10	-	-	-	-	-
1AuEQ_SME_SPLAYS	285	145	105	0.139	Spherical	0.861	72	55	10	-	-	-	-	-
1AuEQ_SMW	100	210	70	0.19	Spherical	0.81	116	116	15	-	-	-	-	-
1AuEQ_TA	150	220	55	0.181	Spherical	0.381	71	110	3	Spherical	0.438	141	123	11
1AuEQ_ZN	165	220	55	0.142	Spherical	0.341	22	41	5	Spherical	0.518	59	53	17
1AuEQ_ZS	125	225	60	0.125	Spherical	0.373	33	26	4	Spherical	0.501	119	131	9
1AuEQ_ZW	120	210	90	0.351	Spherical	0.649	40	40	20	-	-	-	-	-

Notes:

Nugget and normalized sill values from back-transformed normal scores variograms.

14.3.6 *Block Model Set Up*

5x5x5m Block Models

Two 5x5x5m block models were constructed in Leapfrog EDGE v.2023.2.3, both in the WGS84 / UTM Zone 13 N coordinate system (Figure 14-22). The ZTM_NB_SM_5x5x5_Rotated model includes the Fresnillo, Mariposa, Noche Buena, San Miguel East, San Miguel West, Tahonitas, Zapote North, Zapote South, and Zapote West areas, and is rotated 30 degrees counterclockwise to match the dominant strike of mineralized structures in the western project area. The GUAD_LP_5x5x5_Rotated model includes the Guadalupe East, Guadalupe West, and Las Primas areas, and is rotated 20 degrees clockwise to match the dominant strike of mineralized structures in the eastern project area. Both models have a 5x5x5m regular block size. Table 14-16 shows block model parameters for both models.

Figure 14-22 Model extents for 5x5x5m block models

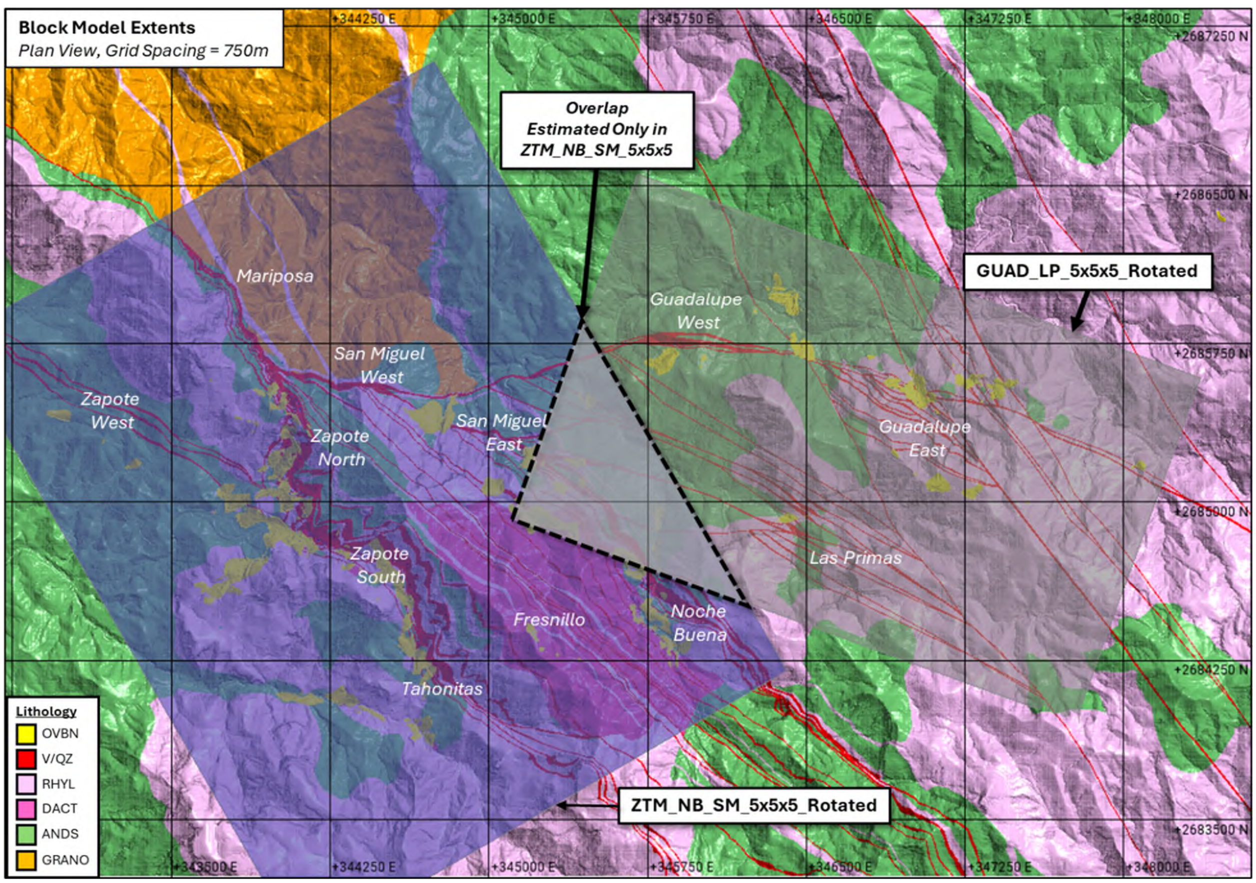


Table 14-18 Block model parameters for 5x5x5m block models

Model Build:	Leapfrog EDGE v.2023.2.3					
Coordinate System:	WGS84 / UTM Zone 13 N					
Model:	GUAD_LP_5x5x5_Rotated			ZTM_NB_SM_5x5x5_Rotated		
Rotation (azi/dip/pitch):	020/0/0			330/0/0		
Coordinate:	Easting (X)	Northing (Y)	Elevation (Z)	Easting (X)	Northing (Y)	Elevation (Z)
Block Size (m)	5	5	5	5	5	5
Min. Corner (m)	345,110	2,684,925	280	344,125	2,682,885	200
Min. Centroid (m)	348,359.5	2,685,586.0	282.5	344,741.1	2,687,082.9	202.5
Number of Blocks	566	347	174	527	666	160

2.5x2.5x2.5m Block Models

Six 2.5x2.5x2.5m block models were constructed in Leapfrog EDGE v.2023.2.3, all in the WGS84 / UTM Zone 13 N coordinate system (Figure 14-23). All models have a 2.5x2.5x2.5m parent block size and are sub-blocked to 1.25x1.25x1.25m along mineralized domain contacts (1AuEQ prefix) and along the contacts of the V/QZ solid from the Property lithology model. The FRE_NB_SME_2pt5_Octree_Rotated model includes the Fresnillo, Noche Buena, and San Miguel East areas, and is rotated 30 degrees counterclockwise to match the dominant strike of mineralized structures along the Central trend. The GE_2pt5_Octree_Rotated model includes the Guadalupe East area and is rotated 20 degrees clockwise to match the dominant strike of the Estaca and Laija veinsets. The GW_2pt5_Octree_Rotated model includes the Guadalupe West area and is rotated 10 degrees clockwise to match the dominant strike of the western extension of the Estaca vein. The LP_2pt5_Octree_Rotated model includes the Las Primas area and is rotated 26 degrees clockwise to match the dominant strike of the Las Primas veinset. The SMW_2pt5_Octree_Rotated model includes the San Miguel West area and is not rotated due to the generally east-west strike of the Central structure at San Miguel West. The ZTM_2pt5_Octree_Rotated model includes the Tahonitas, Mariposa, Zapote North, Zapote South, and Zapote West areas, and is rotated 30 degrees counterclockwise to match the dominant strike of mineralized structures along the Z-T trend. Figure 14-17 shows block model parameters for all 2.5x2.5x2.5m models.

Figure 14-23 Model extents for 2.5x2.5x2.5m block models

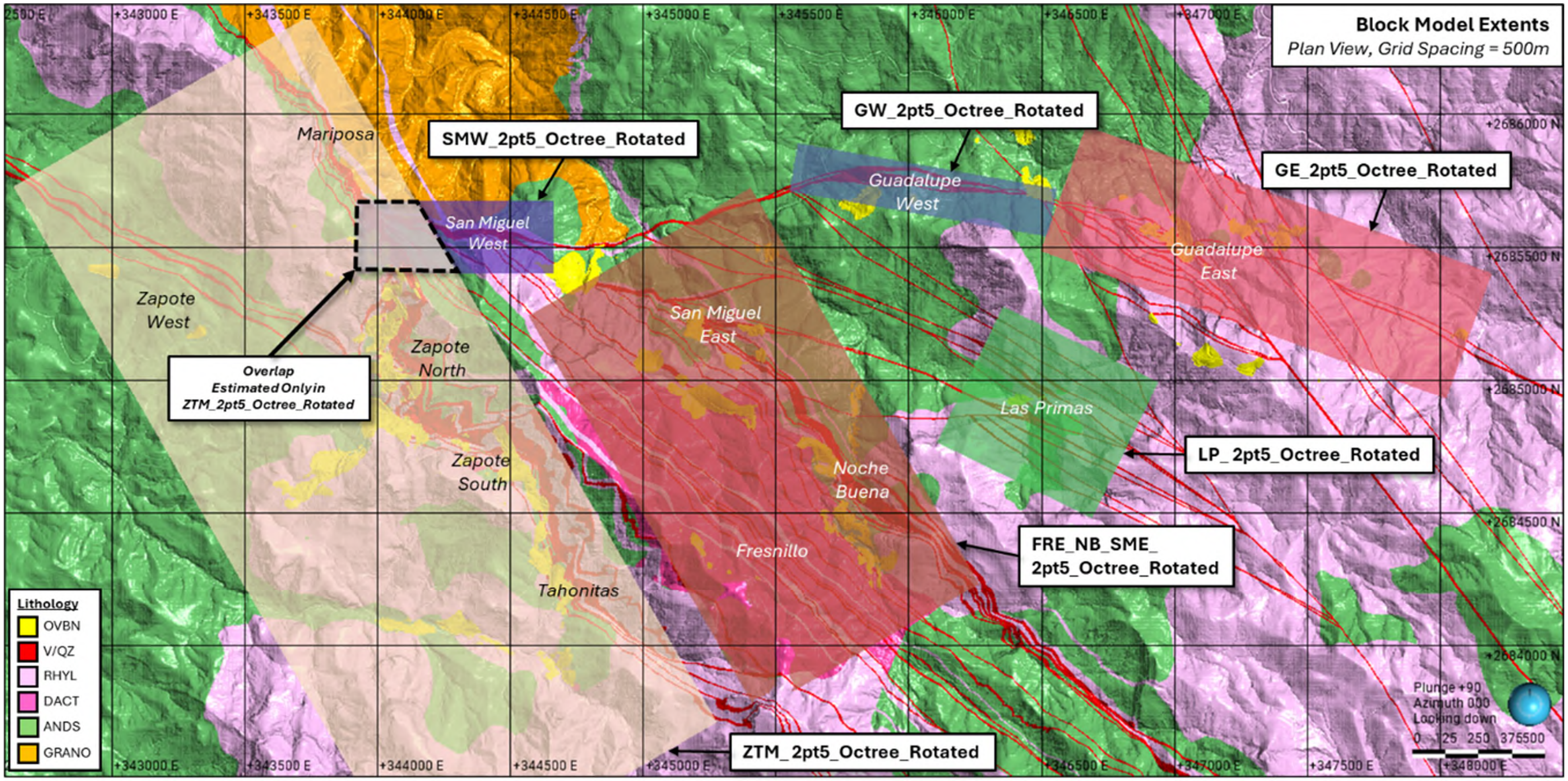


Table 14-19 Model parameters for 2.5x2.5x2.5m block models

Model Build:	Leapfrog EDGE v.2023.2.3								
Coordinate System:	WGS84 / UTM Zone 13 N								
Model:	FRE_NB_SME_2pt5_Octree_Rotated			GE_2pt5_Octree_Rotated			GW_2pt5_Octree_Rotated		
Rotation (azi/dip/pitch):	330/0/0			020/0/0			010/0/0		
Coordinate:	East (X)	North (Y)	Elev. (Z)	East (X)	North (Y)	Elev. (Z)	East (X)	North (Y)	Elev. (Z)
Parent Block Size (m)	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
Sub-blocks (Octree)	2	2	2	2	2	2	2	2	2
Min. Corner (m)	345,430	2,683,750	340	346,495	2,685,485	410	345,550	2,685,710	485
Min. Centroid (m)	345,430.45	2,683,751.70	341.25	346,496.60	2,685,485.70	411.25	345,551.40	2,685,711.00	486.25
Number of Blocks	386	689	226	650	201	272	396	74	166
Model Build:	Leapfrog EDGE v.2023.2.3								
Coordinate System:	WGS84 / UTM Zone 13 N								
Model:	LP_2pt5_Octree_Rotated			SMW_2pt5_Octree_Rotated			ZTM_2pt5_Octree_Rotated		
Rotation (azi/dip/pitch):	026/0/0			000/0/0			330/0/0		
Coordinate:	East (X)	North (Y)	Elev. (Z)	East (X)	North (Y)	Elev. (Z)	East (X)	North (Y)	Elev. (Z)
Parent Block Size (m)	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
Sub-blocks (Octree)	2	2	2	2	2	2	2	2	2
Min. Corner (m)	346,105	2,684,765	410	343,920	2,685,400	500	344,165	2,683,070	175
Min. Centroid (m)	346,106.67	2,684,765.57	411.25	343,921.13	2,685,401.10	501.25	344,165.45	2,683,071.70	176.25
Number of Blocks	260	288	248	298	110	108	514	1228	292

14.3.7 *Grade Interpolation*

Gold and silver grades were estimated by ID3, OK, and nearest neighbor (NN) in all mineralized domains for both the 5x5x5m and 2.5x2.5x2.5m block models. Search ellipse orientation and radii were selected based on variogram models for each individual estimation domain, with variable search orientation (VO) applied according to the nearest vein midpoint surface in the V/QZ. Initial search parameters for each domain were selected using Kriging Neighborhood Analysis and were then refined based on results from preliminary model validation checks.

5x5x5m Block Models

Gold and silver grades in the 5x5x5m block models were estimated by ID3 and NN, using 3 metre composited data within the domains listed in Table 14-8. OK was also performed for mineralized domains (02AuEQ prefix). A two-pass search strategy was applied for all domains, with search ellipse distances doubled in the second estimation pass. Estimation parameters for Au and Ag for domains estimated in the 5x5x5m models are summarized in Table 14-18 and 14-19.

ID3 was selected as the final estimation method for Au and Ag in the 5x5x5m block models because it reconciles well with the nearest neighbor estimates and generally falls within grade-tonnage envelopes generated from SGS (see 'Model Validation' section below). The OK estimate was used for comparison purposes but was not selected as the final estimation method because it tends to show a higher degree of smoothing relative to the NN estimate in Swath plots for most domains, in addition to generally higher tonnes and lower grade than limits defined by SGS grade-tonnage envelopes.

2.5x2.5x2.5m Block Models

Gold and silver grades in the 2.5x2.5x2.5m block models were estimated by ID3 and NN, using 1.5 metre composited data within the domains listed in Table 14-9. OK was also performed for mineralized domains (1AuEQ prefix). A two-pass search strategy was applied for all domains, with search ellipse distances doubled in the second estimation pass. Estimation parameters for Au and Ag for all domains estimated in the 2.5x2.5x2.5m models are summarized in Tables 14-20 and 14-21.

ID3 was selected as the final estimation method for Au and Ag in the 2.5x2.5x2.5m block models because it reconciles well with the nearest neighbor estimates and shows a lesser degree of grade smoothing when compared to OK in most domains.

Table 14-20 Gold estimation parameters used for estimation in 5x5x5m block models

Variable: Au (g/t) Composites: 3m	Leapfrog				Pass 1 Data Search						Pass 2 Data Search					
Domain	**Dip**	**Dip Azi.**	**Pitch**	**Discretization (x/y/z)**	**Major (m)**	**Semi-Major (m)**	**Minor (m)**	**Min. Sample**	**Max. Sample**	**Max. Sample / Hole**	**Major (m)**	**Semi-Major (m)**	**Minor (m)**	**Min. Sample**	**Max. Sample**	**Max. Sample / Hole**
02AuEQ_ESTACA	75	200	15	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_FRE	55	225	20	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_GW	60	190	10	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_LAIJA	70	35	140	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_GUAD_NW	90	55	0	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_LP	80	40	120	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_MAR	45	220	45	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_NB_SME	60	235	40	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_SM_SN	45	35	0	2x2x2	40	40	10	4	10	2	80	80	20	1	4	2
02AuEQ_SME_SPLAYS	55	195	15	2x2x2	40	40	10	4	10	2	80	80	20	1	4	2
02AuEQ_SMW	60	190	20	2x2x2	40	40	7.5	4	10	2	80	80	15	1	4	2
02AuEQ_TA	50	240	35	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_ZN	55	250	35	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_ZS	45	215	30	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_ZW	60	210	0	2x2x2	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ESTACA	75	200	15	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_FRE	55	220	30	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_GUAD_NW	90	55	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_GW	60	190	10	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_LAIJA	70	30	140	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_LP	80	205	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_NB_SME	50	220	50	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_SM_SN	45	35	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_SME_SPLAYS	55	195	15	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ZTM	40	250	20	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ZW	60	210	0	-	60	60	10	4	10	2	120	120	20	1	4	2
BACKGROUND_ GUAD_LP	0	0	90	-	60	60	20	1	4	2	-	-	-	-	-	-
BACKGROUND_ ZTM_NB_SM	0	0	90	-	60	60	20	1	4	2	-	-	-	-	-	-

Notes:

The search ellipse orientations shown above are the global plunge direction for each domain. Local search orientation is determined from variable orientation models.

Table 14-21 Silver estimation parameters used for estimation in 5x5x5m block models

Variable: Ag (g/t) Composites: 3m	Leapfrog				Pass 1 Data Search						Pass 2 Data Search					
Domain	Dip	Dip Azi.	Pitch	Discretization (x/y/z)	Major (m)	Semi-Major (m)	Minor (m)	Min. Sample	Max. Sample	Max. Sample / Hole	Major (m)	Semi-Major (m)	Minor (m)	Min. Sample	Max. Sample	Max. Sample / Hole
02AuEQ_ESTACA	75	200	15	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_FRE	55	220	60	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_GW	60	190	10	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_LAIJA	70	35	140	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_GUAD_NW	90	55	0	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_LP	80	40	120	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_MAR	45	220	45	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_NB_SME	60	235	220	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_SM_SN	45	35	0	2x2x2	40	40	10	4	10	2	80	80	20	1	4	2
02AuEQ_SME_SPLAYS	55	195	15	2x2x2	40	40	10	4	10	2	80	80	20	1	4	2
02AuEQ_SMW	60	190	20	2x2x2	40	40	7.5	4	10	2	80	80	15	1	4	2
02AuEQ_TA	50	240	35	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_ZN	55	250	35	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_ZS	45	220	50	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
02AuEQ_ZW	60	210	0	2x2x2	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ESTACA	75	200	35	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_FRE	55	220	30	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_GUAD_NW	90	55	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_GW	60	190	10	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_LAIJA	70	30	140	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_LP	80	205	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_NB_SME	50	220	50	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_SM_SN	45	35	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_SME_SPLAYS	55	195	15	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ZTM	40	250	20	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ZW	60	210	0	-	60	60	10	4	10	2	120	120	20	1	4	2
BACKGROUND_ GUAD_LP	0	0	90	-	60	60	20	1	4	2	-	-	-	-	-	-
BACKGROUND_ ZTM_NB_SM	0	0	90	-	60	60	20	1	4	2	-	-	-	-	-	-

Notes:

The search ellipse orientations shown above are the global plunge direction for each domain. Local search orientation is determined from variable orientation models.

Table 14-22 Gold estimation parameters used for estimation in 2.5x2.5x2.5m block models

Variable: Au (g/t) Composites: 1.5m	Leapfrog				Pass 1 Data Search						Pass 2 Data Search					
Domain	**Dip**	**Dip Azi.**	**Pitch**	**Discretization (x/y/z)**	**Major (m)**	**Semi-Major (m)**	**Minor (m)**	**Min. Sample**	**Max. Sample**	**Max. Sample / Hole**	**Major (m)**	**Semi-Major (m)**	**Minor (m)**	**Min. Sample**	**Max. Sample**	**Max. Sample / Hole**
1AuEQ_ESTACA	75	200	15	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_FRE	55	225	20	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_GW	60	190	10	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_LAIJA	70	30	140	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_GUAD_NW	90	55	0	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_LP	80	40	120	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_MAR	45	220	45	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_NB_SME	60	235	40	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_SM_SN	45	35	0	2x2x2	40	40	10	4	10	2	80	80	20	1	4	2
1AuEQ_SME_SPLAYS	55	195	15	2x2x2	40	40	10	4	10	2	80	80	20	1	4	2
1AuEQ_SMW	60	190	20	2x2x2	40	40	7.5	4	10	2	80	80	15	1	4	2
1AuEQ_TA	50	240	35	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_ZN	55	250	35	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_ZS	45	215	30	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_ZW	60	210	0	2x2x2	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ESTACA	75	200	15	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_FRE	55	220	30	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_GUAD_NW	90	55	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_GW	60	190	10	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_LAIJA	70	30	140	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_LP	80	205	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_NB_SME	50	220	50	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_SM_SN	45	35	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_SME_SPLAYS	55	195	15	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ZTM	40	250	20	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ZW	60	210	0	-	60	60	10	4	10	2	120	120	20	1	4	2
BACKGROUND_ GUAD_LP	0	0	90	-	60	60	20	1	4	2	-	-	-	-	-	-
BACKGROUND_ ZTM_NB_SM	0	0	90	-	60	60	20	1	4	2	-	-	-	-	-	-

Notes:

The search ellipse orientations shown above are the global plunge direction for each domain. Local search orientation is determined from variable orientation models.

Table 14-23 Silver estimation parameters used for estimation in 2.5x2.5x2.5m block models

Variable: Ag (g/t) Composites: 1.5m	Leapfrog				Pass 1 Data Search						Pass 2 Data Search					
Domain	Dip	Dip Azi.	Pitch	Discretization (x/y/z)	Major (m)	Semi-Major (m)	Minor (m)	Min. Sample	Max. Sample	Max. Sample / Hole	Major (m)	Semi-Major (m)	Minor (m)	Min. Sample	Max. Sample	Max. Sample / Hole
1AuEQ_ESTACA	75	200	15	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_FRE	55	225	20	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_GW	60	190	10	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_LAIJA	70	30	140	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_GUAD_NW	90	55	0	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_LP	80	40	120	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_MAR	45	220	45	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_NB_SME	60	235	40	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_SM_SN	45	35	0	2x2x2	40	40	10	4	10	2	80	80	20	1	4	2
1AuEQ_SME_SPLAYS	55	195	15	2x2x2	40	40	10	4	10	2	80	80	20	1	4	2
1AuEQ_SMW	60	190	20	2x2x2	40	40	7.5	4	10	2	80	80	15	1	4	2
1AuEQ_TA	50	240	35	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_ZN	55	250	35	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_ZS	45	215	30	2x2x2	60	45	10	4	10	2	120	90	20	1	4	2
1AuEQ_ZW	60	210	0	2x2x2	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ESTACA	75	200	35	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_FRE	55	220	30	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_GUAD_NW	90	55	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_GW	60	190	10	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_LAIJA	70	30	140	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_LP	80	205	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_NB_SME	50	220	50	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_SM_SN	45	35	0	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_SME_SPLAYS	55	195	15	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ZTM	40	250	20	-	60	60	10	4	10	2	120	120	20	1	4	2
QV_BX_ZW	60	210	0	-	60	60	10	4	10	2	120	120	20	1	4	2
BACKGROUND_ GUAD_LP	0	0	90	-	60	60	20	1	4	2	-	-	-	-	-	-
BACKGROUND_ ZTM_NB_SM	0	0	90	-	60	60	20	1	4	2	-	-	-	-	-	-

Notes:

The search ellipse orientations shown above are the global plunge direction for each domain. Local search orientation is determined from variable orientation models.

14.3.8 *Bulk Density Modelling*

A total of 4,776 density values have been collected from drill core at the Project. These data were assessed according to logged lithology and alteration, modeled lithology, and by estimation domain to ensure the most representative possible values were assigned to the block models. Density was assigned to the mineralized domains (02AuEQ and 1AuEQ prefixes in the 5x5x5m and 2.5x2.5x2.5m block models, respectively) and QV_BX domains according to the average values within each domain group, and to all other modeled lithologies according to the average values within each solid. A value of 0.0 g/cm3 is assigned to historical workings. Density data collection is ongoing as new drilling is completed, and additional measurements will be incorporated into future resource estimates. Table 14-22 shows the current density values assigned to both the 5x5x5m and 2.5x2.5x2.5m block models.

Table 14-24 Density Values Assigned to Models

Domain/Lithology	Density (g/cm^3)	Source
Mineralized Domains (02AuEQ and 1AuEQ prefixes)	2.543	Mean value from Mineralized domains
QV_BX Domains	2.496	Mean value from QV_BX domains
RHYL	2.425	Mean value from RHYL solid in lithology model
DAC	2.444	Mean value from DAC solid in lithology model
ANDS	2.513	Mean value from ANDS solid in lithology model
GRANO	2.592	Mean value from GRANO solid in lithology model
OVBN	2.463	Mean value from OVBN solid in lithology model
Historical Workings	0.000	Historical workings wireframe model

Notes:

To determine final block density, the original density value flagged according to domain and lithology is corrected by the proportion of the block which has been mined, by the formula: Density[Final] = Density[Original] x (1-Mined_Pct), where 'Mined_Pct' is the historically mined portion of the block.

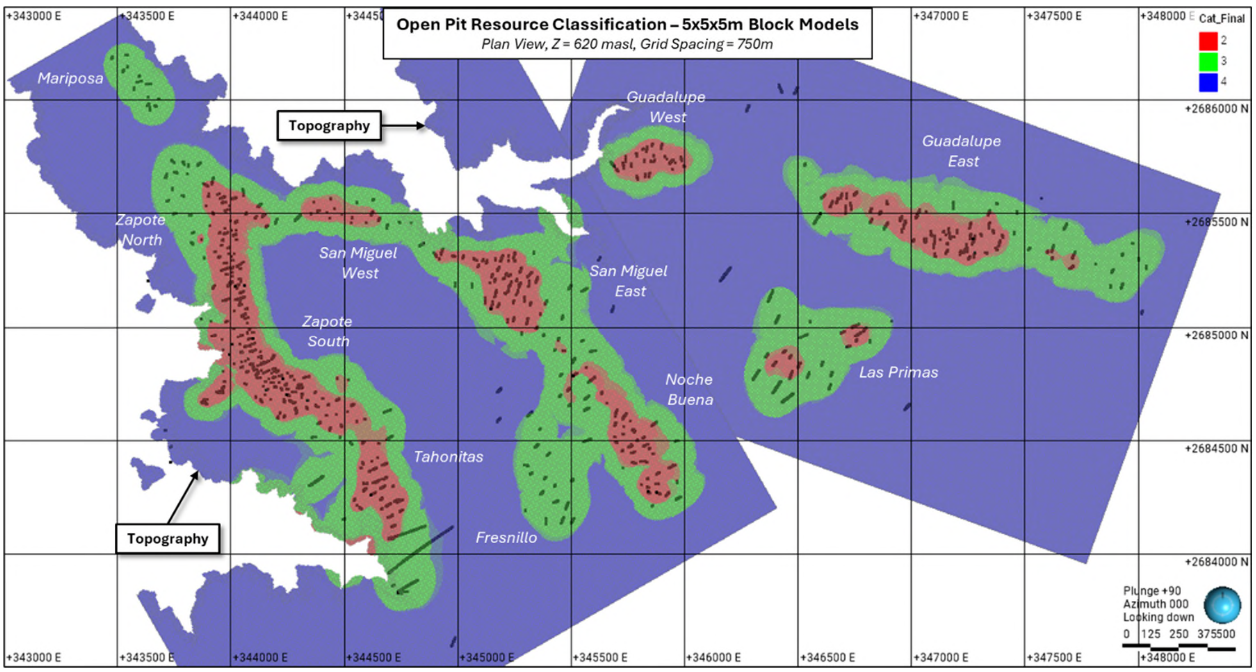
14.3.9 *Mineral Resource Classification*

Mineral Resources for the Project are classified under the categories of Indicated and Inferred, in accordance with CIM Definition Standards. The Measured resource category was not used in either set of models because no modern mining has been undertaken at the Property and it is therefore not possible to reconcile the models against production or tightly spaced data such as grade control drilling.

Open Pit Resource Classification (5x5x5m Block Models)

Data spacing sufficient for Open Pit Indicated resources was determined by calculating the weighted average distance at which the direction 1 variogram models reach 80% of the normalized sill (Gamma = 0.8), determined graphically from back transformed variograms for the mineralized domains in the 5x5x5m block models (02AuEQ prefix). Inferred resource data spacing was determined by calculating the weighted average distance at which the direction 1 variogram models reach 95% of the normalized sill (Gamma = 0.95). Weights for each domain were assigned according to their total Au Oz and Ag Oz inventory, reported from the 5x5x5m block models. As a result of this analysis, Open Pit Indicated resources were categorized based on a drill spacing of 40 metres or less and Inferred resources were categorized based on a drill spacing of 40-80 metres. Figure 14-24 shows the classification codes for the 5x5x5m block models.

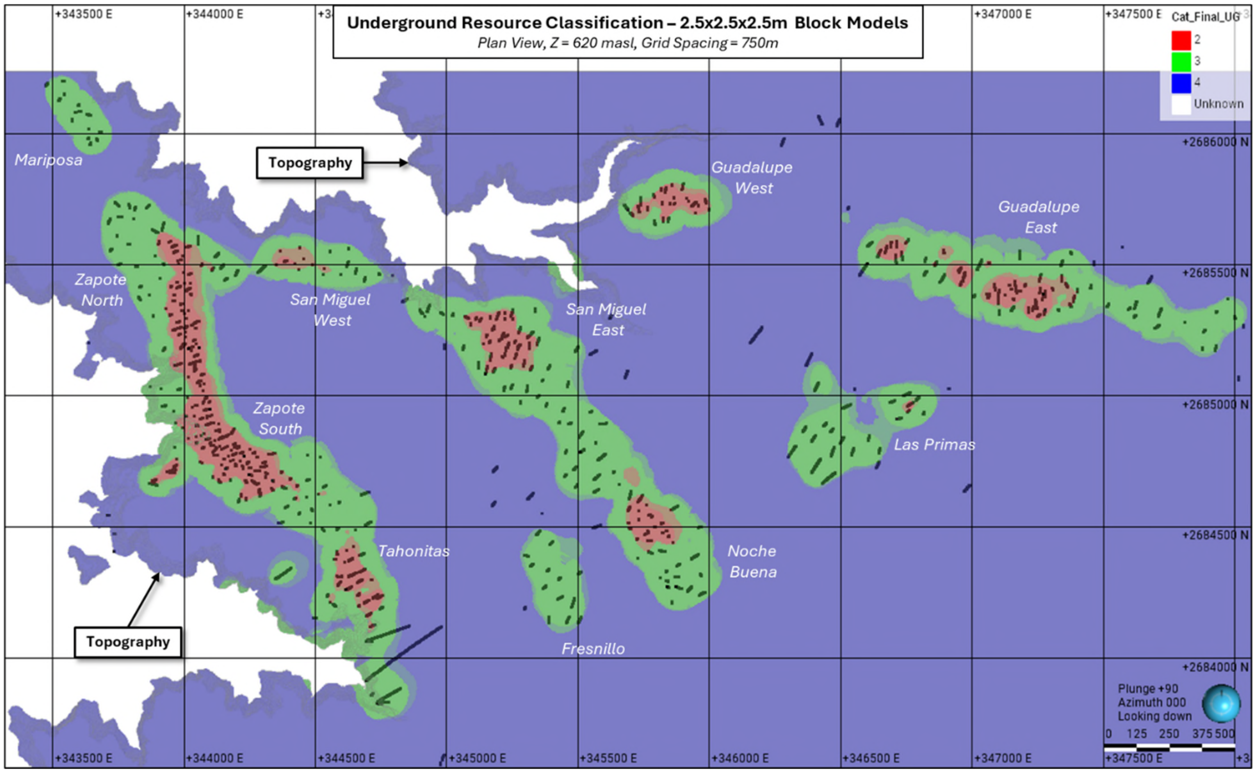
Figure 14-24 Los Reyes resource classification for 5x5x5m block models
Plan view, looking down, at 620m elevation. Cat_Final codes are: 2 Indicated, 3 Inferred, and 4 unclassified



Underground Resource Classification (2.5x2.5x2.5m Block Models)

Data spacing sufficient for underground Indicated resources was determined by calculating the weighted average distance at which the direction 1 variogram models reach 80% of the normalized sill (Gamma = 0.8), determined graphically from back transformed variograms for the mineralized domains in the 2.5x2.5x2.5m block models (1AuEQ prefix). Inferred resource data spacing was determined by calculating the weighted average distance at which the direction 1 variogram models reach 95% of the normalized sill (Gamma = 0.95). Weights for each domain were assigned according to their total Au Oz and Ag Oz inventory, reported from the 2.5x2.5x2.5m block models. As a result of this analysis, underground Indicated resources were categorized based on a drill spacing of 30 metres or less and Inferred Resources were categorized based on a drill spacing of 30-60 metres. Figure 14-25 shows the classification codes for the 2.5x2.5x2.5m block models.

Figure 14-25 Los Reyes resource classification for 2.5x2.5x2.5m block models
Plan view, looking down, at 620m elevation. Cat_Final codes are: 2 Indicated, 3 Inferred, and 4 unclassified



14.3.10 *Model Validation*

Validation checks for both block models are focused on the mineralized domains (02AuEq and 1AuEQ prefixes), which contain >97% of the reported Au inventory and >98% of the reported Ag inventory. The models were validated using the following methods:

- Statistical comparison (ID3 vs. Uncapped ID3, NN (as defined below), and OK).
- Sectional validation – visual comparison between block grades and composite grades.
- Swath plots.
- Comparison to grade-tonnage envelopes from SGS.

<u>Estimate Comparison (ID3 vs Uncapped ID3, NN, and OK)</u>

Statistics for the final ID3 estimates for both Au and Ag were compared to the Nearest Neighbor (“NN”) and OK estimates, globally and domain by domain. The final ID3 estimates were also compared with an uncapped ID3 estimate to evaluate metal loss.

5x5x5m Block Models

The ID3 estimates selected for final resource reporting in the 5x5x5m block models were compared with NN and OK estimates for each mineralized domain (02AuEQ prefix), considering

Indicated and Inferred blocks only, with no pit constraint applied. The difference in average estimated grade between the ID3 and NN estimates is less than 5% for all mineralized domains aside from 02AuEQ_GUAD_NW, which is sparsely drilled and contains 0% of the total reported pit-constrained Au and Ag inventory. The difference in average estimated grade between the ID3 and OK estimates is less than 5% for Au and Ag in all mineralized domains.

The final ID3 estimates for Au and Ag were also compared against estimates prepared using the uncapped 3 metre composite dataset ("ID3 Uncapped"), to evaluate metal loss. The search parameters for the uncapped estimate were otherwise kept identical to the final ID3 estimates. Metal loss due to capping is less than 10% for all domains aside from Au_ID3 in the 02AuEQ_ESTACA, 02AuEQ_LP, and 02AuEQ_SMW domains. The large difference between the capped and uncapped estimates in these three cases is driven by extreme outliers in the uncapped dataset (for example, a single 156 g/t Au composite in the 02AuEQ_ESTACA domain). Tables 14-23 and 14-24 show the comparison between the various estimation methods for Au and Ag, domain by domain.

Table 14-25 Estimate mean comparison between Au_ID3, Au_ID3 Uncapped, Au_NN, and Au_OK for mineralized domains in the 5x5x5m block models

Domain	3 metre Capped Composite Mean (g/t)	Comp. Count	Au_ID3 Capped (g/t)	Au_ID3 Uncapped (g/t)	ID3 Capped vs. ID3 Uncapped	Au_NN Capped (g/t)	ID3 Capped vs. NN Capped	Au_OK Capped (g/t)	ID3 Capped vs. OK Capped	Domain Tonnes
02AuEQ_ESTACA	1.67	695	1.72	2.00	-16.0%	1.76	-2.1%	1.68	2.7%	4,617,637
02AuEQ_FRE	0.37	385	0.36	0.36	0.0%	0.36	0.6%	0.37	-0.5%	12,292,862
02AuEQ_GUAD _NW	0.56	86	0.28	0.28	0.0%	0.26	8.2%	0.28	0.7%	373,632
02AuEQ_GW	0.57	433	0.39	0.39	-0.3%	0.38	2.4%	0.40	-1.5%	3,467,924
02AuEQ_LAIJA	1.37	843	1.12	1.15	-2.5%	1.17	-3.7%	1.12	0.5%	4,747,290
02AuEQ_LP	0.45	351	0.39	0.41	-6.5%	0.38	0.8%	0.38	0.5%	7,405,638
02AuEQ_MAR	0.64	201	0.63	0.64	-1.1%	0.63	-0.3%	0.61	2.6%	3,298,861
02AuEQ_NB_SME	0.53	1,549	0.43	0.44	-0.9%	0.43	0.5%	0.43	0.7%	17,259,106
02AuEQ_SM_SN	0.54	165	0.82	0.82	0.0%	0.84	-1.9%	0.81	1.5%	1,589,349
02AuEQ_SME _SPLAYS	0.40	245	0.38	0.40	-3.9%	0.38	0.8%	0.39	-2.5%	1,766,573
02AuEQ_SMW	1.01	143	0.69	0.79	-15.1%	0.69	0.6%	0.70	-1.6%	1,402,616
02AuEQ_TA	0.46	1,097	0.43	0.44	-0.5%	0.43	0.5%	0.44	-0.5%	16,836,605
02AuEQ_ZN	0.76	2,647	0.57	0.58	-0.9%	0.57	0.7%	0.57	1.4%	19,192,879
02AuEQ_ZS	0.82	1,685	0.62	0.62	0.0%	0.61	1.3%	0.63	-1.4%	15,257,969

Notes:

1. Au_ID3, Au_NN, and Au_OK values are estimated using capped 3 metre composite dataset.
2. Au_ID3 Uncapped is estimated using uncapped 3 metre composites, with the same search parameters as for Au_ID3.
3. Indicated and Inferred resource categories only, no pit constraint applied.

Table 14-26 Estimate mean comparison between Ag_ID3, Ag_ID3 Uncapped, Ag_NN, and Ag_OK for mineralized domains in the 5x5x5m block models

Domain	3 metre Capped Composite Mean (g/t)	Comp. Count	Ag_ID3 Capped (g/t)	Ag_ID3 Uncapped (g/t)	ID3 Capped vs. ID3 Uncapped	Ag_NN Capped (g/t)	ID3 Capped vs. NN Capped	Ag_OK Capped (g/t)	ID3 Capped vs. OK Capped	Domain Tonnes
02AuEQ_ESTACA	106.00	695	110.37	110.98	-0.5%	115.60	-4.5%	105.90	4.2%	4,617,637
02AuEQ_FRE	6.78	385	7.03	7.16	-1.9%	6.99	0.5%	7.03	-0.1%	12,292,862
02AuEQ_GUAD_NW	21.75	86	14.77	14.77	0.0%	13.43	10.0%	15.28	-3.4%	373,632
02AuEQ_GW	19.90	433	19.17	19.16	0.0%	19.08	0.4%	19.16	0.0%	3,467,924
02AuEQ_LAIJA	45.73	843	45.05	46.37	-2.9%	44.67	0.8%	45.74	-1.5%	4,747,290
02AuEQ_LP	22.44	351	16.98	17.01	-0.2%	16.60	2.3%	17.06	-0.5%	7,405,638
02AuEQ_MAR	10.49	201	10.55	10.55	0.0%	10.60	-0.5%	10.47	0.7%	3,298,861
02AuEQ_NB_SME	22.66	1,549	20.64	20.73	-0.5%	20.51	0.6%	20.39	1.2%	17,259,106
02AuEQ_SM_SN	28.80	165	47.75	50.44	-5.6%	47.86	-0.2%	46.68	2.3%	1,589,349
02AuEQ_SME_SPLAYS	32.51	245	29.19	29.60	-1.4%	29.30	-0.4%	29.71	-1.7%	1,766,573
02AuEQ_SMW	21.16	143	14.89	15.06	-1.1%	14.61	1.9%	14.71	1.2%	1,402,616
02AuEQ_TA	29.96	1,097	25.75	27.13	-5.4%	25.57	0.7%	26.01	-1.0%	16,836,605
02AuEQ_ZN	13.57	2,647	12.78	12.78	0.0%	12.76	0.2%	12.63	1.2%	19,192,879
02AuEQ_ZS	20.61	1,685	18.82	18.83	-0.1%	18.80	0.1%	18.78	0.2%	15,257,969

Notes:

1. Ag_ID3, Ag_NN, and Ag_OK values are estimated using the capped 3 metre composite dataset.
2. Ag_ID3 Uncapped is estimated using uncapped 3 metre composites, with the same search parameters as for Ag_ID3.
3. Indicated and Inferred resource categories only, no pit constraint applied.

2.5x2.5x2.5m Block Models

The ID3 estimates selected for final resource reporting in the 2.5x2.5x2.5m block models were compared with NN and OK estimates for each mineralized domain (1AuEQ prefix), considering Indicated and Inferred blocks only, with no MSO constraint applied. The difference in average estimated grade between the ID3 and NN estimates is less than 5% for all mineralized domains aside from 1AuEQ_LP, 1AuEQ_SM_SN, and 1AuEQ_SMW, which collectively contain <3% of the total reported Au and Ag inventory.

The final ID3 estimates for Au and Ag were also compared against estimates prepared using the ID3 Uncapped, to evaluate metal loss. The search parameters for the uncapped estimate were otherwise kept identical to the final ID3 estimates. Metal loss due to capping is less than 10% for all domains aside from Au_ID3 in the 1AuEQ_ESTACA, 1AuEQ_MAR, 1AuEQ_SME_SPLAYS, and 1AuEQ_SMW domains. The large difference between the capped and uncapped estimates in these cases is driven by extreme outliers in the uncapped dataset (for example, a single 156 g/t

Au composite in the 1AuEQ_ESTACA domain). Tables 14-25 and 14-26 show the comparison between the various estimation methods for Au and Ag, domain by domain.

Table 14-27 Estimate mean comparison between Au_ID3, Au_ID3 Uncapped, Au_NN, and Au_OK for mineralized domains in the 2.5x2.5x2.5m block models

Domain	1.5 metre Capped Composite Mean (g/t)	Comp. Count	Au_ID3 Capped (g/t)	Au_ID3 Uncapped (g/t)	ID3 Capped vs. ID3 Uncapped	Au_NN Capped (g/t)	ID3 Capped vs. NN Capped	Au_OK Capped (g/t)	ID3 Capped vs. OK Capped	Domain Tonnes
1AuEQ_ESTACA	2.75	733	2.73	3.03	-11.2%	2.81	-3.0%	2.54	7.6%	3,661,777
1AuEQ_FRE	0.98	70	0.89	0.89	0.0%	0.88	0.7%	0.90	-1.3%	1,310,731
1AuEQ_GW	1.36	213	1.23	1.28	-4.3%	1.18	4.1%	1.22	0.7%	677,077
1AuEQ_LAIJA	2.31	876	2.02	2.09	-3.8%	1.99	1.3%	1.94	3.8%	2,891,499
1AuEQ_LP	1.04	166	0.92	1.00	-9.1%	0.86	7.2%	0.96	-4.2%	1,957,599
1AuEQ_MAR	1.98	79	1.81	2.05	-13.1%	1.77	2.3%	1.76	2.9%	1,122,359
1AuEQ_NB_SME	1.43	802	1.24	1.24	-0.5%	1.22	1.8%	1.21	1.9%	5,182,339
1AuEQ_SM_SN	1.77	44	1.58	1.64	-3.8%	1.93	-18.1%	1.46	8.4%	542,463
1AuEQ_SME _SPLAYS	1.32	98	1.43	1.52	-6.5%	1.46	-2.1%	1.35	5.5%	385,872
1AuEQ_SMW	6.79	36	7.70	8.70	-12.9%	7.28	5.8%	7.50	2.7%	117,826
1AuEQ_TA	1.22	538	1.04	1.06	-1.4%	1.03	0.9%	1.04	0.1%	7,509,531
1AuEQ_ZN	2.27	1,264	1.80	1.81	-1.1%	1.77	1.3%	1.74	3.1%	5,475,724
1AuEQ_ZS	2.05	1,055	1.73	1.74	-0.6%	1.74	-0.5%	1.69	2.0%	5,512,418

Notes:

1. Au_ID3, Au_NN, and Au_OK values are estimated using capped 1.5 metre composite dataset.
2. Au_ID3 Uncapped is estimated using uncapped 1.5 metre composites, with the same search parameters as for Au_ID3.
3. Indicated and Inferred resource categories only, no pit constraint applied.

Table 14-28 Estimate mean comparison between Ag_ID3, Ag_ID3 Uncapped, Ag_NN, and Ag_OK for mineralized domains in the 2.5x2.5x2.5m block models

Domain	1.5 metre Capped Composite Mean (g/t)	Comp. Count	Ag_ID3 Capped (g/t)	Ag_ID3 Uncapped (g/t)	ID3 Capped vs. ID3 Uncapped	Ag_NN Capped (g/t)	ID3 Capped vs. NN Capped	Ag_OK Capped (g/t)	ID3 Capped vs. OK Capped	Domain Tonnes
1AuEQ_ESTACA	170.10	733	170.66	172.98	-1.4%	178.75	-4.5%	161.91	5.4%	3,661,777
1AuEQ_FRE	23.99	70	18.60	18.60	0.0%	18.64	-0.2%	18.60	0.0%	1,310,731
1AuEQ_GW	31.84	213	39.82	40.19	-0.9%	39.73	0.2%	39.93	-0.3%	677,077
1AuEQ_LAIJA	74.94	876	80.97	84.08	-3.8%	80.21	0.9%	78.20	3.5%	2,891,499
1AuEQ_LP	54.58	166	38.82	39.88	-2.7%	37.87	2.5%	33.45	16.1%	1,957,599
1AuEQ_MAR	20.96	79	20.96	20.96	0.0%	21.30	-1.6%	20.21	3.7%	1,122,359
1AuEQ_NB _SME	58.15	802	57.69	58.80	-1.9%	57.45	0.4%	56.24	2.6%	5,182,339
1AuEQ_SM_SN	82.55	44	74.08	83.83	-13.2%	120.15	-38.3%	68.49	8.2%	542,463
1AuEQ_SME _SPLAYS	99.48	98	106.34	116.23	-9.3%	109.98	-3.3%	101.84	4.4%	385,872
1AuEQ_SMW	82.49	36	87.68	95.05	-8.4%	86.41	1.5%	82.13	6.8%	117,826
1AuEQ_TA	73.60	538	74.67	76.59	-2.6%	73.67	1.4%	74.66	0.0%	7,509,531
1AuEQ_ZN	23.77	1,264	24.38	24.38	0.0%	24.48	-0.4%	23.71	2.8%	5,475,724
1AuEQ_ZS	40.40	1,055	42.96	42.96	0.0%	43.36	-0.9%	42.18	1.9%	5,512,418

Notes:

1. Ag_ID3, Ag_NN, and Ag_OK values are estimated using the capped 1.5 metre composite dataset.
2. Ag_ID3 Uncapped is estimated using uncapped 1.5 metre composites, with the same search parameters as for Ag_ID3.
3. Indicated and Inferred resource categories only, no pit constraint applied.

Sectional Validation – Blocks versus Composites

Estimated gold and silver block grades, resource classification, lithology model and underground workings wireframe assignment to blocks, and drill hole composite data were compared visually in plan and cross section for all deposit areas and in both sets of block models, discussed below.

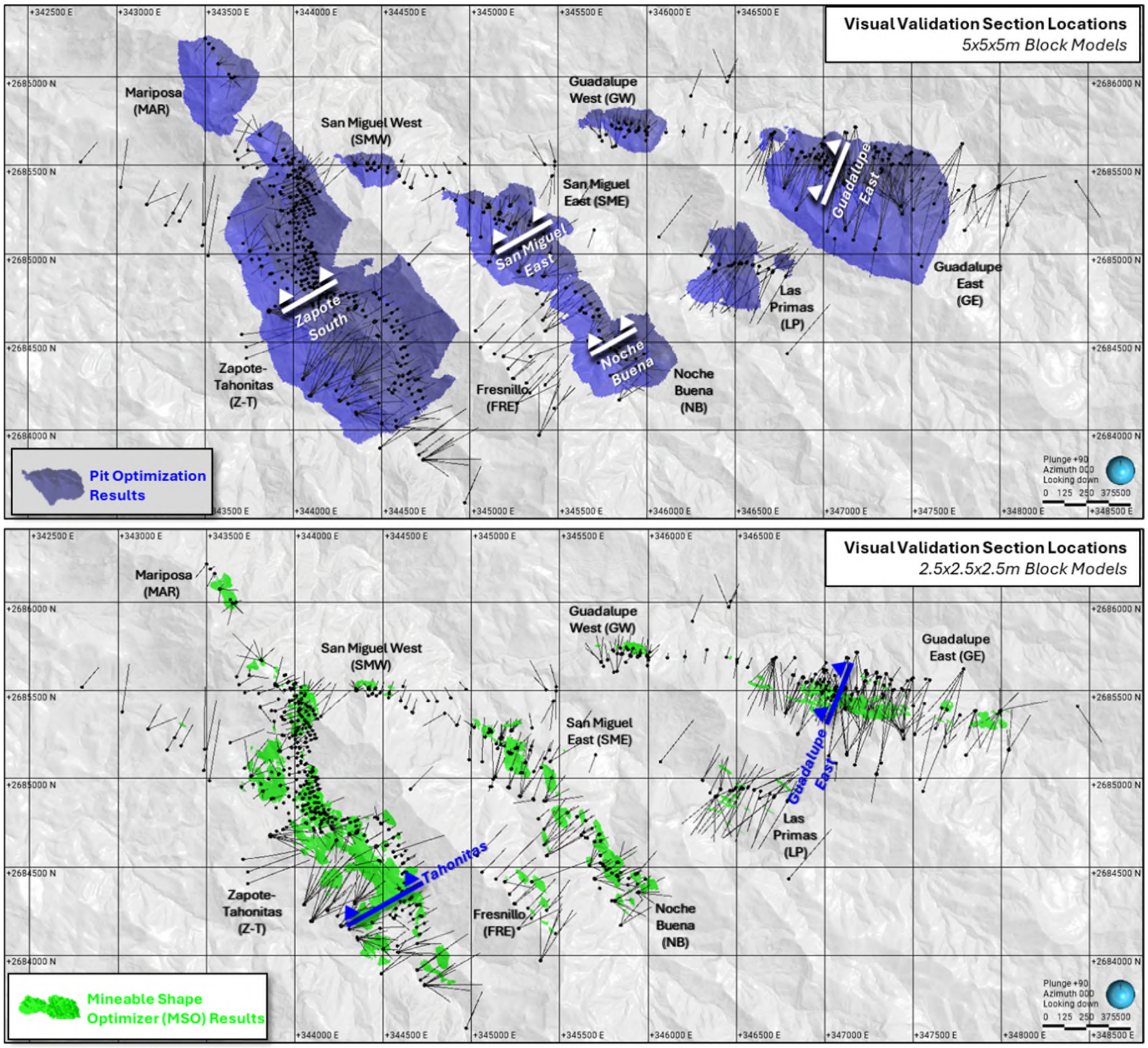
5x5x5m Block Models

Visual validation demonstrates that ID3-estimated 5x5x5m block grades reproduce the 3 metre composite grades well. Figures 14-27 through 14-30 show several examples comparing estimated Au and Ag grades to the composited dataset within pit shells generated using the Hochbaum Pseudoflow algorithm (see the section titled 'Assessment of Reasonable Prospects for Eventual Economic Extraction' below).

2.5x2.5x2.5m Block Models

Visual validation demonstrates that ID3-estimated 2.5x2.5x2.5m block grades reproduce the 1.5 metre composite grades well. Figures 14-31 through 14-34 show several examples comparing estimated Au and Ag grades to the composited dataset within stopes generated using Datamine's MSO (see the section titled 'Assessment of Reasonable Prospects for Eventual Economic Extraction' below).

Figure 14-26 Section locations for Figures 14-27 through 14-30 (upper) and Figures 14-31 through 14-34 (lower)



Notes:

Pit optimization and MSO results are determined independently using the 5x5x5m block models and 2.5x2.5x2.5m block models, respectively (optimization parameters are listed in the section titled 'Assessment of Reasonable Prospects for Eventual Economic Extraction' below). These shapes are used for model validation and sensitivity analysis only and do not represent the final combined set of open pit and underground resource-constraining wireframes (Figure 14-46).

Figure 14-27 Zapote South Au Visual Validation – 5x5x5m Block Model

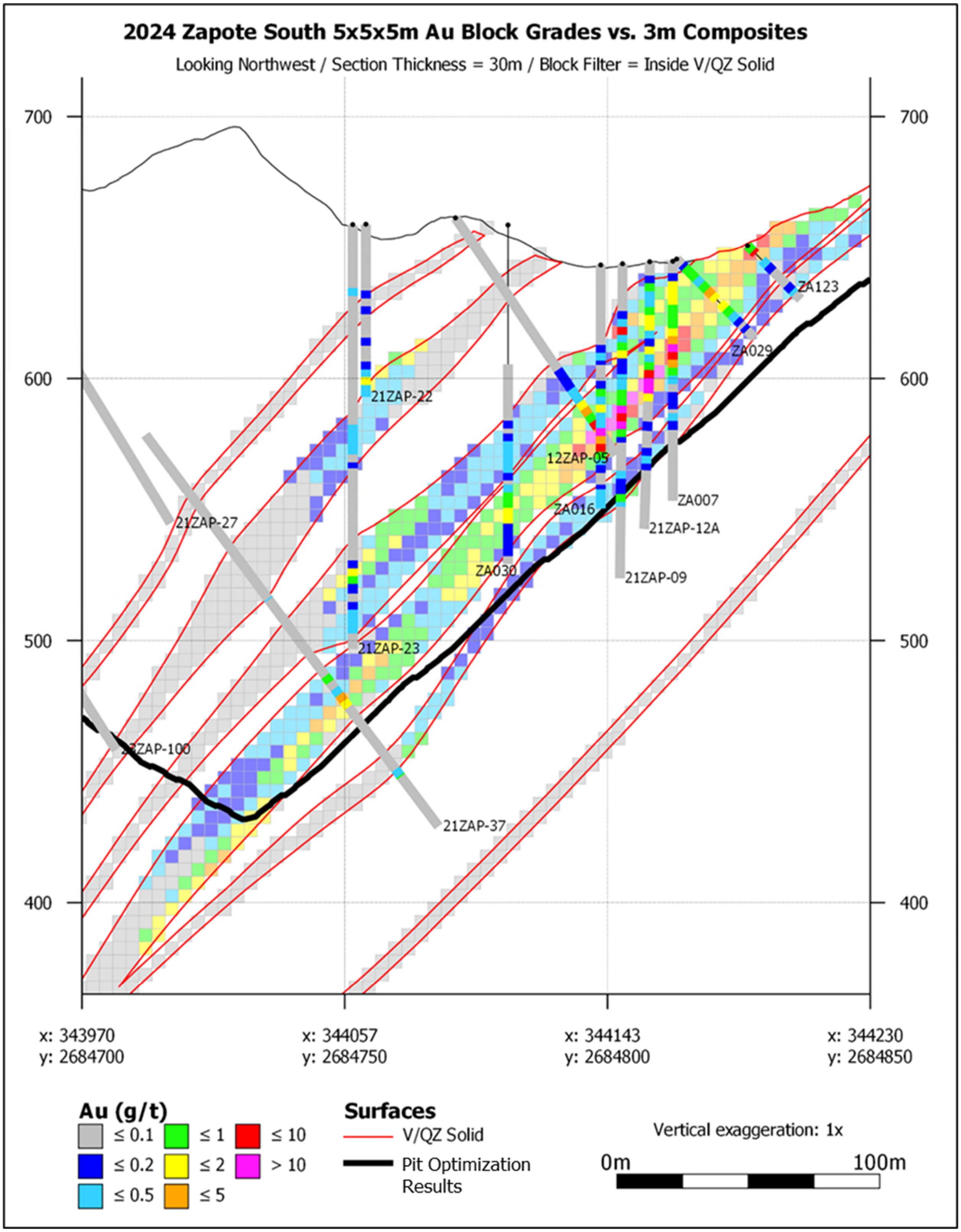


Figure 14-28 Noche Buena Au Visual Validation – 5x5x5m Block Model

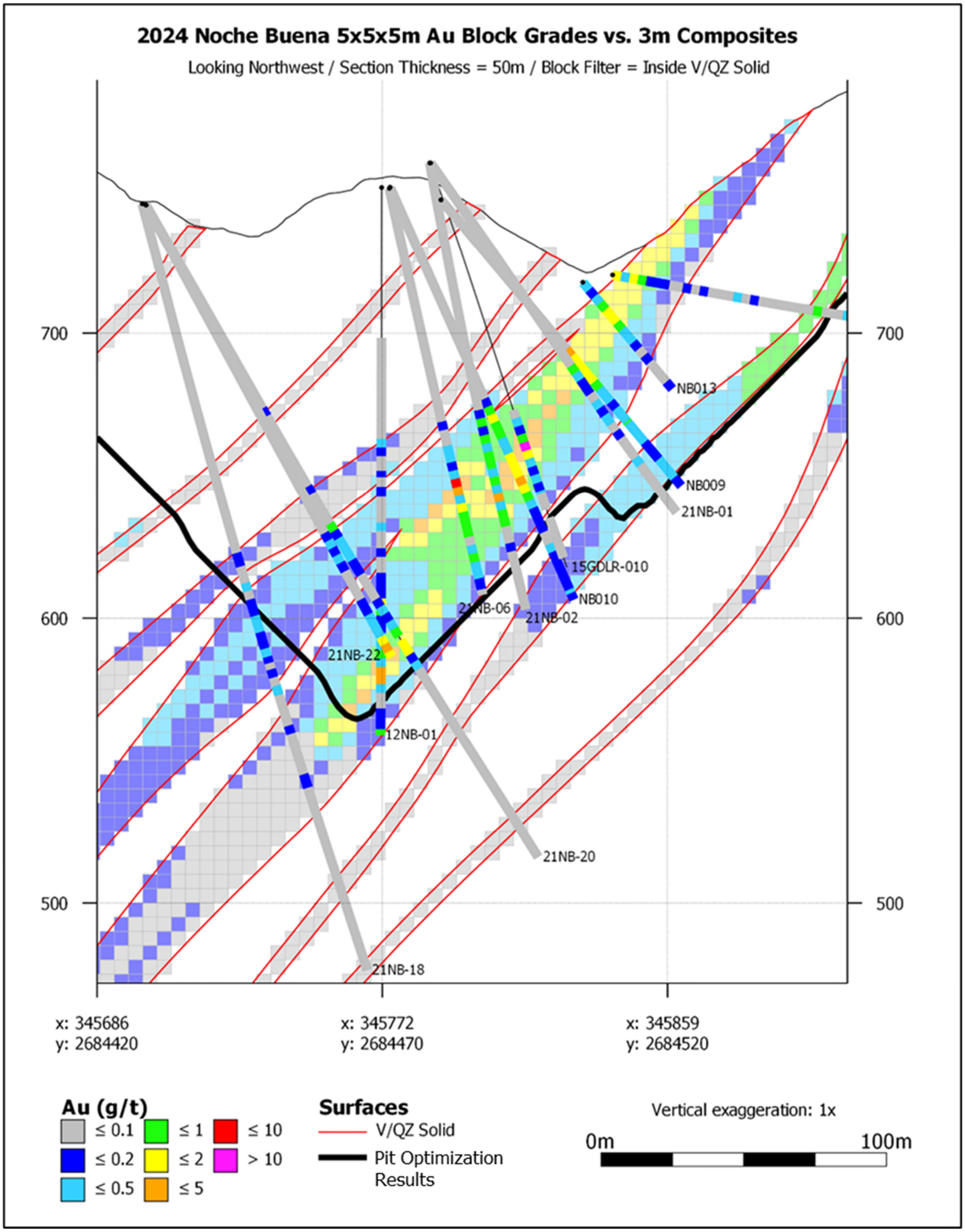


Figure 14-29 Guadalupe East Ag Visual Validation – 5x5x5m Block Model

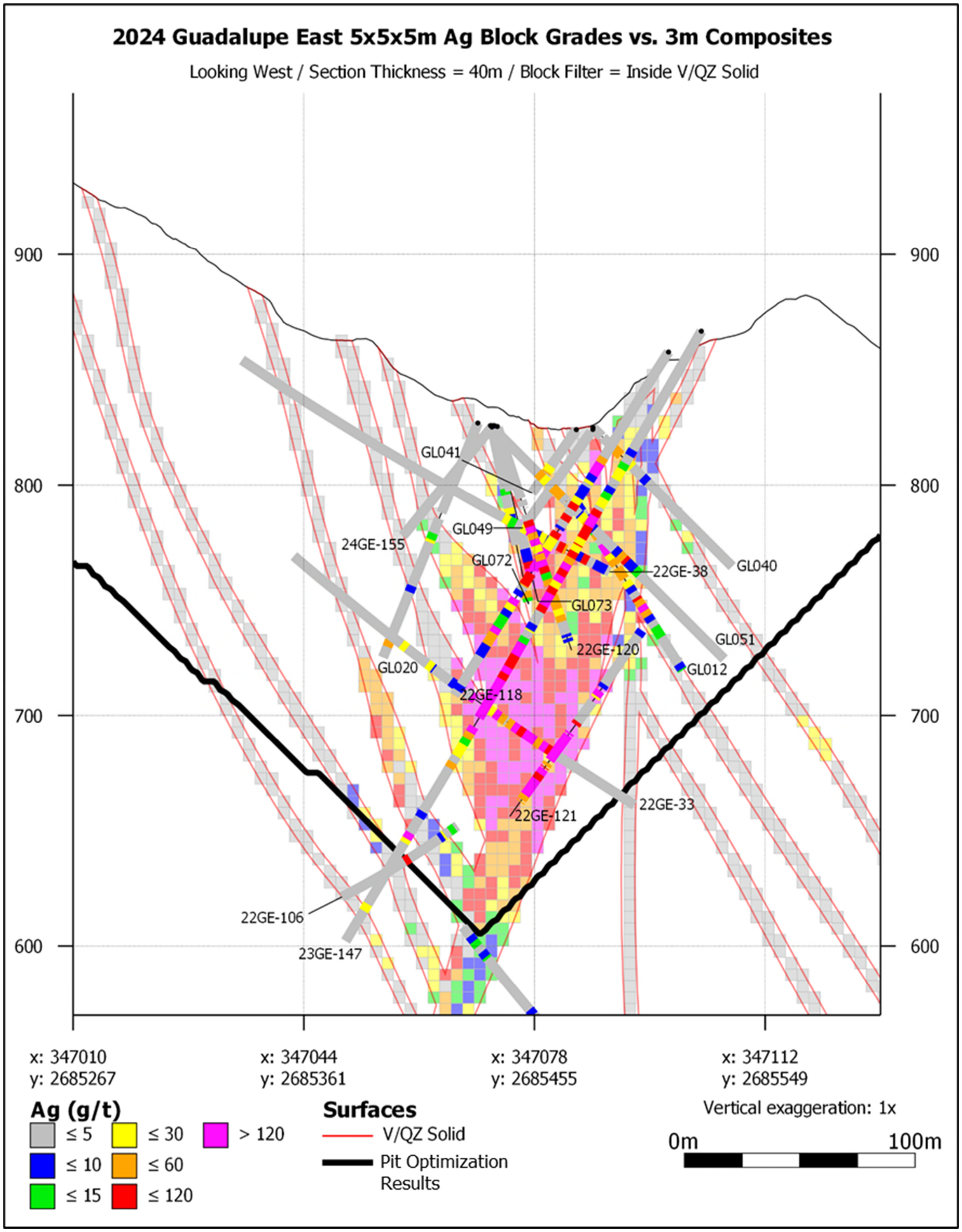


Figure 14-30 San Miguel East Ag Visual Validation – 5x5x5m Block Model

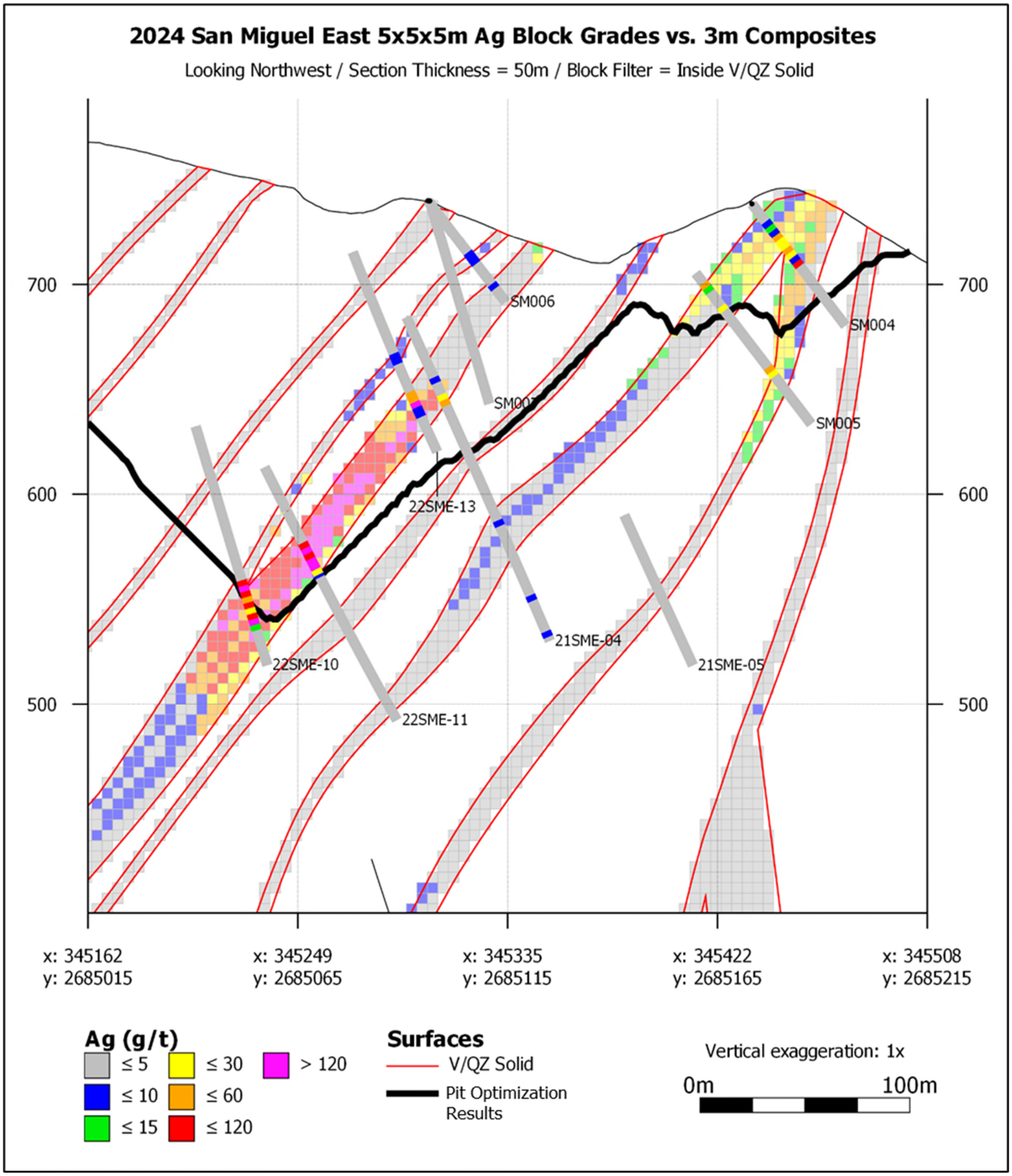


Figure 14-31 Tahonitas Au Visual Validation – 2.5x2.5x2.5m Block Model

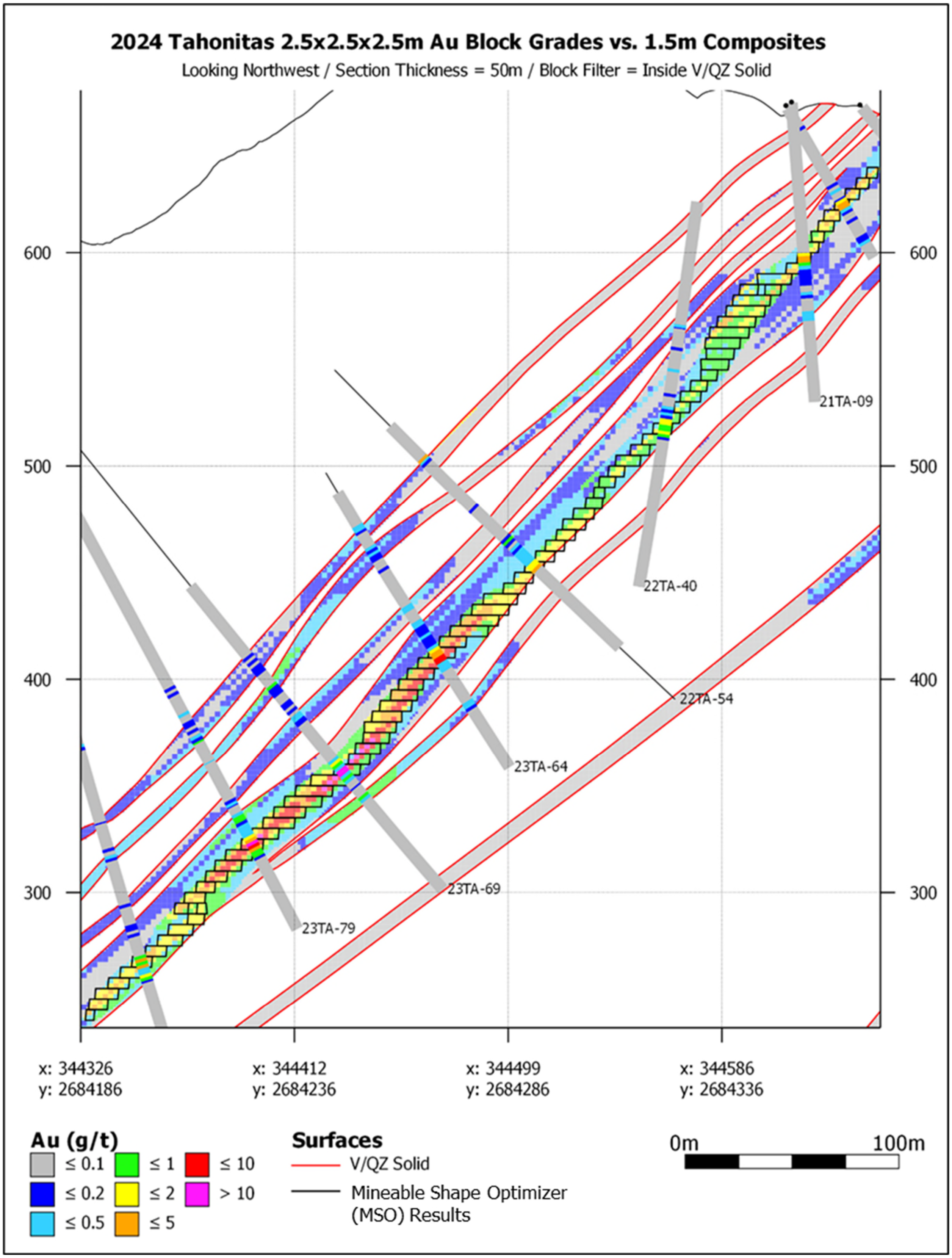


Figure 14-32 Guadalupe East Au Visual Validation – 2.5x2.5x2.5m Block Model

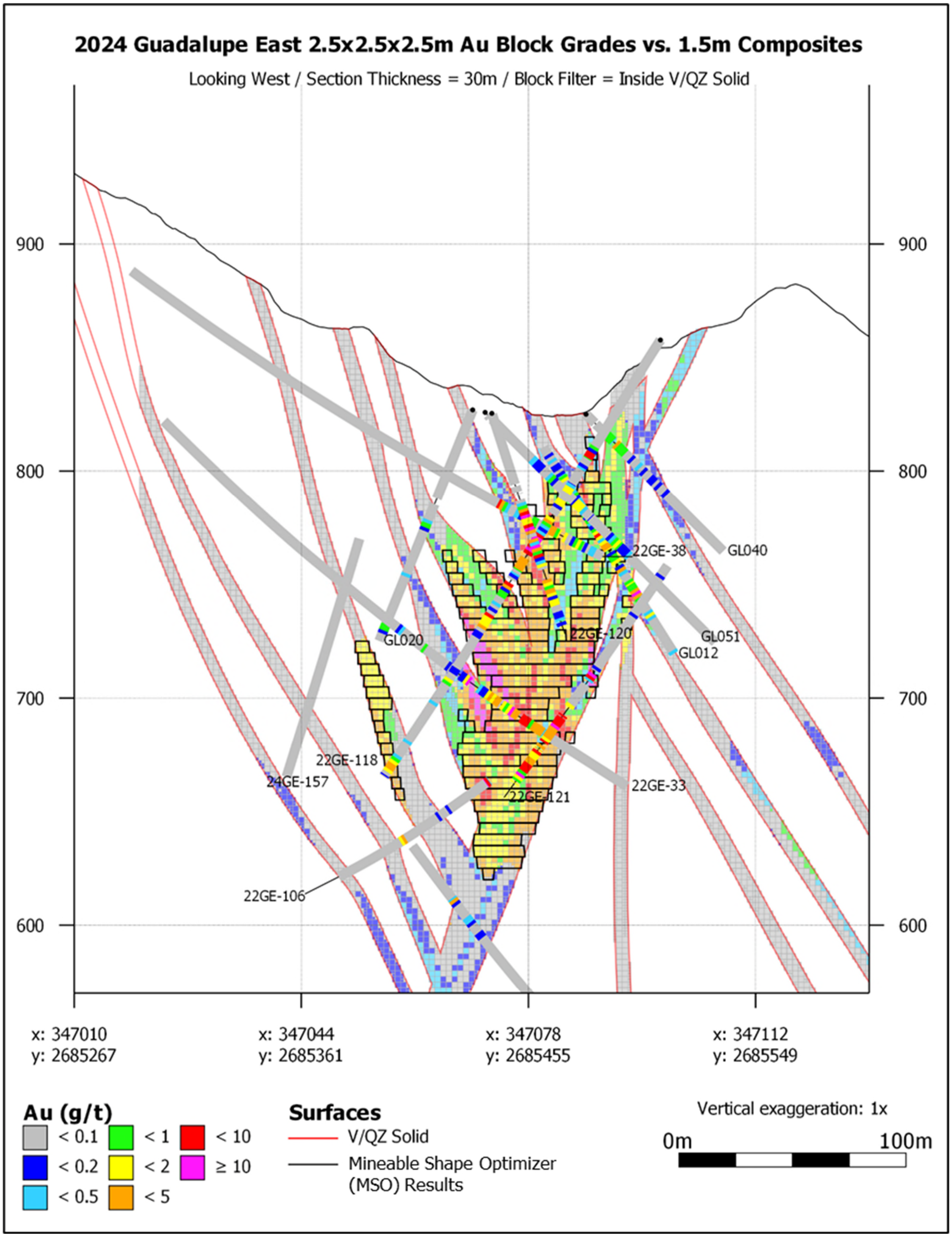


Figure 14-33 Tahonitas Ag Visual Validation – 2.5x2.5x2.5m Block Model

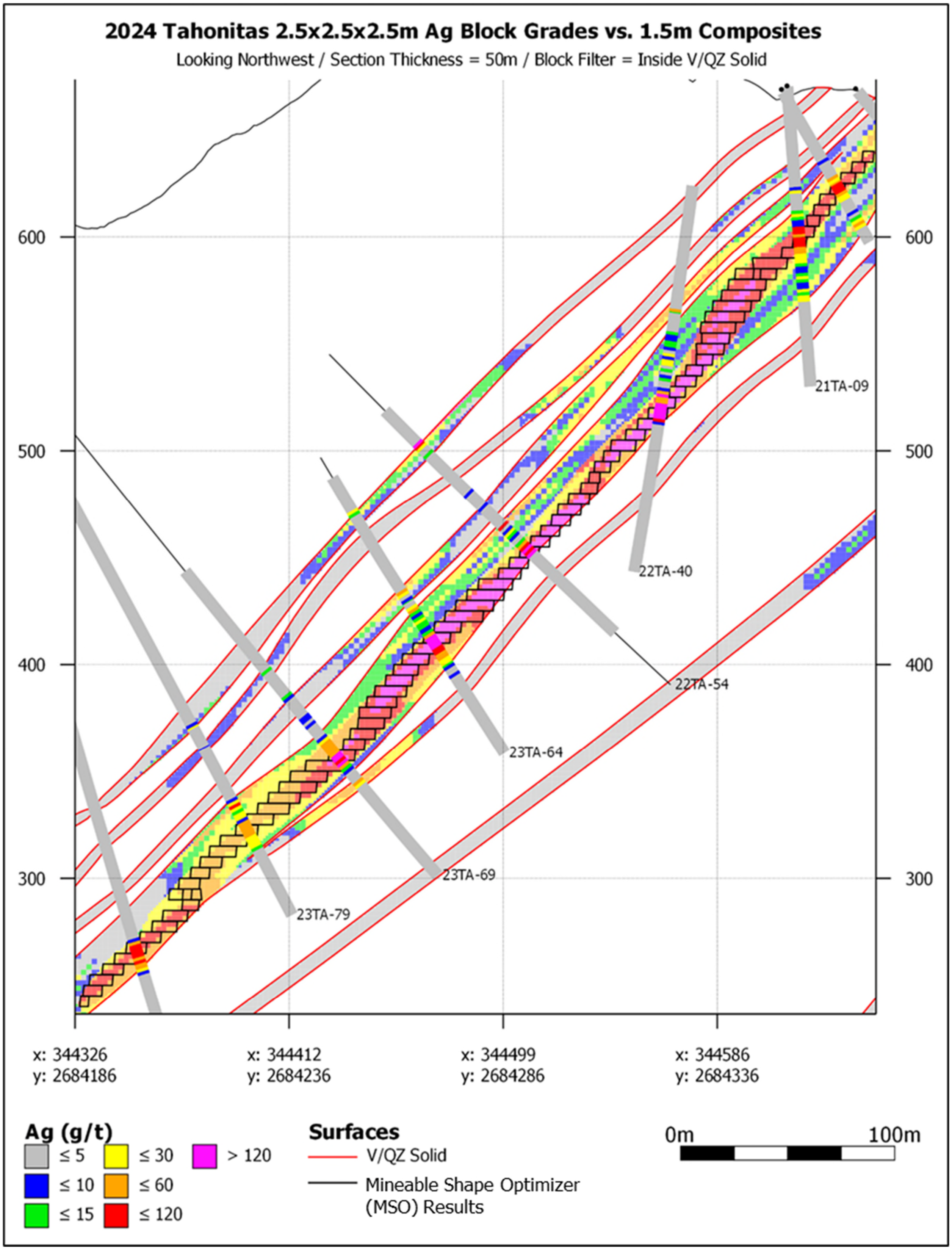
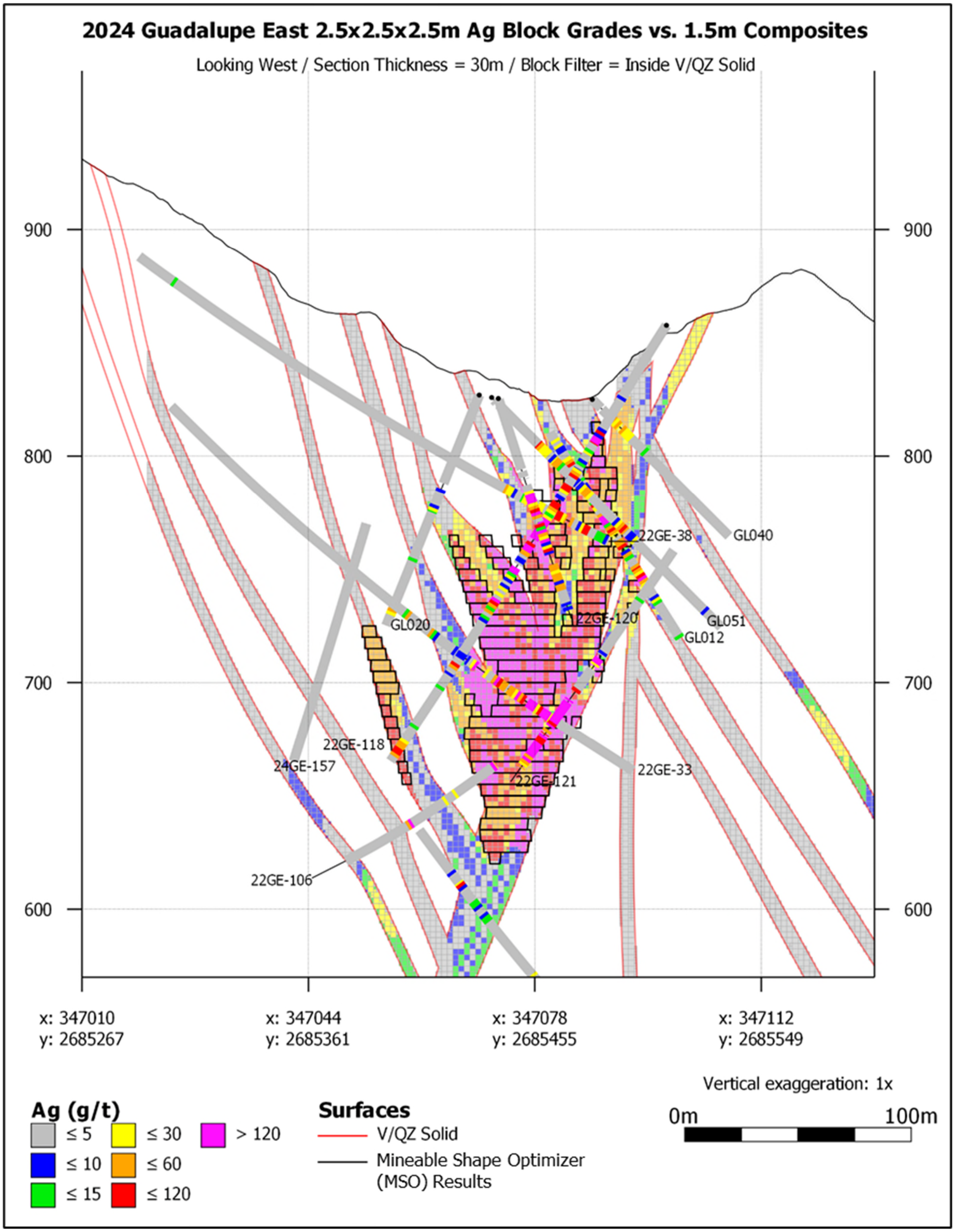


Figure 14-34 Guadalupe East Ag Visual Validation – 2.5x2.5x2.5m Block Model



Swath Plots

Swath plots were generated for each mineralized estimation domain to compare the ID3, NN, and OK estimates against one another and against composite grades. Results from each set of block models is described below.

5x5x5m Block Models

Results demonstrate that the ID3 estimates for Au and Ag in mineralized domains (02AuEQ prefix) in the 5x5x5m block models do not show a systematic high or low bias against the NN estimate or 3 metre composites, and that the estimated grades for all three methods match the composite grades well in easting, northing, and elevation. The OK estimates tend to show a higher degree of smoothing relative to ID3, hence the selection of ID3 as the final estimation method. Figures 14-35 through 14-38 show examples from several mineralized domains.

2.5x2.5x2.5m Block Models

Results demonstrate that the ID3 estimates for Au and Ag in mineralized domains (1AuEQ prefix) in the 2.5x2.5x2.5m block models do not show a systematic high or low bias against the NN estimate or 1.5 metre composites, and that the estimated grades for all three methods match the composite grades well in easting, northing, and elevation. The OK estimates tend to show a higher degree of smoothing relative to ID3, hence the selection of ID3 as the final estimation method. Figures 14-39 through 14-42 show examples from several mineralized domains.

Figure 14-35 Au Swath plots from the 02AuEQ_ZS estimation domain (5x5x5m block model)

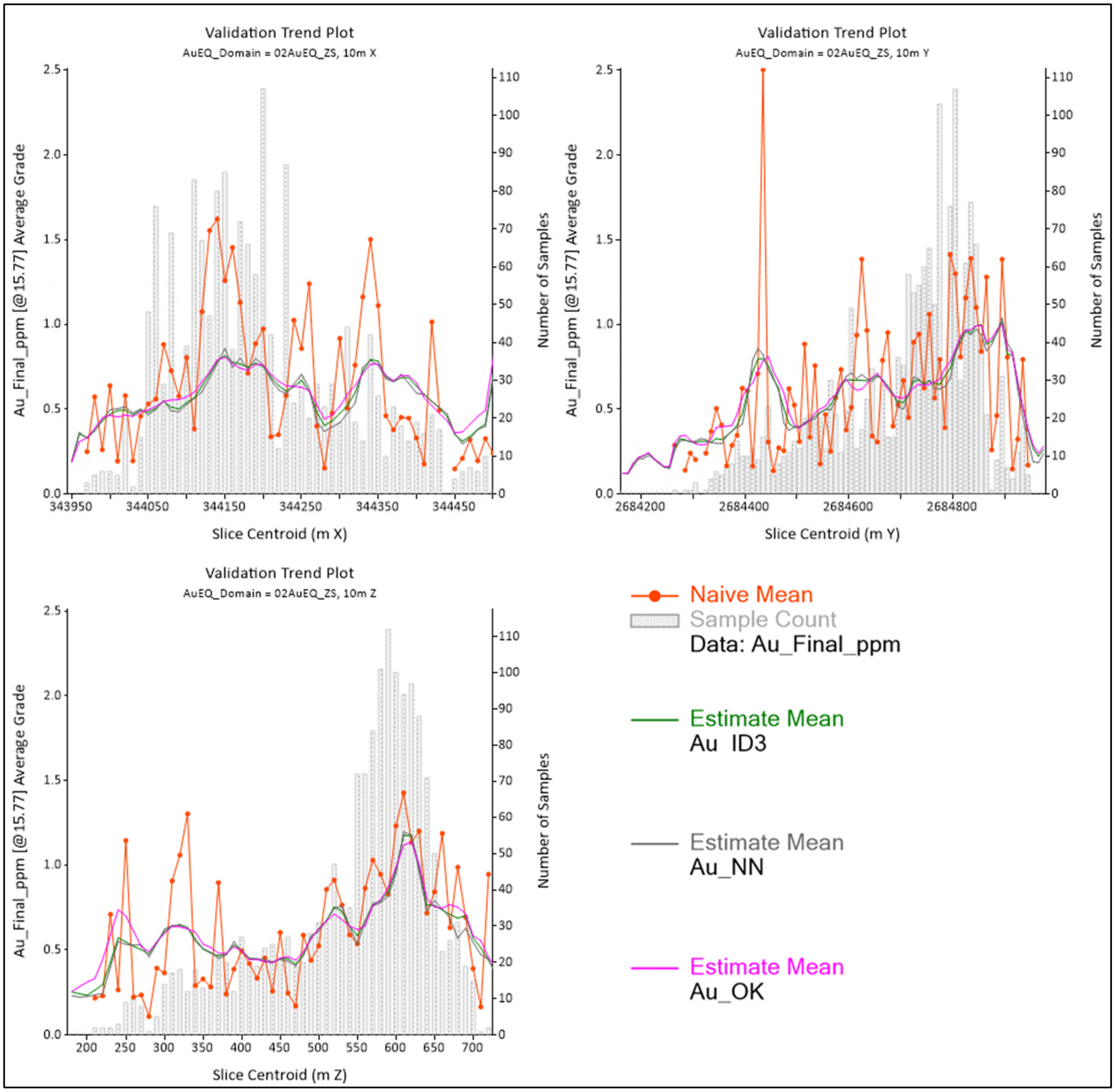


Figure 14-36 Au Swath plots from the 02AuEQ_ESTACA estimation domain (5x5x5m block model)

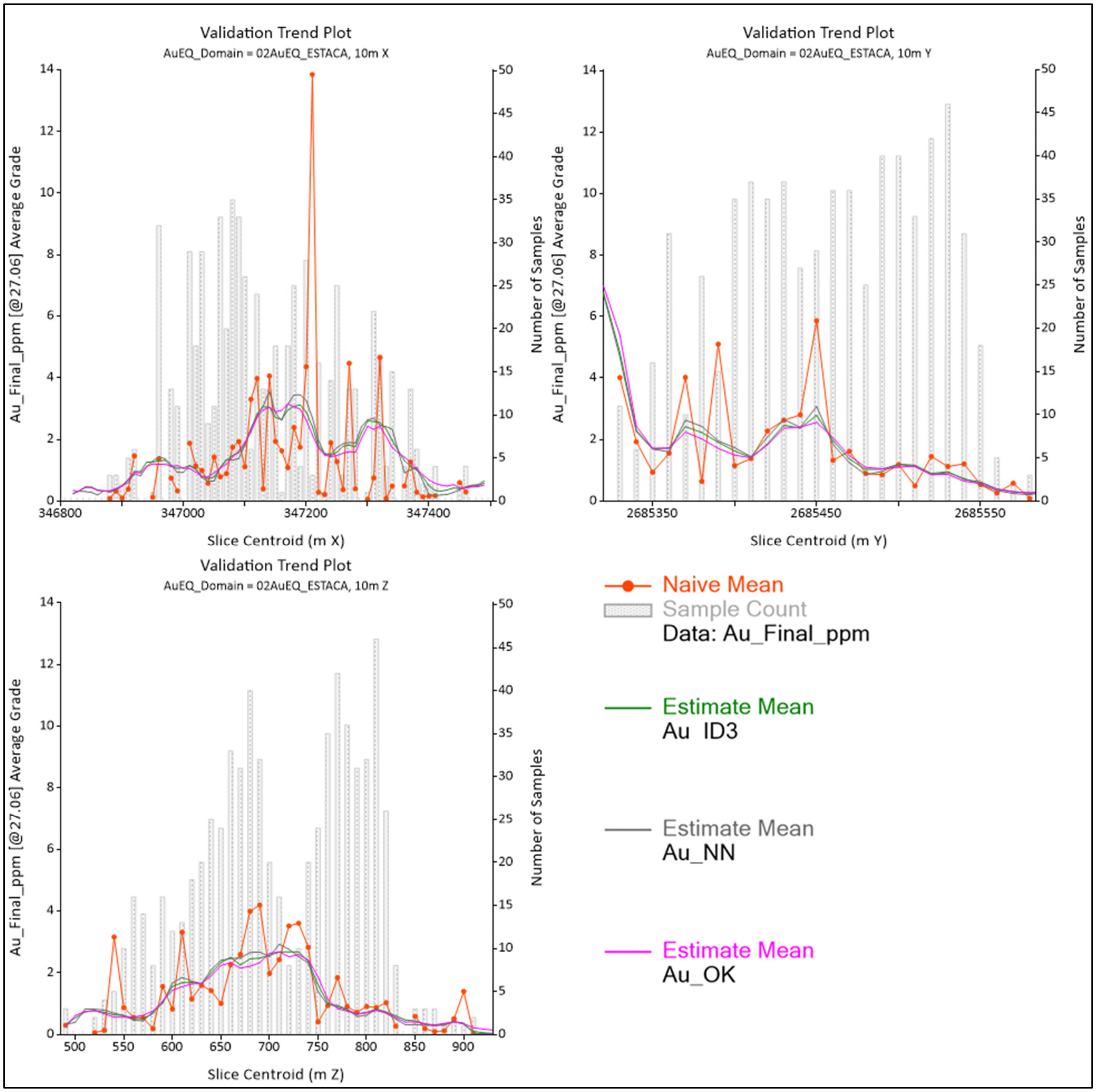


Figure 14-37 Ag Swath plots from the 02AuEQ_NB_SME estimation domain (5x5x5m block model)

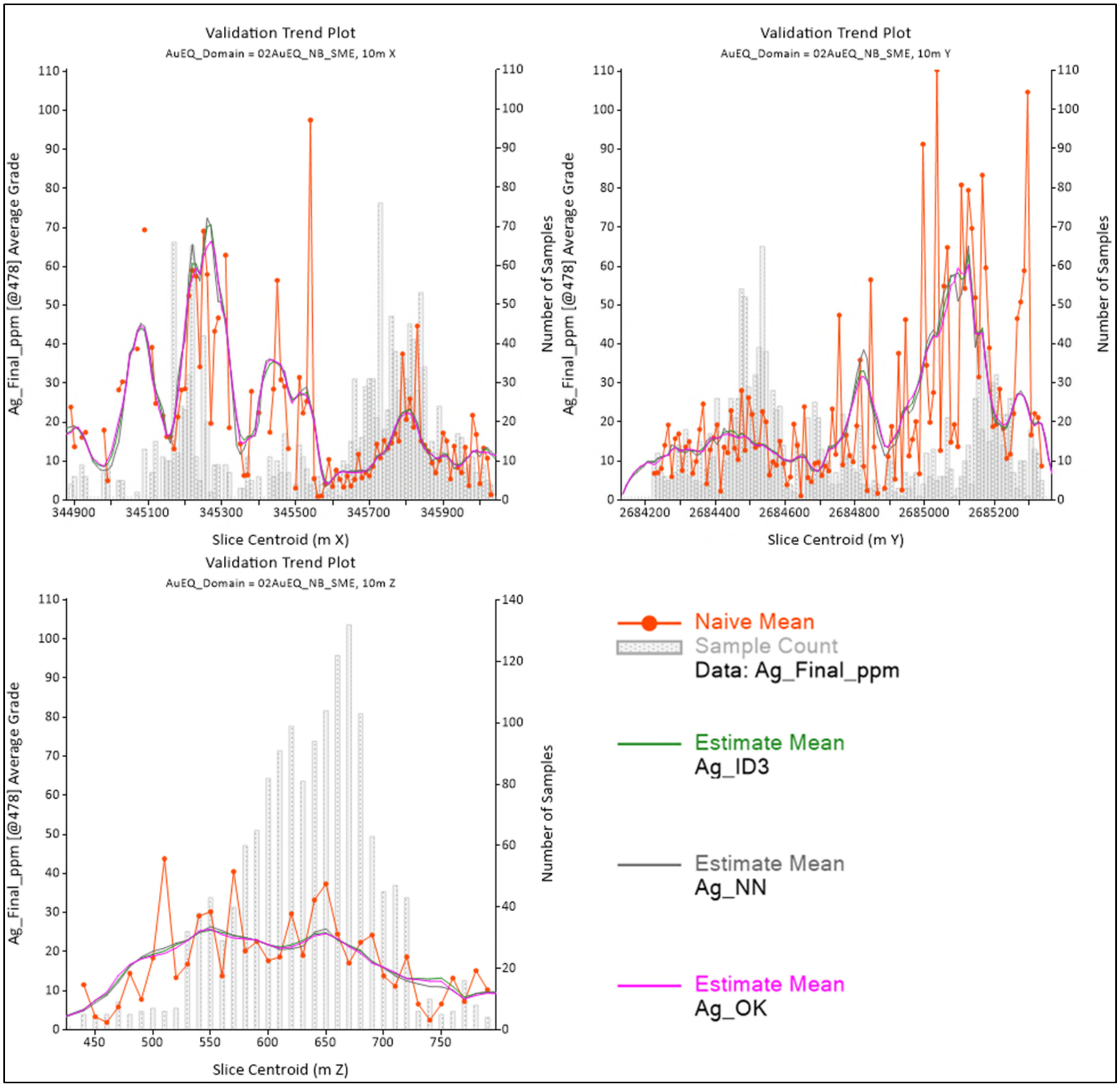


Figure 14-38 Ag Swath plots from the 02AuEQ_TA estimation domain (5x5x5m block model)

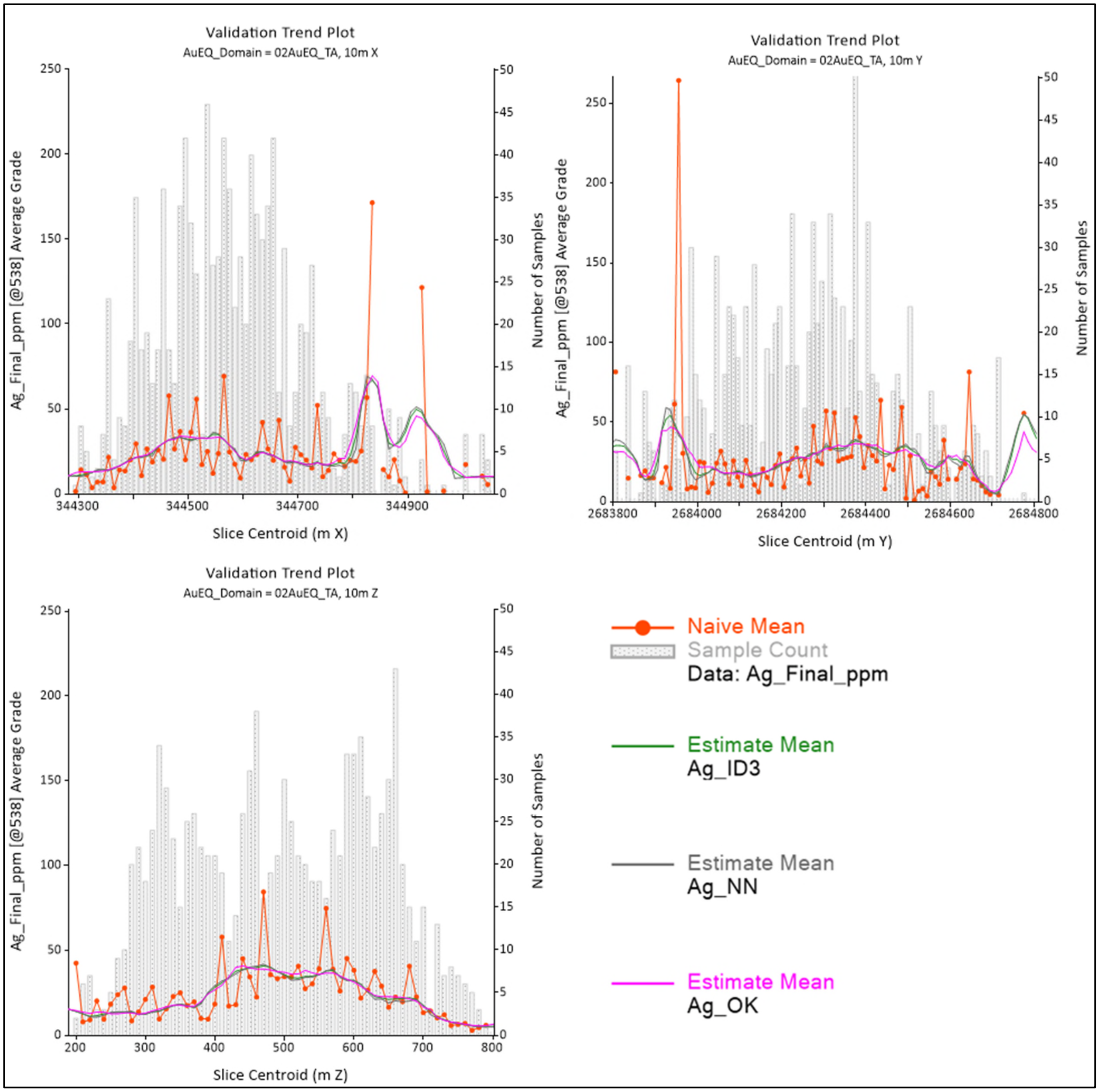


Figure 14-39 Au Swath plots from the 1AuEQ_ESTACA estimation domain (2.5x2.5x2.5m block model)

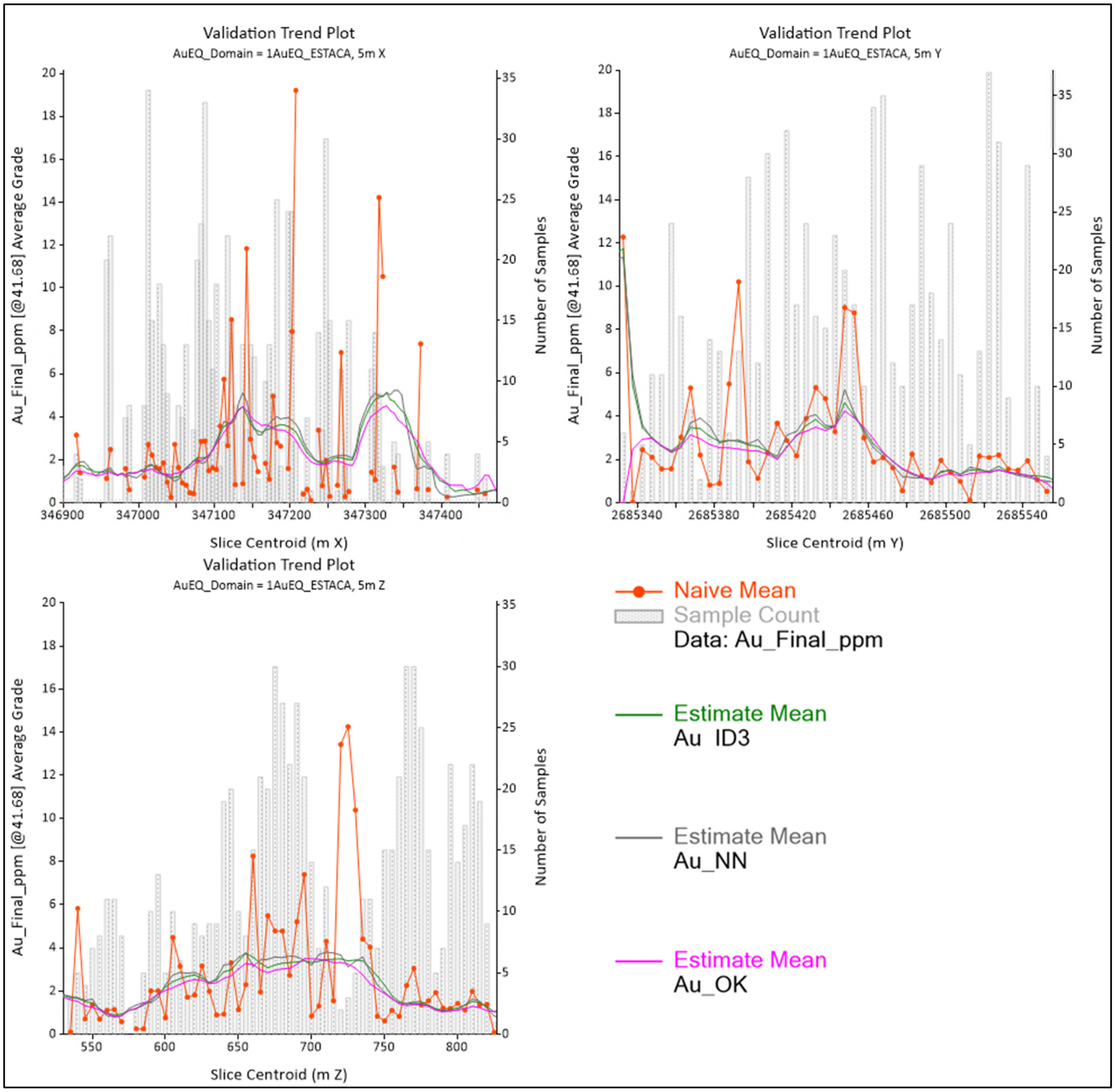


Figure 14-40 Au Swath plots from the 1AuEQ_ZS estimation domain (2.5x2.5x2.5m block model)

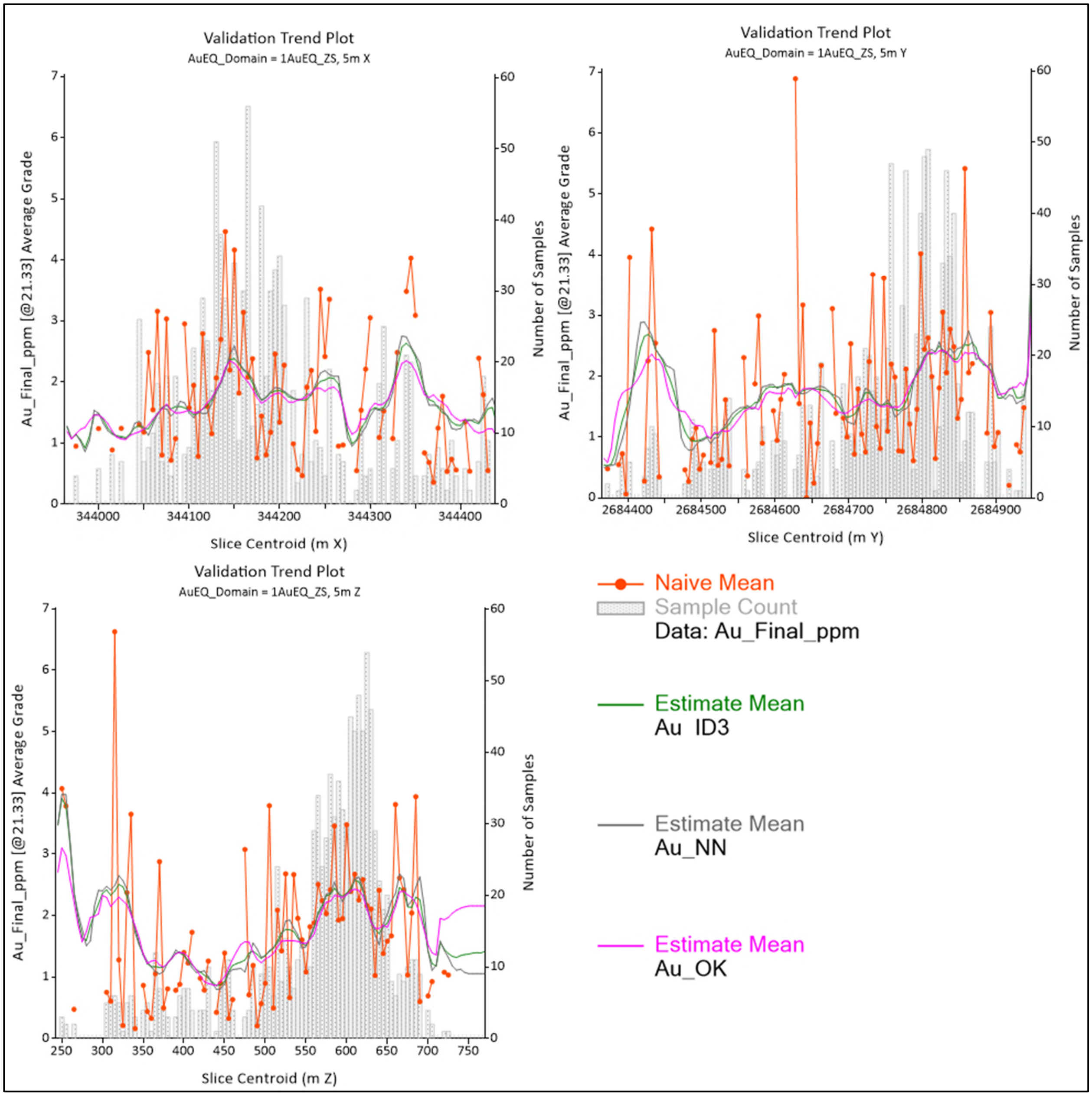


Figure 14-41 Ag Swath plots from the 1AuEQ_LAIJA estimation domain (2.5x2.5x2.5m block model)

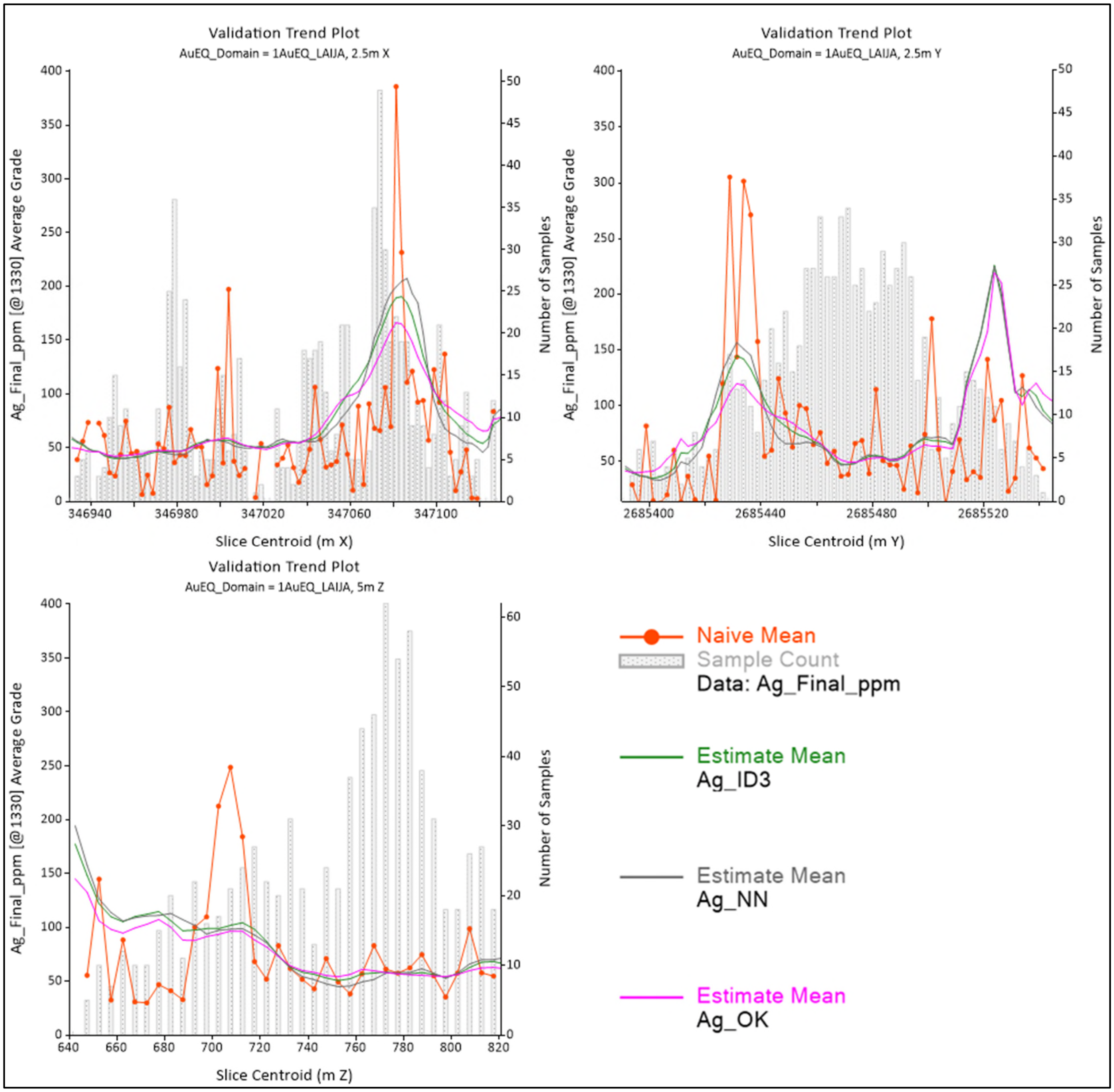
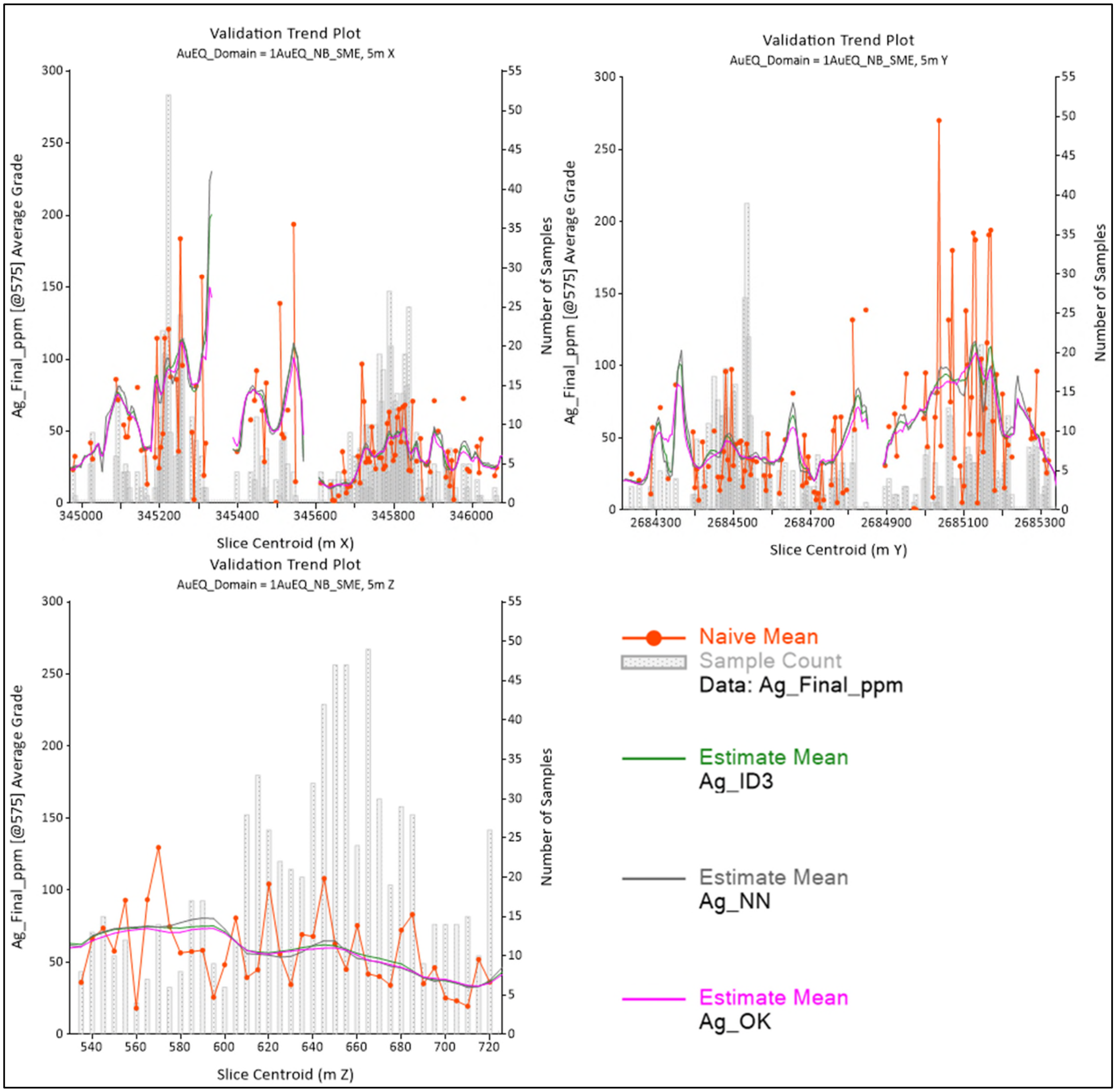


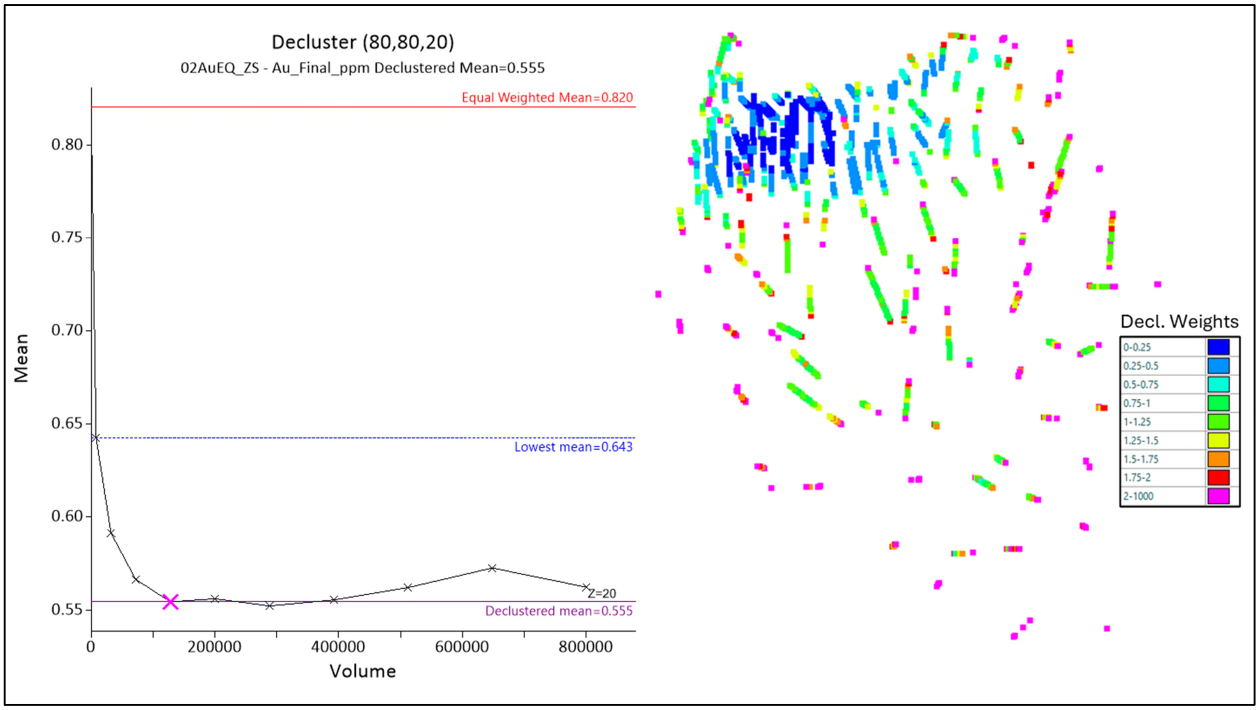
Figure 14-42 Ag Swath plots from the 1AuEQ_NB_SME estimation domain (2.5x2.5x2.5m block model)



Sequential Gaussian Simulation

SGS was completed for mineralized estimation domains in the 5x5x5m set of block models to provide a range of possible grade-tonnage scenarios, to refine OK and ID3 estimation parameters, and to aid in selecting the final estimation method for resource reporting. The simulations were completed using declustered, normal scores transformed data and normal scores variograms for each domain, with simple kriging selected as the estimator. An example showing cell size selection for declustering is shown in Figure 14-43, and the full set of simulation parameters for Au and Ag are presented in Tables 14-27 and 14-28. Simulation results were checked to ensure a mean estimated normal score value close to 0 and a variance close to 1 were achieved in each domain prior to use in validation. Simulation was not completed for domains in the 2.5x2.5x2.5m block models due to software limitations related to models with very large numbers of cells.

Figure 14-43 Cell declustering and weights for the 02AuEQ_ZS estimation domain (5x5x5m block model)



Comparison of the ID3 and OK estimates to SGS grade-tonnage envelopes demonstrates that the ID3 estimate tends to fall between the 5th and 95th ranked simulations (p5-p95) for both grade and tonnes (Figures 14-28 and 14-29). The OK estimates, however, tend to show lower grades than the p5 simulations and higher tonnes than the p95 simulations. This suggests that OK produces an over-smoothed result, and ID3 was therefore selected as the grade variable for final reporting purposes for both Au and Ag.

Table 14-29 Sequential Gaussian Simulation parameters for Au in mineralized estimation domains (5x5x5m block models)

			Block Size			Points Per Block			Search (m)[1]						
Domain[2]	Kriging Type	Number of Simulations	X	Y	Z	X	Y	Z	Major	Semi-Major	Minor	Assign Data to Node?	Min. Samples	Max. Samples	Max. previously simulated nodes
1AuEQ_ESTACA	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_FRE	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_GW	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_LAIJA	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_LP	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_MAR	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_NB_SME	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_SM_SN	Simple	100	5	5	5	2	2	2	80	80	20	N	1	40	20
1AuEQ_SME_SPLAYS	Simple	100	5	5	5	2	2	2	80	80	20	N	1	40	20
1AuEQ_SMW	Simple	100	5	5	5	2	2	2	80	80	15	N	1	40	20
1AuEQ_TA	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_ZN	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_ZS	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20

Notes:

1. Search directions for each domain are taken from Table 14-18, with search dimensions set equal to that of the second search pass used in estimation.
2. Simulations were completed considering Indicated and Inferred resource categories only.

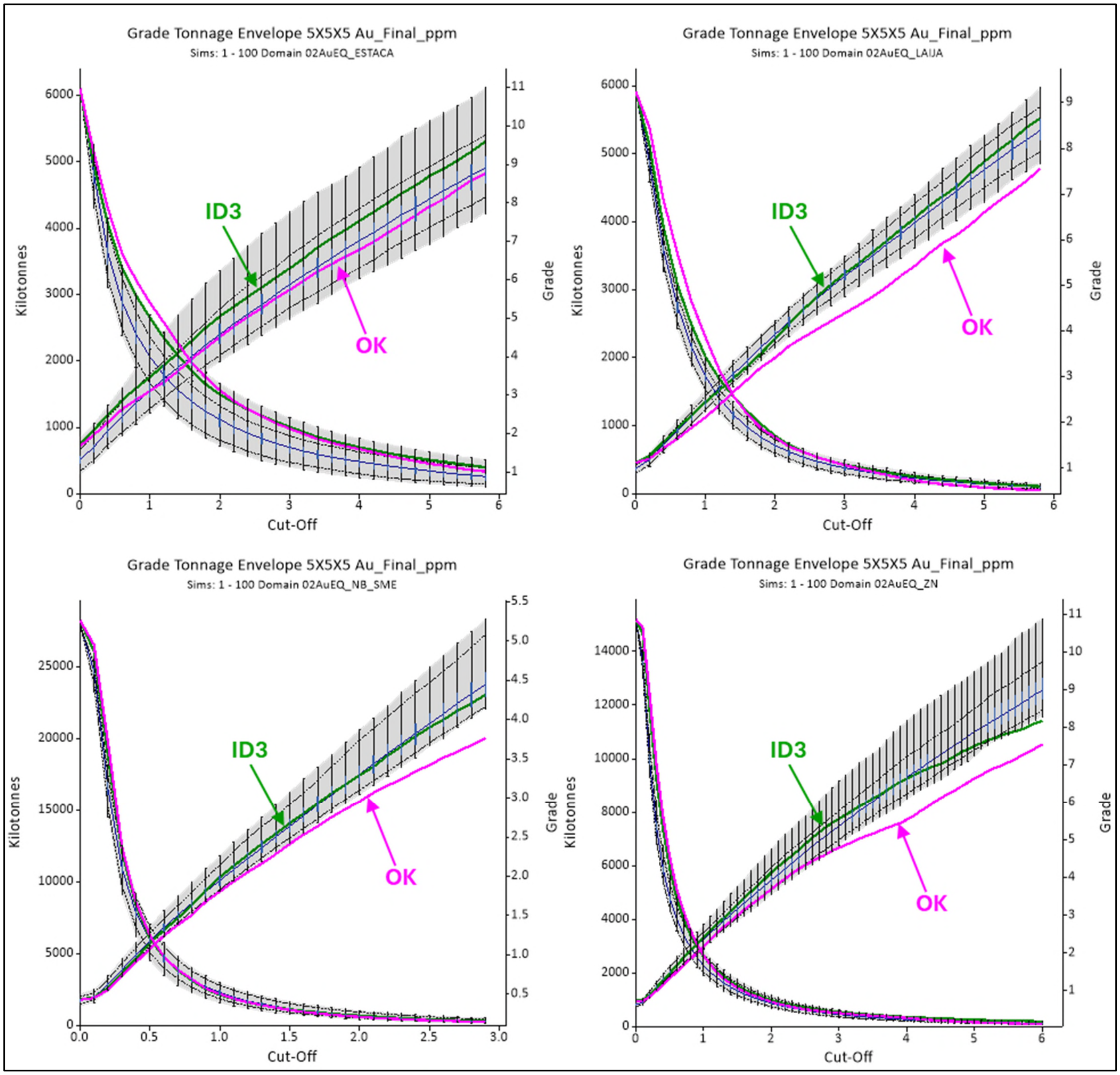
Table 14-30 Sequential Gaussian Simulation parameters for Ag in mineralized estimation domains (5x5x5m block models)

			Block Size			Points Per Block			Search (m)[1]						
Domain[2]	Kriging Type	Number of Simulations	X	Y	Z	X	Y	Z	Major	Semi-Major	Minor	Assign Data to Node?	Min. Samples	Max. Samples	Max. previously simulated nodes
1AuEQ_ESTACA	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_FRE	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_GW	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_LAIJA	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_LP	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_MAR	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_NB_SME	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_SM_SN	Simple	100	5	5	5	2	2	2	80	80	20	N	1	40	20
1AuEQ_SME _SPLAYS	Simple	100	5	5	5	2	2	2	80	80	20	N	1	40	20
1AuEQ_SMW	Simple	100	5	5	5	2	2	2	80	80	15	N	1	40	20
1AuEQ_TA	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_ZN	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20
1AuEQ_ZS	Simple	100	5	5	5	2	2	2	120	90	20	N	1	40	20

Notes:

1. Search directions for each domain are taken from Table 14-19, with search dimensions set equal to that of the second search pass used in estimation.
2. Simulations were completed considering Indicated and Inferred resource categories only.

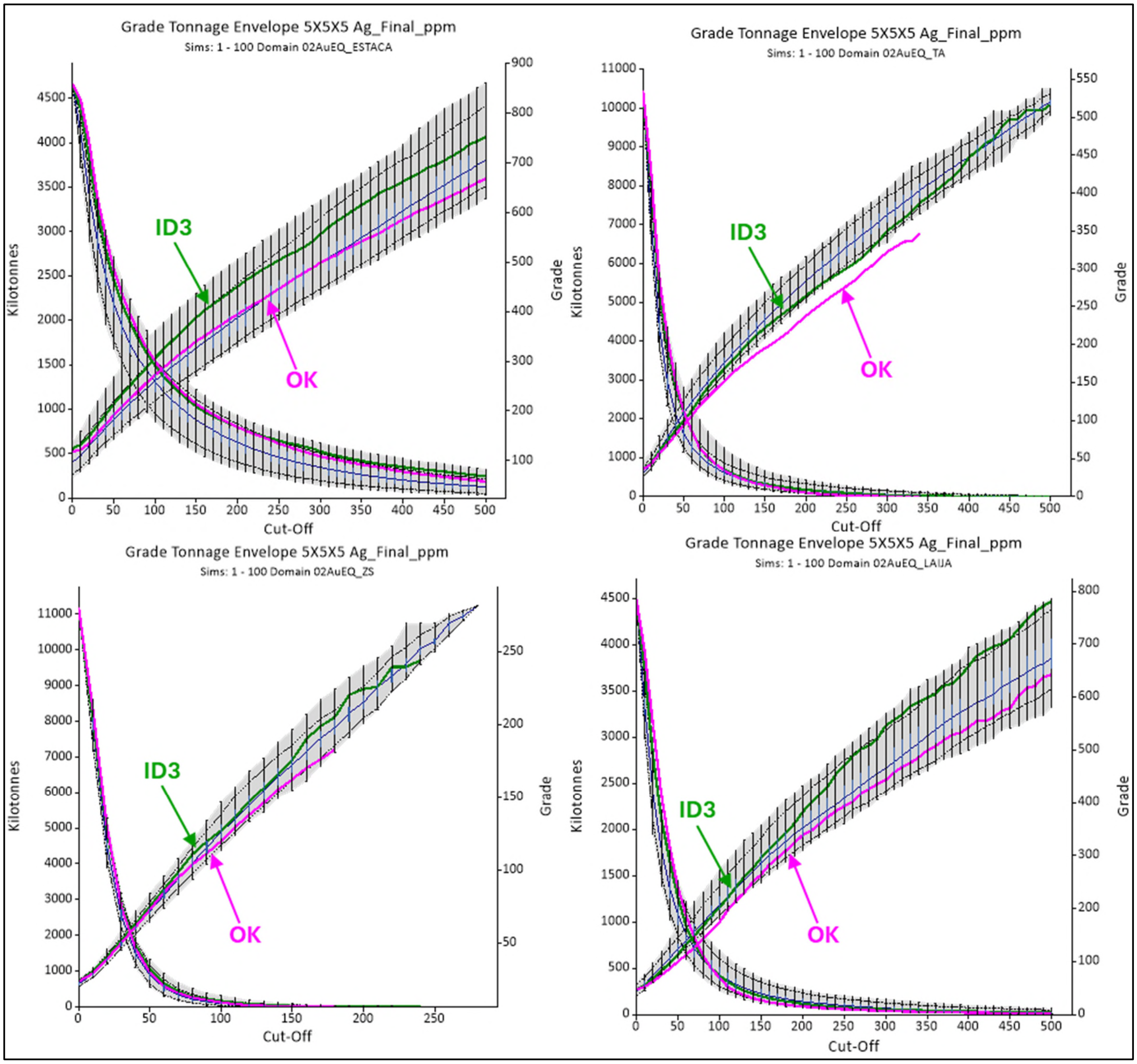
Figure 14-44 Grade-tonnage curve comparison between ID3, OK, and SGS for Au in select mineralized domains



Notes:

The median (p50) simulation is represented by the solid blue line in the center of the grade-tonnage envelope. Dashed lines represent the p5 and p95 simulations.

Figure 14-45 Grade-tonnage curve comparison between ID3, OK, and SGS for Ag in select mineralized domains



Notes:

The median (p50) simulation is represented by the solid blue line in the center of the grade-tonnage envelope. Dashed lines represent the p5 and p95 simulations.

14.3.11 *Assessment of Reasonable Prospects for Eventual Economic Extraction*

Snowden Optiro was commissioned to assist the Company in support of the MRE presented in this report. Three sets of optimization were completed to support the assessment of reasonable prospects for eventual economic extraction of open pit and underground resources – (1) Pit optimization using the 5x5x5m set of block models (Table 14-16), (2) Underground stope optimization with MSO using the 2.5x2.5x2.5m set of block models (Table 14-17), and (3) 'Residual' pit optimization using the 5x5x5m block models, assuming stopes from (2) are mined and backfilled before optimization is completed. Each is described in detail below.

Open Pit Optimization – 5x5x5m Block Models

Open pit optimization was prepared using Datamine Studio NPVS, a strategic mine planning software package that generates an optimized pit shell based on economic input parameters and overall slope angles using the Hochbaum Pseudoflow algorithm. The optimization considers blocks of Indicated and Inferred assurance categories only. The density of the historically mined portion blocks was assumed to be 0.0 g/cm3. Selected pits were computed using the NSR cutoff, which were subsequently filtered to include blocks with grades above the 0.17 g/t gold-only cutoff as stated (or other cutoff grade sensitivities using the same methodology as shown in Table 14-29).

Table 14-31 Pit optimization parameters

Parameter		Unit	Value
Mining	Waste mining cost	$/tonne	2.00
	Ore mining cost[1]	$/tonne	2.50
	Mining loss	%	5
	Mining dilution	%	5
	Slope angle	degrees	42-47 (by zone)
Processing	Heap leach recoveries	%	73% Au, 25% Ag
	Mill recoveries	%	95.6% Au, 81% Ag
	Heap leach cost	$/tonne (ore)	5.53
	Mill cost	$/tonne (ore)	16.81
	General and administration (G&A)	$/tonne (ore)	2.00
Selling	Price[2]	$/oz	1,950 Au, 25.24 Ag
	Selling cost	%	1 (on both Au and Ag)
	Royalty[3]	%	3.00

Notes:

1. Ore mining cost allows for additional haulage distance.
2. Base selling prices of gold and silver are based on three-year trailing averages.
3. Royalty is based on percent of revenue.
4. All costs in United States Dollars (USD).
5. Unless otherwise stated, open pit resources declared in this Technical Report are reported at a gold-only cutoff grade of greater than or equal to 0.17 g/t.

Underground Optimization – 2.5x2.5x2.5m Block Models

Underground optimization was prepared using Datamine Studio's MSO, a strategic mine planning software package used to generate the optimal shape and location of stopes for underground mine design using an input of block model grades or values, economic input assumptions, and stope design parameters. The optimization considers blocks of Indicated and Inferred assurance categories only and assumes a mechanized cut and fill mining method. Blocks which touch or are within historically mined workings were not considered by MSO. Optimization parameters are listed in table 14-30.

Table 14-32 MSO parameters

Parameter		Unit	Value
Mechanized Cut and Fill Mining	Ore mining cost[1]	$/tonne	60.00
	Minimum stope width	metres	4.0
	Stope height	metres	5.0
	Stope length	metres	5.0
	Minimum pillar between stopes in adjacent veins	metres	2.0
	Stope wall dip	degrees	85
	Mining recovery	%	98
	Dilution	-	In design
Processing	Heap leach recoveries	-	N/A
	Mill recoveries	%	95.6% Au, 81% Ag
	Heap leach cost	-	N/A
	Mill cost	$/tonne (ore)	16.81
	General and administration (G&A)	$/tonne (ore)	4.00
Selling	Price[2]	$/oz	1,950 Au, 25.24 Ag
	Selling cost	%	1 (on both Au and Ag)
	Royalty[3]	%	3.00

Notes:

1. Assumes mechanized cut and fill mining.
2. Base selling prices of gold and silver are based on three-year trailing averages.
3. Royalty is based on percent of revenue.
4. All costs in United States Dollars (USD).

Residual Open Pit Optimization – 5x5x5m Block Models with Stopes Backfilled

Prior to residual pit optimization, stopes generated by MSO were first flagged to the 5x5x5m block models using a proportional cell evaluation which records the proportion of a block that falls within a given stope volume. This portion is then assumed to be backfilled with 0 grade material for both Au and Ag, at 2/3 the original rock density. The final estimated grades and density are therefore calculated by the formulas below, where ‘Backfill_Pct’ represents the stoped and backfilled proportion of a 5x5x5m block:

Au_g/t [Final] = Au_g/t [originally estimated] x (1-Backfill_Pct)

Ag_g/t [Final] = Ag_g/t [originally estimated] x (1-Backfill_Pct)

Density_g/cm3 [Final] = (Density [originally assigned] x (1-Backfill_Pct)) + (Density [originally assigned] x (2/3) x (Backfill_Pct))

Residual open pit optimization was then prepared using Datamine Studio NPVS, considering the same optimization parameters as described in table 14-29. The optimization considers blocks of Indicated and Inferred assurance categories only. The selected pits were computed using the NSR cutoff, which were subsequently filtered to include blocks with grades above the 0.17 g/t gold-only cutoff as stated (or other cutoff grade sensitivities using the same methodology as shown in Table 14-29).

Open Pit and Underground Indicated and Inferred Resources

Indicated and Inferred resources for the Project are reported using a combination of economically constrained open pits, underground stopes, and residual open pits generated using the methods described above. Resources for each individual deposit are either sourced from - (1) Pit-constrained resources only, (2) underground MSO-constrained resources only, (3) pit-constrained resources and underground MSO-constrained resources contained in stopes outside the pit volumes, or (4) underground MSO-constrained resources and pit-constrained resources from residual pit optimization. The final reported Indicated and Inferred resources and constituent components for each individual deposit are shown in Tables 14-31 and 14-32 and Figures 14-47 through 14-48.

Table 14-33 Mineral Resource Statement by mining method and process stream

Mining Method and Process	Class	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
Open Pit - Mill	Indicated	24,657	1.13	899	35.7	28,261
	Inferred	7,211	0.89	207	42.8	9,916
Underground - Mill	Indicated	4,132	3.02	402	152.4	20,243
	Inferred	4,055	2.10	273	78.6	10,247
Total Mill	**Indicated**	**28,789**	**1.41**	**1,301**	**52.4**	**48,504**
	Inferred	**11,266**	**1.33**	**480**	**55.7**	**20,163**
Open Pit - Heap Leach	Indicated	20,254	0.29	190	8.4	5,492
	Inferred	5,944	0.30	58	7.3	1,398
Total	**Indicated**	**49,042**	**0.95**	**1,491**	**34.2**	**53,995**
	Inferred	**17,210**	**0.97**	**538**	**39.0**	**21,561**

Notes:

1. Open Pit Resource estimates are based on economically constrained open pits generated using the Hochbaum Pseudoflow algorithm in Datamine's Studio NPVS and the following optimization parameters (all dollar values are in US dollars):
   - $1,950/ounce gold price and $25.24/ounce silver price.
   - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
   - Heap leach recoveries of 73% and 25% for gold and silver, respectively.
   - Pit slopes by area ranging from 42-47 degrees overall slope angle.
   - 5% ore loss and 5% dilution factor applied to the 5 x 5 x 5m open pit resource block models.
   - Mining costs of $2.00 per tonne of waste mined and $2.50 per tonne of ore mined.
   - Milling costs of $16.81 per tonne processed.
   - Heap Leach costs of $5.53 per tonne processed.
   - G&A cost of $2.00 per tonne of material processed.
   - 3% royalty costs and 1% selling costs were also applied.
   - A 0.17 g/t gold only cutoff was applied to ex-pit processed material (which is above the heap-leaching NSR cutoff).
2. Underground Resource estimates are based on economically constrained stopes generated using Datamine's Mineable Shape Optimizer (MSO) algorithm and the following optimization parameters (all dollar values are in US dollars):
   - $1,950/ounce gold price and $25.24/ounce silver price.
   - Mill recoveries of 95.6% and 81% for gold and silver, respectively.
   - Mechanized cut and fill mining with a $60.00 per tonne cost.
   - Diluted to a minimum 4m stope width with a 98% mining recovery.
   - G&A cost of $4.00 per tonne of material processed.
   - Milling costs of $16.81 per tonne processed.
   - 3% royalty costs and 1% selling costs were also applied.
3. Where mentioned, "residual open pits" assumes that any underground stopes are backfilled with zero grade material at two-thirds of the original rock density. Economic-constrained open pits are then estimated with this mined-out, backfilled material in the open pit block selective mining unit ("SMU") model and assuming the resource parameters above.
4. Mineral Resources are not Mineral Reserves (as that term is defined in the CIM Definition Standards) and do not have demonstrated economic viability.

Table 14-34 Mineral Resource Statement by Mining Method and Area

Area	Mining Method	Classification	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
Z-T Trend	Open Pit	Indicated	29,183	0.78	734	21.7	20,316
		Inferred	9,322	0.68	205	29.9	8,957
	Underground	Indicated	2	1.26	0	24.6	2
		Inferred	1,624	1.98	103	78.7	4,110
Guadalupe Trend	Open Pit	Indicated	3,907	0.72	90	24.6	3,094
		Inferred	333	0.40	4	21.5	230
	Underground	Indicated	3,813	2.95	362	158.7	19,452
		Inferred	854	2.34	64	152.9	4,195
Central Trend	Open Pit	Indicated	10,972	0.71	251	28.3	9,977
		Inferred	3,069	0.48	48	20.4	2,018
	Underground	Indicated	135	6.63	29	72.6	316
		Inferred	397	1.44	18	36.3	463
Generative Areas	Open Pit	Indicated	849	0.49	13	13.4	366
		Inferred	431	0.55	8	7.9	110
	Underground	Indicated	182	1.83	11	81.0	473
		Inferred	1,180	2.31	88	39.0	1,479
Total	Open Pit	Indicated	44,910	0.75	1,089	23.4	33,753
		Inferred	13,155	0.63	265	26.8	11,314
	Underground	Indicated	4,132	3.02	402	152.4	20,243
		Inferred	4,055	2.10	273	78.6	10,247
	Total	**Indicated**	**49,042**	**0.95**	**1,491**	**34.2**	**53,995**
		Inferred	**17,210**	**0.97**	**538**	**39.0**	**21,561**

Table 14-35 Description of Resource Components for Tables 14-31 and 14-32, and Figure 14-46

Area	Deposit	Resource Description
Z-T Trend	Zapote-Tahonitas	Revenue Factor 1.0 Open Pits @0.17 g/t Au only cutoff plus remaining economic stopes
Guadalupe Trend	Guadalupe East	Economic underground stopes plus residual economic open pits above @0.17 g/t Au only cutoff
	Guadalupe West	Revenue Factor 1.0 Open Pits @0.17 g/t Au only cutoff
Central Trend	Noche Buena	Revenue Factor 1.0 Open Pits @0.17 g/t Au only cutoff plus remaining economic stopes
	San Miguel East	Revenue Factor 1.0 Open Pits @0.17 g/t Au only cutoff plus remaining economic stopes
	San Miguel West	Economic underground stopes plus residual economic open pits above @0.17 g/t Au only cutoff
Generative Areas	Mariposa	Economic underground stopes
	Las Primas	Economic underground stopes plus residual economic open pits above @0.17 g/t Au only cutoff
	Fresnillo	Economic underground stopes

Figure 14-46 Plan view demonstrating final open pit and underground Resource solids for Los Reyes. Section Lines for Figures 14-47 and 14-48 also shown.

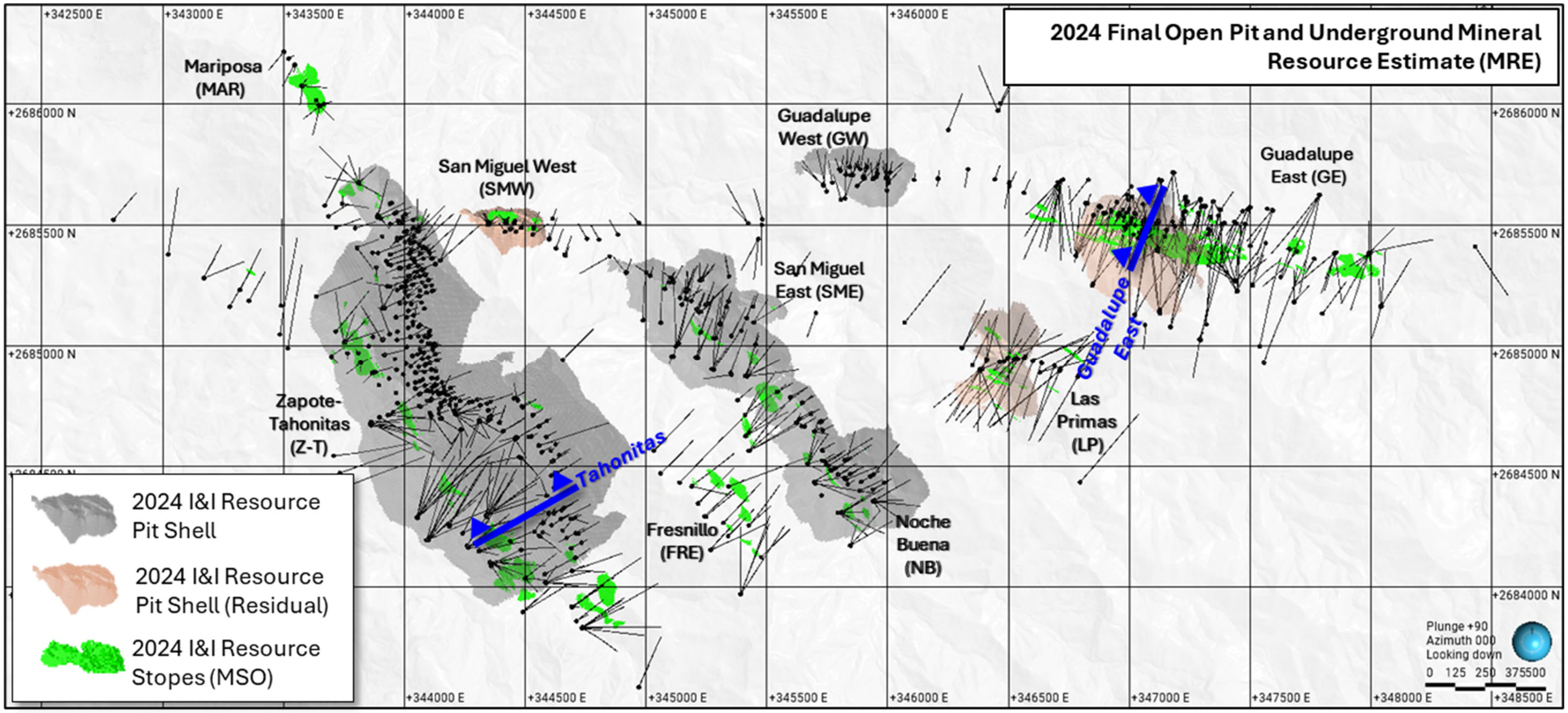


Figure 14-47 Cross section showing underground and residual open pit gold (left) and silver (right) Resources at Guadalupe East.

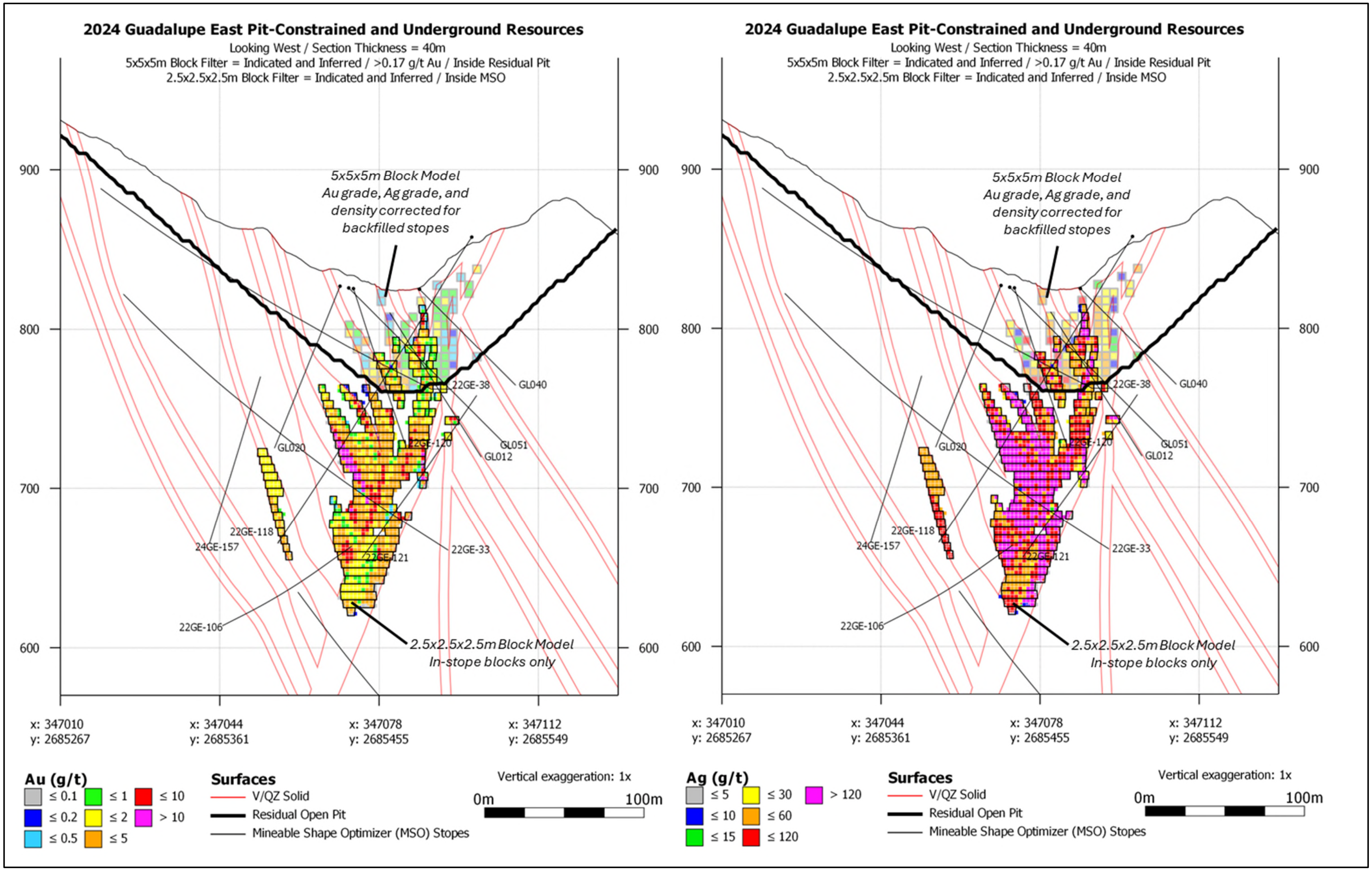


Figure 14-48 Cross section showing open pit and underground gold (left) and silver (right) Resources at Tahonitas.

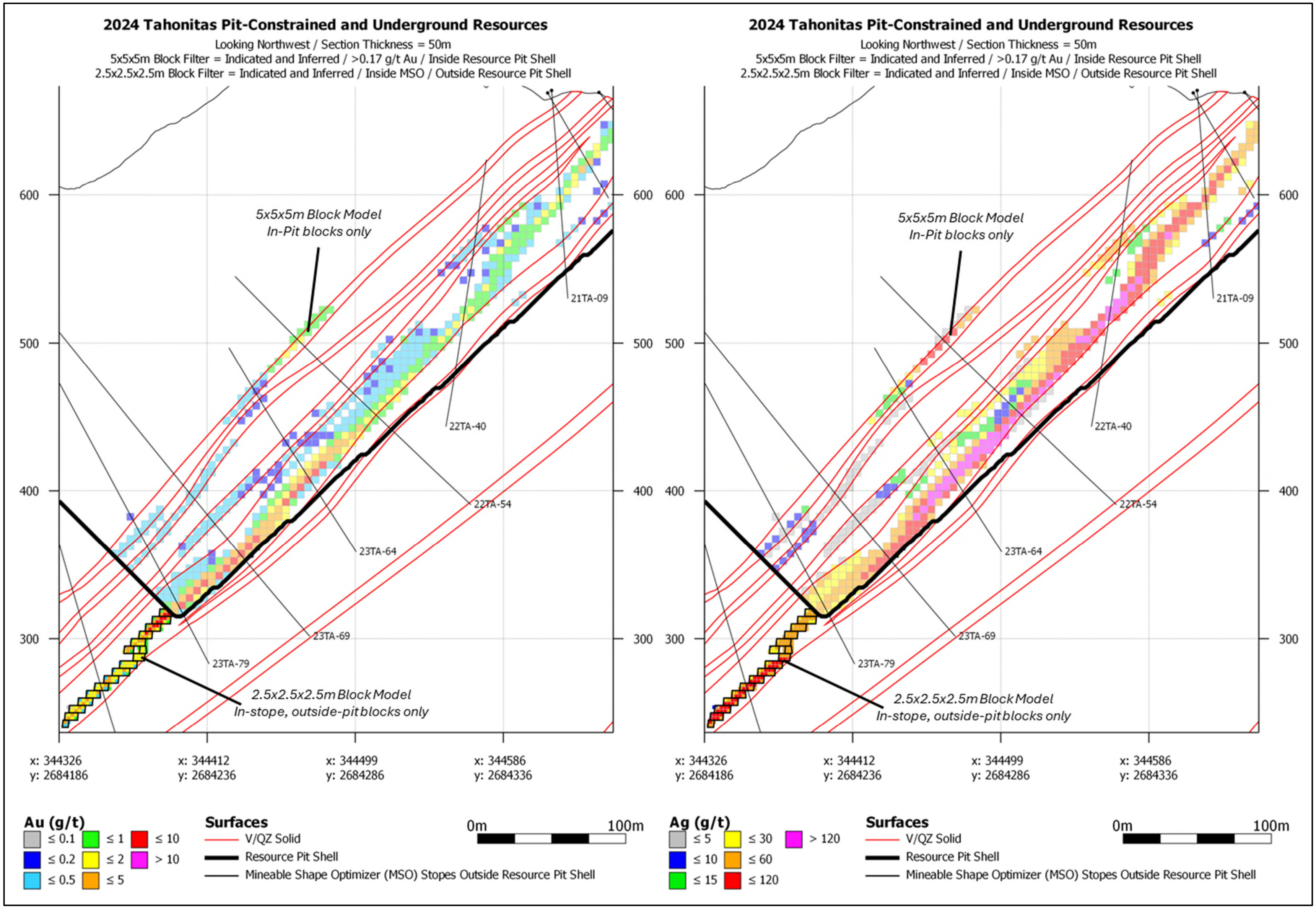
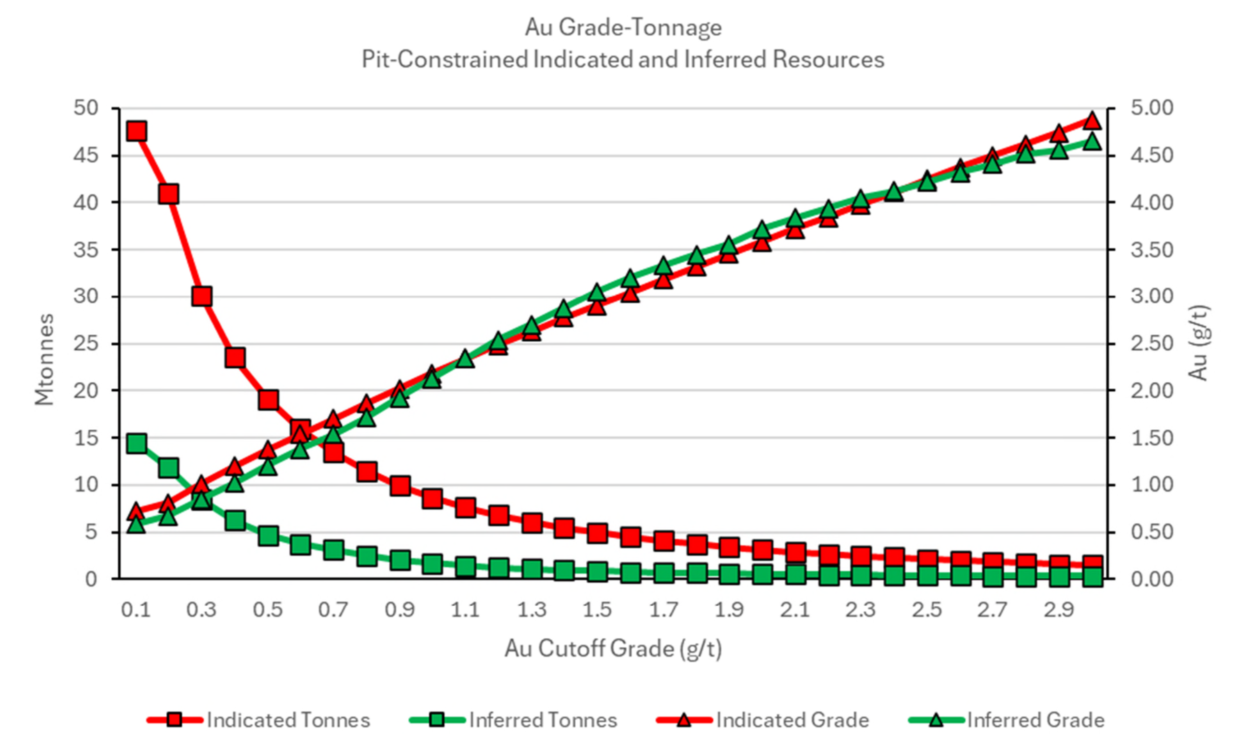


Figure 14-49 Grade-tonnage curves for Los Reyes pit-constrained Indicated and Inferred Resources at various gold-only cutoff grades



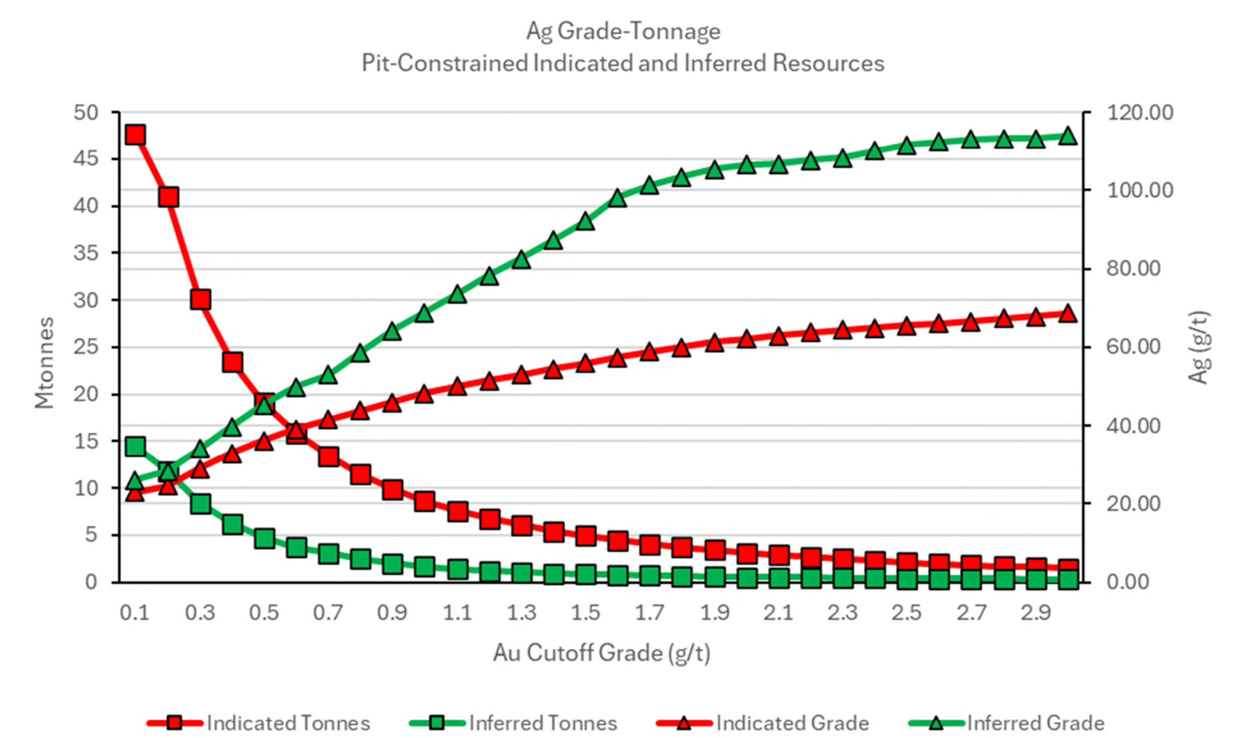
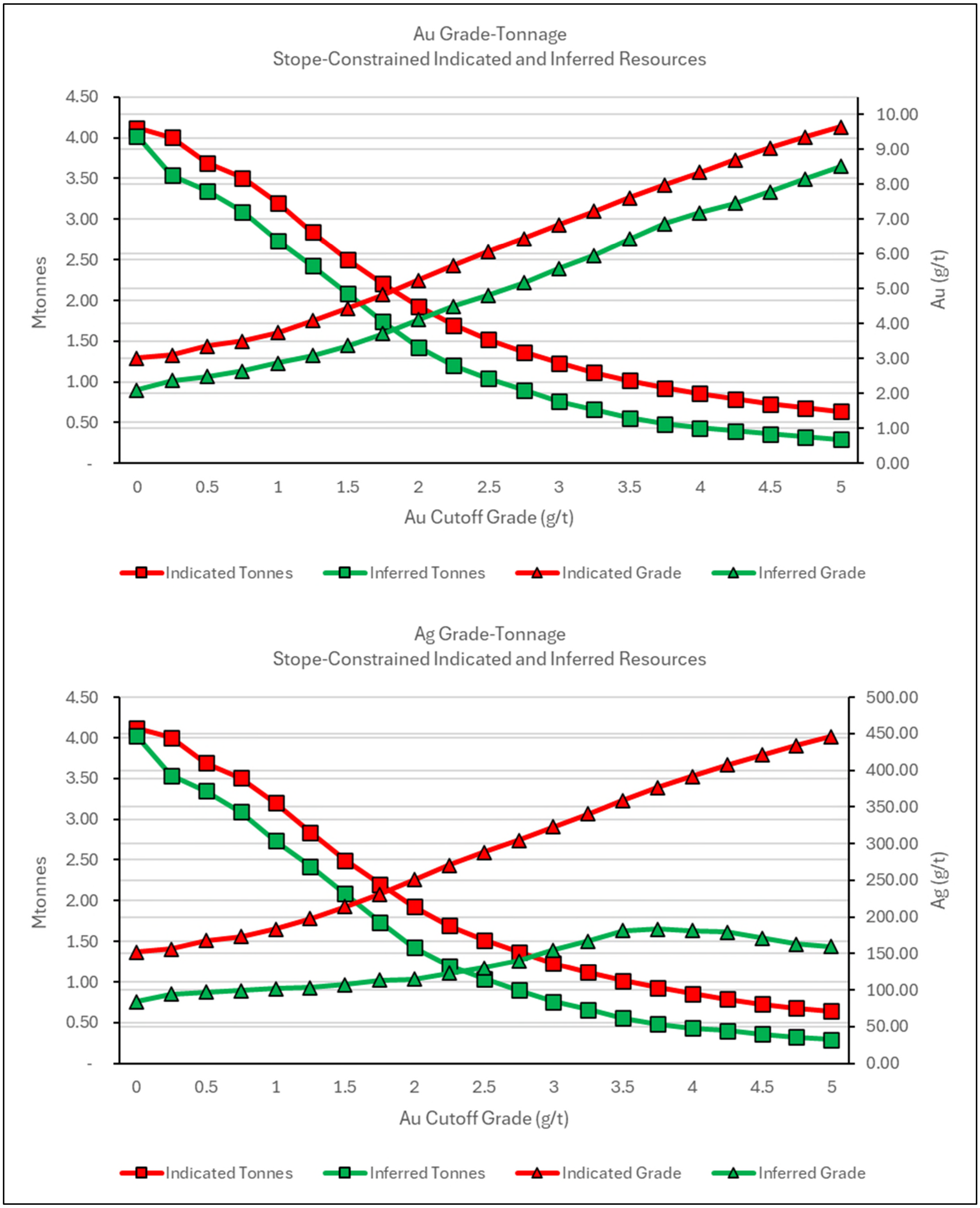


Figure 14-50 Grade-tonnage curves for Los Reyes stope-constrained Indicated and Inferred Resources at various gold-only cutoff grades



Open Pit and Underground Inventory Sensitivity Analysis

The following inventory sensitivities are presented in lieu of, and not in addition to the open pit and underground MRE outlined in Tables 14-1 through 14-3 and 14-31 through 14-33, respectively. They are intended for comparison purposes between underground and open pit optimization methods only. Two scenarios were evaluated – (1) an 'open pit only' scenario, which includes pit-constrained material reported from the 5x5x5m block models, at a 0.17 g/t gold-only cutoff grade, and does not include any stope-constrained material from the 2.5x2.5x2.5m block models, and (2) an 'underground mining prioritized' scenario which includes all material in MSO stopes reported from the 2.5x2.5x2.5m block models, and assumes that residual pits are mined after underground stopes are backfilled (see above for backfill methodology in the 5x5x5m block models). These inventory sensitivities are presented in Tables 14-24 and 14-25 and Figures 14-51 and 14-52.

Figure 14-51 Pit optimization results considering 5x5x5m block models, reported in Table 14-34

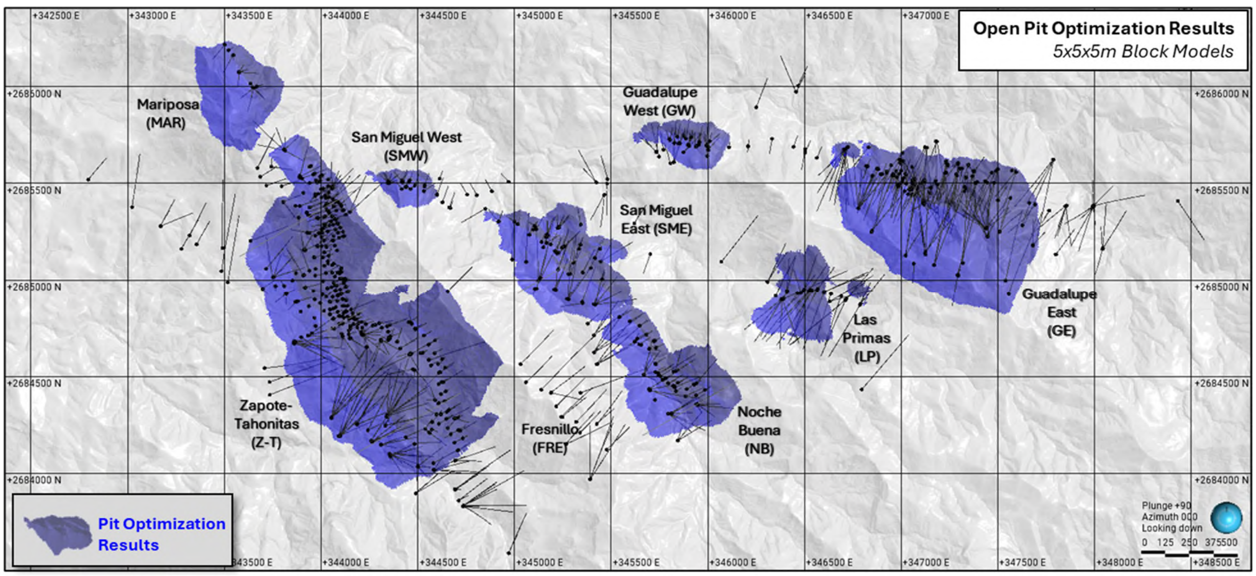


Table 14-36 'open pit only' inventory sensitivity reported from 5x5x5m block models

Area	Mining Method	Processing Method	Classification	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
Z-T	Open Pit	Mill	Indicated	16,016	1.19	611	32.2	16,556
			Inferred	5,516	0.96	171	44.9	7,955
		Heap Leach	Indicated	13,167	0.29	124	8.9	3,760
			Inferred	3,806	0.28	34	8.2	1,001
Guadalupe	Open Pit	Mill	Indicated	8,361	1.82	489	91.4	24,563
			Inferred	192	0.57	4	31.9	197
		Heap Leach	Indicated	2,699	0.28	24	9.8	852
			Inferred	256	0.26	2	8.6	71
Central	Open Pit	Mill	Indicated	5,884	1.19	225	48.4	9,150
			Inferred	1,367	0.67	30	39.3	1,728
		Heap Leach	Indicated	5,205	0.29	49	6.9	1,161
			Inferred	1,707	0.33	18	5.3	289
Generative	Open Pit	Mill	Indicated	726	0.90	21	32.3	753
			Inferred	1,455	1.53	72	16.0	748
		Heap Leach	Indicated	675	0.29	6	7.7	166
			Inferred	1,751	0.32	18	7.8	441
Total	Open Pit	Mill	Indicated	30,986	1.35	1,345	51.2	51,021
			Inferred	8,530	1.00	275	38.8	10,629
		Heap Leach	Indicated	21,747	0.29	203	8.5	5,940
			Inferred	7,520	0.30	73	7.5	1,803

Notes:

1. Inventory sensitivity presented in lieu of, and not in addition to the open pit and underground MRE in Tables 14-1 and 14-31.
2. All open pit inventories are reported at a gold-only cutoff grade of 0.17 g/t.
3. The Guadalupe Trend includes the Guadalupe East and Guadalupe West deposits, the Central Trend includes the Noche Buena, San Miguel East, and San Miguel West deposits, and Generative areas include the Mariposa, Las Primas, and Fresnillo deposits.

Figure 14-52 Underground and residual open pit optimization results considering 2.5x2.5x2.5m and 5x5x5m block models, respectively, reported in Table 14-35

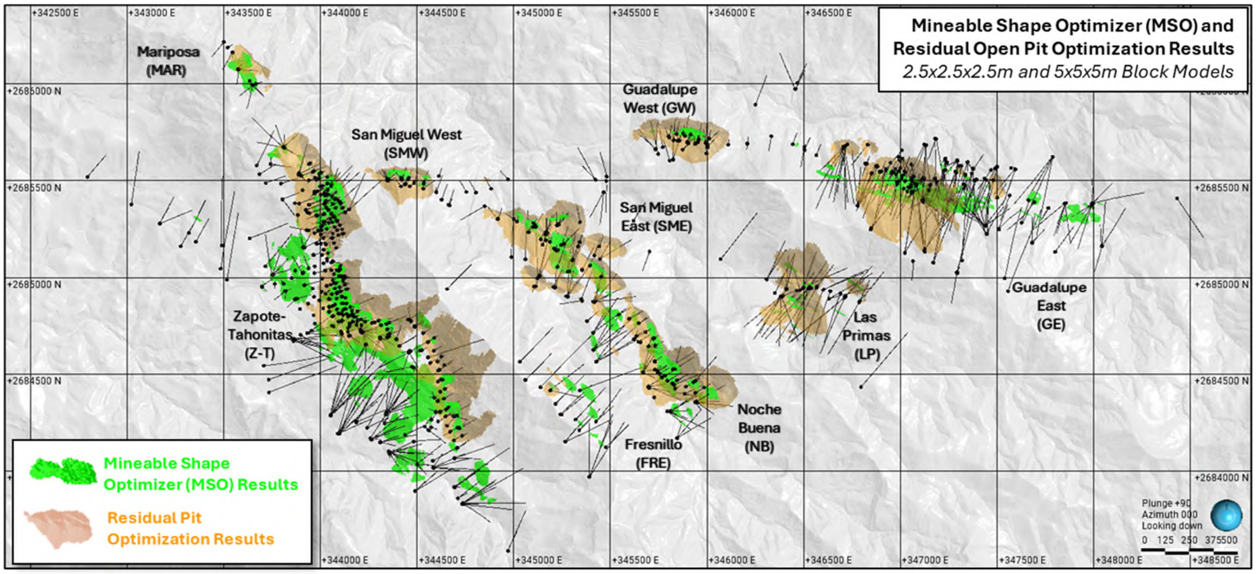


Table 14-37 'underground mining prioritized' inventory sensitivity reported from 2.5x2.5x2.5m and 5x5x5m block models with stopes backfilled

Area	Mining Method	Classification	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
Z-T Trend	Underground	Indicated	2,536	2.47	201	40.7	3,317
		Inferred	5,572	2.17	389	78.2	14,015
	Open Pit (Residual)	Indicated	9,681	0.58	181	12.8	3,987
		Inferred	1,041	0.56	19	15.6	523
Guadalupe Trend	Underground	Indicated	4,117	2.87	380	149.9	19,843
		Inferred	875	2.31	65	150.3	4,228
	Open Pit (Residual)	Indicated	3,549	0.63	71	23.0	2,625
		Inferred	328	0.40	4	21.6	228
Central Trend	Underground	Indicated	1,397	2.61	117	81.8	3,673
		Inferred	1,353	1.72	75	86.6	3,769
	Open Pit (Residual)	Indicated	5,087	0.48	79	17.5	2,865
		Inferred	1,523	0.48	23	16.6	815
Generative Areas	Underground	Indicated	182	1.83	11	81.0	473
		Inferred	1,180	2.31	88	39.0	1,479
	Open Pit (Residual)	Indicated	849	0.49	13	13.4	366
		Inferred	590	0.52	10	8.1	154
Total	Underground	Indicated	8,231	2.7	709	103.2	27,306
		Inferred	8,979	2.1	617	81.4	23,492
	Open Pit (Residual)	Indicated	19,166	0.6	345	16.0	9,842
		Inferred	3,483	0.5	56	15.4	1,721

Notes:

1. Inventory sensitivity presented in lieu of, and not in addition to the open pit and underground MRE in Tables 14-1 and 14-2.
2. All open pit inventories are reported at a gold-only cutoff grade of 0.17 g/t.
3. The Guadalupe Trend includes the Guadalupe East and Guadalupe West deposits, the Central Trend includes the Noche Buena, San Miguel East, and San Miguel West deposits, and Generative areas include the Mariposa, Las Primas, and Fresnillo deposits.
4. Prior to residual pit optimization, stopes generated in MSO are flagged to the 5x5x5m block models and are assumed to be backfilled with 0 g/t Au and Ag grade material at 2/3 the original rock density.

14.3.12 *Comparison to Previous Resource Estimates*

Since the previous MRE released in 2023, the Company has completed significant additional work in the Los Reyes district, including detailed field mapping, geochemical analyses, underground LiDAR surveys, and 86,676m of drilling completed in 255 diamond drillholes across the various deposits with Mineral Resources declared in this Technical Report. This work has resulted in key updates to the MRE methodology for the Project in the following areas:

Dataset – The dataset used for this MRE includes 654 drillholes completed by Prime after acquiring the Property in 2020. Additional improvements to the estimation inputs in 2024 include updated underground workings solids and a full update of the Property's geologic model and estimation domains.

Declaration of Underground Resources – Previous MREs for the Project in 2020 and 2023 considered open pit resources only, while the 2024 MRE considers both open pit and underground resources. Underground Mineral Resources were declared based on stopes generated through Datamine's MSO, considering 2.5x2.5x2.5m sub-blocked block models which were developed using a composite size, domain strategy, and estimation setup appropriate for the smaller underground SMU. 5x5x5m block models were developed independently, with appropriate parameters for the larger open pit SMU, for pit optimization and declaration of open pit Mineral Resources.

Resource Classification – Drillhole spacing for open pit Indicated resources is defined as 40 metres or less in 2024, with drillhole spacing for Inferred resources defined as 40-80 metres. This represents an increase in data spacing for both categories vs. the 2023 MRE (30 metres or less for Indicated data spacing and 30-60 metres for Inferred), driven by greater continuity of Au and Ag mineralization and improved variography within the updated domains used for estimation in the 5x5x5m block models in 2024. Drillhole spacing for underground Indicated resources is defined as 30 metres or less in 2024, with drillhole spacing for Inferred resources defined as 30-60 metres. Neither open pit nor underground Measured resources were declared in 2023 or 2024, given the lack of modern mining and absence of closely spaced data such as grade control drilling in the district which could be used to confirm Measured resources.

Comparisons between the 2023 and 2024 block models and resource pit shells and stopes are outlined in Figures 14-53 through 14-55. The 2024 MRE issued in this Technical Report represents an increase of 486 Koz Au (48%) and 18,975 Koz Ag (54.2%) in the Indicated resource category and an increase of 50 Koz Au (10%) and 3,489 Koz Ag (19%) in the Inferred resource category.

Figure 14-53 Resource pit shell and stope comparison – 2023 vs. 2024

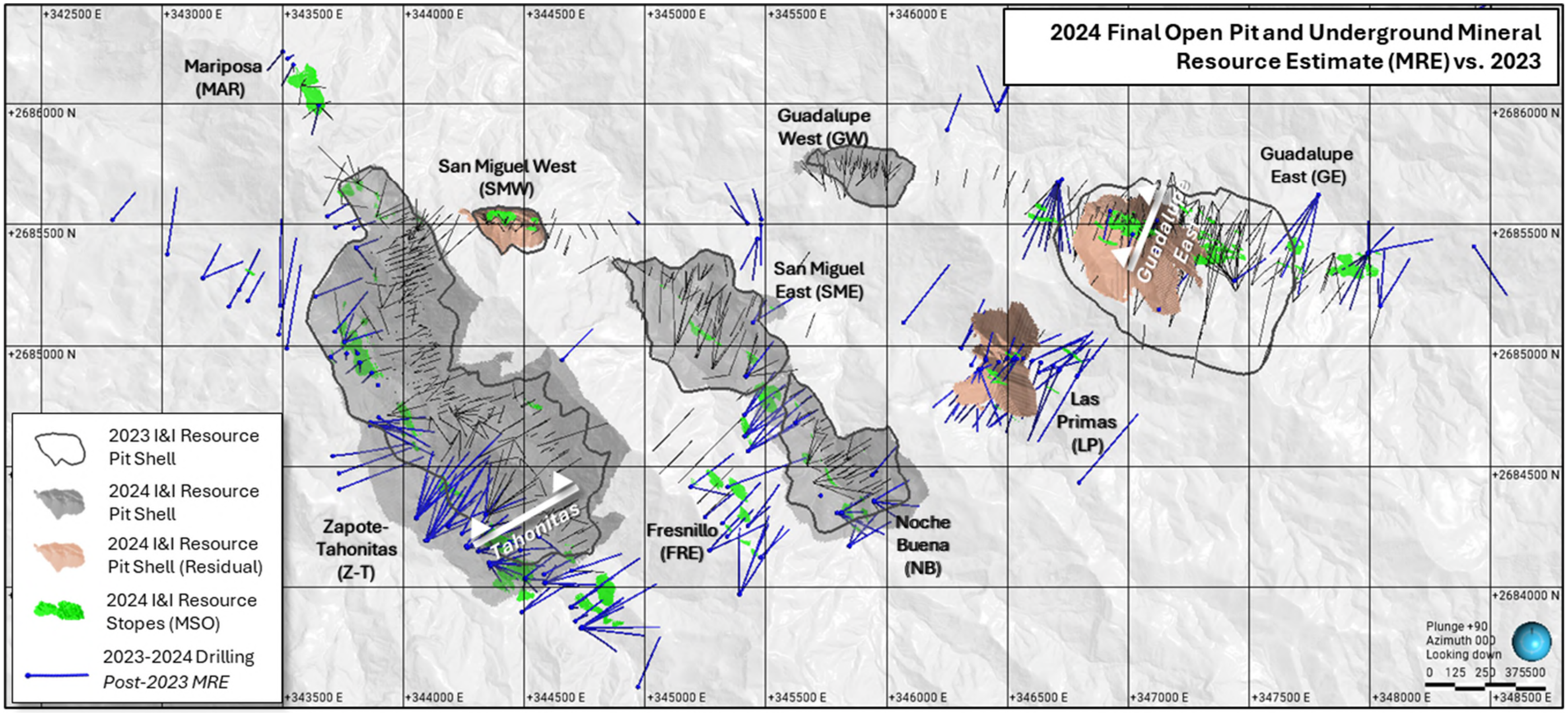


Figure 14-54 Block model section comparison, Tahonitas – 2023 (left) vs. 2024 (right)

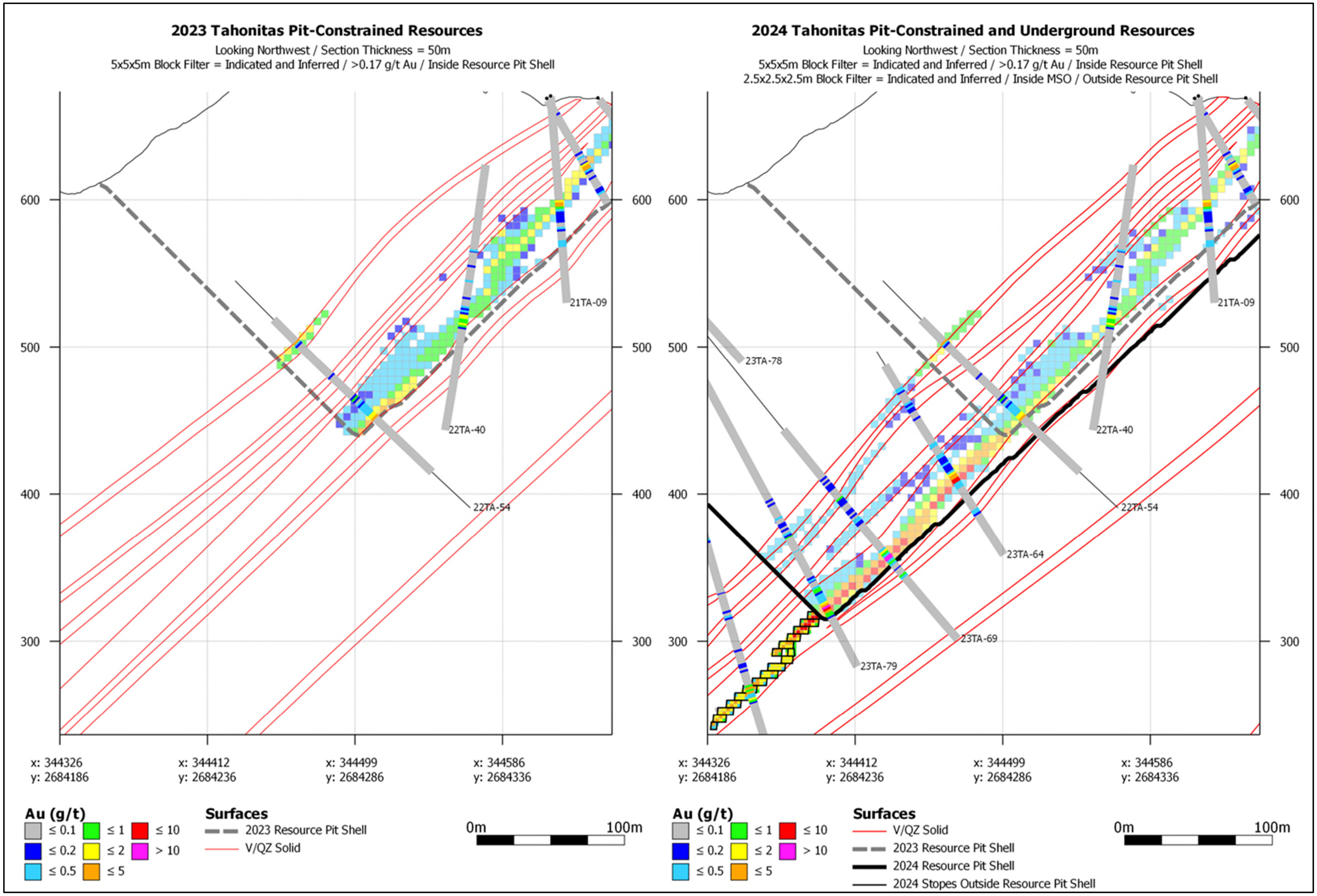
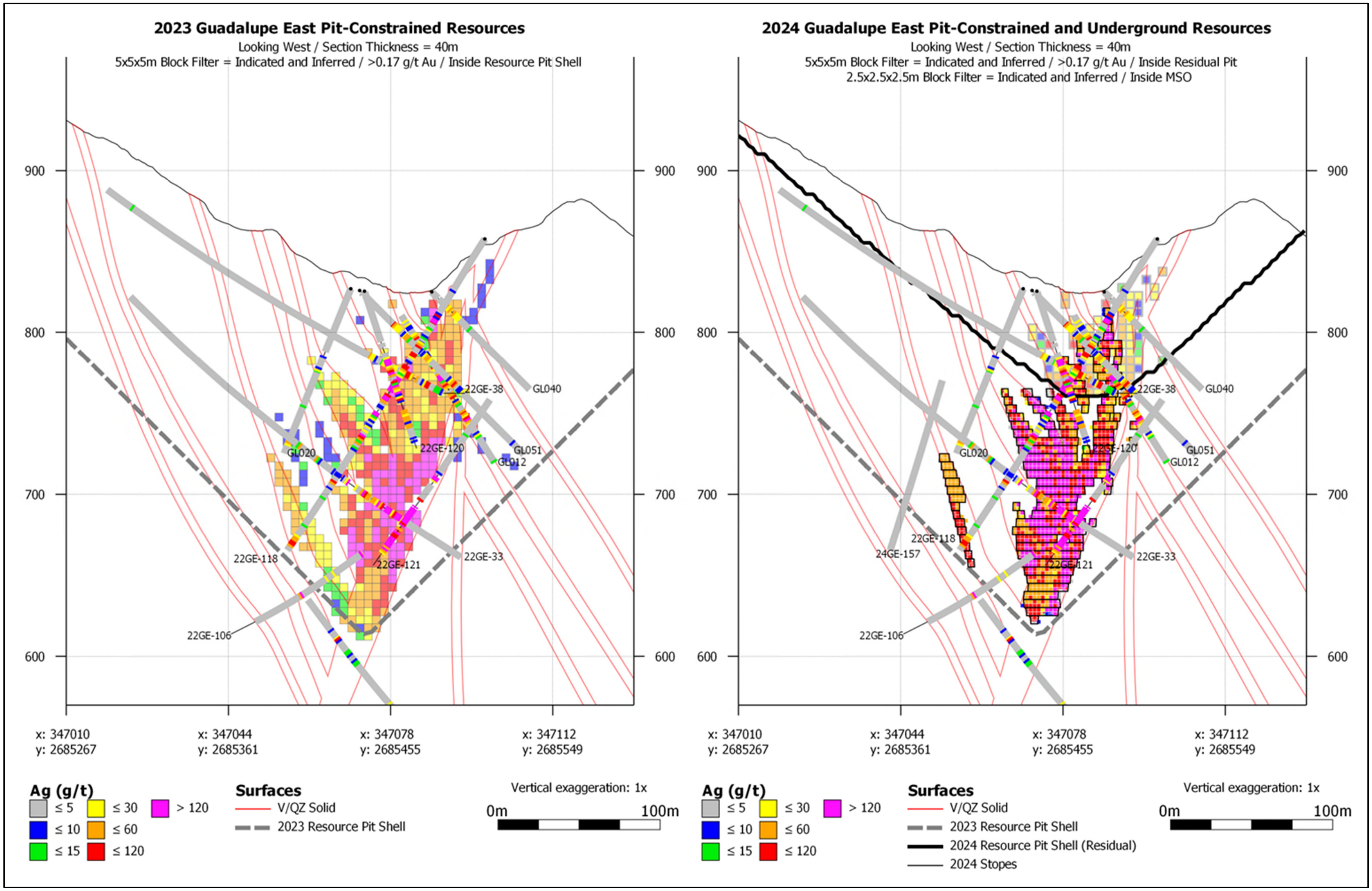


Figure 14-55 Block model section comparison, Guadalupe East – 2023 (left) vs. 2024 (right)



14.4 Comment on Mineral Resources

John Sims, CPG, has certified that, to the best of his professional judgment as a Qualified Person (as defined under NI 43-101), the MREs have been prepared in compliance with NI 43-101, including the CIM Definition Standards incorporated by reference, and conform to generally accepted mining industry best practices. Mineral Resources are not Mineral Reserves and there is no assurance that Mineral Resources will ultimately be classified as Proven or Probable (as those terms are defined in CIM Definition Standards) Mineral Reserves.

The Mineral Resource presented here should be accepted with the understanding that additional data and analysis available after the date of the estimates may necessitate revision. Potential risks that may impact the accuracy of the MRE include the following:

> The geologic interpretation, modelling of geologic attributes such as lithology, faults, and mineralization controls, and the resulting resource estimates were prepared using the most accurate information available at the time this report was completed. However, additional drilling, data collection, and analysis may require revisions to wireframes, interpolation methodologies, density modelling, or other attributes which may impact future MREs.
>
> Commodity price changes and capital and operating cost estimates could impact revenue and cost inputs used in the MRE, and overall economic interpretation of the viability of Project study and development.
>
> The accuracy of historical mine workings cannot be verified in cases where collapse or other unsafe conditions result in limited access to the excavations. Construction of the current depletion solids therefore relied on a combination of LiDAR-surveyed workings where available, voids encountered in surveyed drillholes, and historical production maps. While the work was completed to the highest level of accuracy possible with the current dataset, the position of some underground workings may be inaccurate. Other historical mine workings may also be present which have not been documented.
>
> Future technical studies, including geotechnical and metallurgical, could result in revisions to pit slope angles, underground stope dimensions, and process recovery assumptions.

15. MINERAL RESERVE ESTIMATES

No Mineral Reserves are being declared. This section is not applicable for this level of study.

16. MINING METHODS

This section is not applicable for this level of study.

17. RECOVERY METHODS

This section is not applicable for this level of study.

18. PROJECT INFRASTRUCTURE

This section is not applicable for this level of study.

19. MARKETS AND CONTRACTS

This section is not applicable for this level of study.

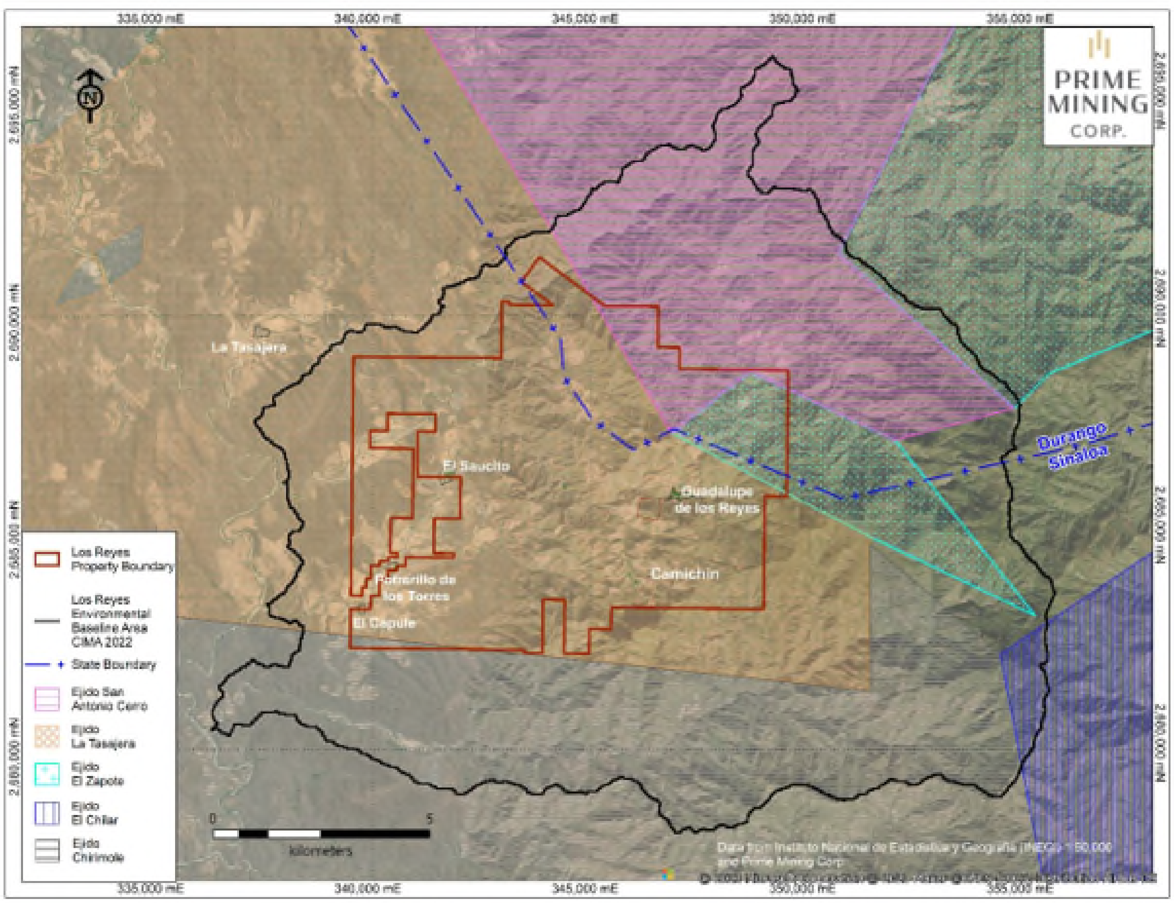
20. ENVIRONMENTAL STUDIES, PERMITTING AND SOCIAL OR COMMUNITY IMPACT

20.1 Environmental Studies

The environmental conditions of the Project area were documented in the environmental baseline study carried out by CIMA in 2022. The study analyzed, characterized, and described the current conditions in which the area of interest is located in order to understand or identify future changes that could be the product of the activities carried out by the Company, and to facilitate future permitting.

The observations made by the Technical Report covered an area of 21,079 ha, which extends beyond the delimitation of the Los Reyes claim area (see Figure 20-1).

Figure 20-1 Environmental Area of Interest



20.1.1 *Geology*

The geology of the area is dominated by sedimentary and extrusive igneous rocks, according to data from the Mexican Geological Survey (SGM).

20.1.2 *Physiography*

The physiography of the area is defined with information from the National Institute of Statistics and Geography (INEGI), which establishes that the environmental system belongs to the SMO province, and Grand Plateau and Durango Canyons subprovince (Gran Meseta y Cañadas Duranguenses).

20.1.3 *Edaphology*

The dominant soils in the area are poorly developed soils, such as leptosol, phaeozem, cambisol and regosol, due to the presence of hard rock at shallow depths.

20.1.4 *Climate*

The climate classification used to describe the area is the modification of García (1973) to the Köpen system (1936). There are 4 climates in the area: Aw0, Aw1, (A)C(w2) and Aw2; all of them warm to semi-warm, sub-humid. The most extensive is Aw1, where the mean annual temperature is above 22°C and the temperature of the coldest month is above 18°C. In the driest month, precipitation ranges from 0 to 60 mm; and during the summer rains the precipitation-temperature ratio varies between 43.2 and 55.3. The percentage of winter rain is between 5 and 10.2% of the annual total.

The wettest month is August, with an average of 487.3 mm of precipitation, and the driest is April with 5.4 mm.

The warmest month is May, with an average temperature of 26.4 °C, and the coldest month is January, with an average temperature of 20.1 °C.

The most frequent meteorological events are: fog, with presence throughout the year that intensifies in July and August; hail from June to September; and thunderstorms from July to September.

20.1.5 *Hydrology*

The availability of surface and groundwater is published by the National Water Commission (CONAGUA), its most recent update was carried out in 2020, from which the following results are obtained: in the surface hydrological scenario, the environmental system is located within the sub-basin Elota River, which has an availability of 92.8 million cubic metres per year. In the groundwater, within the Río Elota aquifer, there is an availability of 13.8 million cubic metres per year.

20.1.6 *Biodiversity*

The Project is in a biotic environment made up of the flora and fauna that inhabits the transition between low deciduous forest to oak and pine-oak forest.

The biodiversity of the environmental system is estimated at 155 species of flora and 68 wild vertebrates. Some of the most important plant species are: crucillo (Randia echinocarpa Sessé & Moc. Ex-DC), cardón (Pachycereus pecten-aboriginum (Engelm.)), Eysenhardtia platycarpa (Pennell & Saff), papelillo (Jatropha cordata (Ortega) Mull.), drago (Croton draco Schltdl), pino amarillo (Pinus oocarpa Schiede), haba (Hura polyandra Baill.), pino escobetón (Pinus devoniana Lindl), mango (Mangifera indica L.), azulillo (Haematoxylum brasiletto Karst.), arrayán (Psidium sartorianum (Berg.) Nied.), cubata (Vachellia campechiana (Mill.) Seigler & Ebinger) and encino amarillo (Quercus magnolifolia Née), among others.

Distinctive faunal species are: opossum, cottontail rabbit, yellow squirrel, coyote, gray fox, raccoon, coati, striped skunk, bobcat, puma, white-tailed deer, Pacific spiny lizard, blue-bellied spiny lizard, green iguana, coastal water snake, Pacific rattlesnake and gray rattlesnake, among others.

Of the plant species, none of those present in the environmental system are within the Mexican protection regulations, only six of them are classified as Appendix II (threatened species with populations that have been greatly reduced, without being in danger of extinction; see Table 2-1) by the Convention on International Trade in Endangered Species of Wild Fauna and Flora (“CITES”): cardón gigante (Pachycereus pecten-aboriginum), nopal duraznillo (Opuntia durangensis), nopal lengua (Opuntia karwinskiana Salm-Dick), nopal de culebra (Opuntia puberula Pfeiffer), nopal chamacuelo (Opuntia tomentosa Salm-Dyck), and xoconostle (Pereskiopsis porteri).

Of the fauna present in the area, six species have some threat status in accordance with NOM-059-SEMARNAT-2010; and 10 species are listed in CITES as Appendix II (Table 20-1).

Table 20-1 Study Area Species of Interest

No.	Technical Name	Common Name	Status	
			NOM-059-SEMARNAT-2010	CITES
1	Lynx rufus Baileyi	Bobcat		AP II
2	Puma concolor azteca	Puma		AP II
3	Leopardus pardalis	Leopard	P	
4	Accipiter cooperi	Dove Hawk	Pr	AP II
5	Buteo jamaicensis	Red Tailed Hawk		AP II
6	Falco sparverius	Falcon		AP II
7	Glaucidium brasilianum	Little Owl		AP II
8	Progne sinaloae	Sinaloan Swallow	Pr	
9	Amazilia violicepes	Violet-headed Hummingbird		AP II
10	Cynanthus latirostris	Thick-billed Hummingbird		AP II
11	Stellula calliope	Stripe-throated Hummingbird		AP II
12	Iguana iguana	Green Iguana	Pr	AP II
13	Crotalus basiliscus	Pacific rattlesnake	Pr	
14	Crotalus lepidus maculosus	Gray Rattlesnake	Pr	

Notes:

P: in danger of extinction.

Pr: subjected to special protection.

AP II: threatened species with populations that have been greatly reduced, although they are not in danger of extinction.

20.1.7 *Cultural Heritage*

In addition to the vegetative and faunal conditions of the area, sites of cultural interest have been evaluated. The town of Guadalupe de Los Reyes is considered a cultural heritage site and is subject to no modifications to its buildings, which include the Chapel of Nuestra Señora de Guadalupe, the cobbled streets, and the facades of the buildings.

20.1.8 *Water Quality Monitoring*

In addition to the environmental baseline, water analysis was carried out in various areas of the Project including at places where residents and the Company take water to carry out their activities. A total of 14 locations were selected, including historical mines/adits, streams and water wells. The sampling is divided into two seasons: prior to the rainy season (June) and after the rainy season (November), to observe changes in the composition of the water. The results show good water quality in accordance with Mexican regulations. The statistical analysis of the stream samples prior to and after the rainy season returned only minor changes in the composition of the water of a number of parameters. On the other hand, the statistical analysis of the mine samples varies only in phosphorus content.

20.2 Permitting Considerations

The Project is located in a vegetative area where low deciduous forest, oak forest, oak-pine forest, and rainfed agriculture develop.

The regulations for the protection, preservation and restoration of the ecological balance are established by LGEEPA.

The current activities of the Project are focused on mining exploration, these are supervised by SEMARNAT, which issues a standard called NOM-120-SEMARNAT-2020, that establishes the environmental protection specifications for this activity.

The statutes that arise in the law and standard previously mentioned, are strictly complied with by the Company, which has received no sanctions from the regulatory entities since the beginning of operations.

Currently, and in accordance with article 28 of the LGEEPA, the Environmental Impact Manifesto (Manifiesto de Impacto Ambiental, MIA) is being developed, which will be submitted in the future to SEMARNAT for approval.

20.3 Social Considerations

The Project is located in the state of Sinaloa, in the northwestern portion of México, within the municipality of Cosalá. Its area of 6,257.78 ha is divided into the Ejidos La Tasajera (88%), San Antonio del Cerro (5%) and Zapote (7%). The ejido acts as a legal entity and is made up of land for production, common or collective use and human settlements.

Being the ejido with the largest presence in Los Reyes, numerous agreements have been carried out with the 302 members of Ejido La Tasajera, for the benefit of the inhabitants and the Company. The entirety of the current stated resources is contained within the Ejido La Tasajera.

The Company signed a contract in 2020 with the ejido, effective for 15 years and renewable for a second 15-year term, where the obligations and rights for both parties are established in order to guarantee access and exploration work without affecting the interests of the tenants. The agreement also makes allowances for compensation during Project construction and operation. This contract originally provided for development on 900 hectares and was doubled to 1,800 hectares in 2023. Also in 2023, Prime signed a 307 hectare surface rights agreement with Ejido San Antonio for current and future activities at the Property, and with same effective years and conditions as Tasajera.

As part of the recognition of the Project, a socioeconomic baseline study was carried out by CIMA, S.C. in 2021, where a quantitative analysis is carried out on the status of the social, economic, environmental and/or institutional aspects of the population in the area.

In response to the results obtained in the socioeconomic baseline, the Company has developed a series of agreements with the ejidatarios.

The main areas in which the Company provides support to the communities are access to water, maintenance of roads and employment.

The Company is committed to distributing water via pipes to the communities during the dry season to supply community storage units. Water harvesting has also been put into practice with the creation and maintenance of small dams. These are carried out in areas of interest to the ejidatarios, from where they satisfy the needs of livestock and croplands.

Some of the communities within the Project have water wells, where the Company can provide pump and pipe maintenance if required.

Gravel road maintenance is an activity that remains active throughout the year and is carried out with heavy machinery. Employment is one of the Company's largest commitments to the community and locals are hired preferentially when possible. It is estimated that 58% of the employees belong to the ejidal community.

21. CAPITAL AND OPERATING COSTS

This section is not applicable for this level of study.

22. ECONOMIC ANALYSIS

This section is not applicable for this level of study.

23. ADJACENT PROPERTIES

The "6 De Enero" claim is privately held and surrounded by Prime's claims along the Guadalupe trend. It is understood that the 6 De Enero claim has not been the focus of recent exploration (see Figure 1-3).

There are several placer claims in an inlier on the western side of the Project that are not part of Prime's Los Reyes claims package. There is no known hard rock mineralization associated with the placer claims.

In March 2021, Prime applied for a claim area ("El Rey") consisting of 7,500 hectares immediately east of the Property (see Figure 1-4 for location). Due to bureaucratic delays, these concessions have not yet been granted.

24. OTHER RELEVANT DATA AND INFORMATION

No additional information relevant to this section is required for this Technical Report.

25. INTERPRETATION AND CONCLUSIONS

Based on the highly prospective geology, size and continuity of the mineralized structural corridors identified to date, including surface mapping and drilling results by both Prime and others, Property mineralization may be much more extensive than currently reported.

The Project contains Indicated and Inferred Mineral Resources that are associated with well-defined mineralized trends. All deposits are generally open along strike and at depth. Prime believes that the Property has the potential for the delineation of additional Mineral Resources within the three main trends and that further additional exploration is warranted on high-priority targets identified from detailed mapping and surface sampling within the Property.

Under the supervision of John Sims of Sims Resources LLC., Independent QP, and based on NI 43-101 definitions and standards, the Project contains the following MRE, as of October 15, 2024:

Table 25-1 Mineral Resource Estimate

Mining Method and Process	Class	Tonnage (kt)	Gold Grade (g/t)	Gold Contained (koz)	Silver Grade (g/t)	Silver Contained (koz)
Open Pit - Mill	Indicated	24,657	1.13	899	35.7	28,261
	Inferred	7,211	0.89	207	42.8	9,916
Underground - Mill	Indicated	4,132	3.02	402	152.4	20,243
	Inferred	4,055	2.10	273	78.6	10,247
Total Mill	**Indicated**	**28,789**	**1.41**	**1,301**	**52.4**	**48,504**
	Inferred	**11,266**	**1.33**	**480**	**55.7**	**20,163**
Open Pit - Heap Leach	Indicated	20,254	0.29	190	8.4	5,492
	Inferred	5,944	0.30	58	7.3	1,398
Total	**Indicated**	**49,042**	**0.95**	**1,491**	**34.2**	**53,995**
	Inferred	**17,210**	**0.97**	**538**	**39.0**	**21,561**

The reported MRE considers contained Au and Ag ounces reported from within economically constrained pits generated using the Hochbaum Pseudoflow algorithm implemented in Datamine's Studio NPVS or underground stope shapes generated using Datamine's MSO, using the following optimization parameters:

- $US1950/ounce gold price and $US25.24/ounce silver price.
- Mill recoveries of 95.6% and 81% for gold and silver, respectively.
- Heap leach recoveries of 73% and 25% for gold and silver, respectively.
- Indicated and Inferred Mineral Resource categories only.
- Economically constrained open pit estimates consider:
    - Pit slopes by area ranging from 42-47 degrees overall slope angle
    - 5% ore loss and 5% dilution factor applied to the 5x5x5m open pit resource block models

  - Mining costs of $2.00 per tonne of waste mined and $2.50 per tonne of ore mined
  - G&A cost of $2.00 per tonne of material processed
  - All open pit material is reported above a 0.17 g/t Au cut-off grade, which is above the NSR estimated cutoff, unless otherwise indicated in a sensitivity table.
  - Where mentioned, a 'residual' open pit assumes that any underground stopes are backfilled with zero-grade material at two-thirds of the original rock density. Economically constrained open pits are then generated with this mined-out, backfilled material flagged to the open pit SMU (5x5x5m) block model. Pit optimization for the residual pits otherwise assumes the parameters described above.
- MSO estimates consider:
  - Mechanized cut and fill mining with a $60.00 per tonne cost
  - Diluted to a minimum 4m stope width with a 98% mining recovery
  - G&A cost of $4.00 per tonne of material processed
- Milling costs of $16.81 per tonne processed and heap leaching costs of $5.53 per tonne processed.
- 3% royalty costs and 1% selling costs were also applied.

This MRE could be influenced by changes in any of the contributing inputs and macroeconomic assumptions used to generate the estimate, including, but not limited to:

1. The geologic interpretation, modelling of geologic attributes such as lithology, faults, and mineralization controls, and the resulting MREs were prepared using the most accurate information available at the time this Technical Report was completed. However, additional drilling, data collection, and analysis may require revisions to wireframes, interpolation methodologies, density modelling, or other attributes which may impact future resource MREs.
2. Commodity price changes and capital and operating cost estimates could impact revenue and cost inputs used in the MRE, and overall economic interpretation of the viability of Project study and development.
3. The accuracy of historical mine workings cannot be verified in cases where collapse or other unsafe conditions result in limited access to the excavations. Construction of the current depletion solids therefore relied on a combination of LiDAR-surveyed workings where available, voids encountered in surveyed drillholes, and historical production maps. While the work was completed to the highest level of accuracy possible with the current dataset, the position of some underground workings may be inaccurate. Other historical mine workings may also be present which have not been documented.
4. Future technical studies, including geotechnical and metallurgical, could result in revisions to slope angle and process recovery assumptions.
5. Changes to the regulatory or permitting environment and laws in México that affect operating or capital costs, taxes, royalties, anticipated environmental compliance regulations, closure costs and obligations among others.

This MRE is not a Mineral Reserve and following NI 43-101 does not have demonstrated economic viability. In addition, based on the metallurgical test work results, the following processing design parameters were recommended by KCA:

- Heap Parameters:
  - Three-stage crushing to 80% passing 6.3 mm for heap leach material
  - 90-day leach cycle
  - Average gold recovery of 73% and silver recovery of 25%
- Mill Parameters:
  - Target grind size of 80% passing 0.037 mm (400 mesh)
  - Gravity concentration with agitated leach on gravity tails
  - Overall mill recoveries of 95.6% for gold and 81% for silver

In general, the various deposits at the Property show amenability to cyanide leaching for the recovery of gold and silver values, with improved recoveries with fine crushing/grinding.

26. RECOMMENDATIONS

26.1 Exploration Program

The Project contains Indicated and Inferred Mineral Resources that are associated with well-defined mineralized trends and models. All deposits are generally open along strike and at depth. Prime believes that the Project has the potential for the delineation of additional Mineral Resources within the three main trends and additional exploration is warranted on new high-priority targets identified from detailed mapping, surface sampling and preliminary drilling within the Property.

The exploration program should include a phased approach of drilling along the extensions (along strike and at depth) of the known deposits (resource drilling) along with drilling other identified high-priority targets (discovery drilling) as well as other key objectives as listed below:

- Continue detailed field mapping and sampling, rock and soil geochemistry along currently defined and possible new structural corridors.
- Completion of the budgeted 2024 drilling program, consisting of resource expansion and generative exploration, totaling approximately 50,000 metres (October 15 Mineral Resource included 30,645 metres of the budgeted 2024 program).
- Drilling in 2025 and beyond will be subject to the Company's overall Project development strategy and the success of its 2024 drilling campaign. A minimum of 20,000 metres is recommended.
- Almost three-quarters of the updated MRE is at the Indicated level of confidence, which is already sufficient for inclusion in a PFS and potential conversion to Mineral Reserves. Prior to commencement of a PEA, exploration should focus on adding resource extensions at the Inferred level of confidence.

26.2 Project Study and Development

Prime should conduct a PEA in order to justify the expenditure required to complete a PFS and declaration of Mineral Reserves. In order to complete this work, Prime should:

- Continue to evaluate mining methods for both open pit and underground mining assessments.
- Optimize potential mineral processing options and flowsheets and continue to advance geochemical domaining to guide further preliminary metallurgical testing on representative samples to identify geometallurgical domains and associated parameters (hardness, abrasiveness, reagent consumption and recovery characteristics).
- Continue to assess infrastructure needs (power, water, tailings, mining waste dumps), and potential locations for these, at a scoping level, in conjunction with continued environmental studies.

- Combine information from above with revised operating and capital cost estimates to evaluate Project economics for one or multiple development scenarios within a PEA.
- Prepare for further engineering and detailed analysis to prepare for an eventual PFS:
  - Advance geotechnical assessments to establish slope angles by pit and pit wall sector as well as underground development and stoping parameters.
  - Begin engineering designs for open pit and underground mine plans
  - Further engineering estimates for select processing methodologies
  - Evaluate trade-off studies with regard to infrastructure, mining and processing
  - Complete infill drilling for economically mineable Inferred ounces to the Indicated category of confidence.
  - Advance permit planning and environmental study work.

26.3 Estimated Exploration and Project Study Budget

The following table is an estimate of costs to complete substantive additional exploration drilling, and completion of a PEA, should the Company choose to pursue further technical study work.

Table 26-1 Estimated Exploration and Project Study costs (2025)

2025	
Activity Type	**Cost ($CAD)**
Field Program • Detailed mapping and sampling along structural corridors and newly exposed access • Exploration drilling (estimated at 20,000m) • Assaying, interpretation and resource modelling, if required	$7.3 M
Technical Work • Additional metallurgical test work and flowsheet development options • Continued geotechnical assessment for design parameters • Evaluation of mining methods and optimization • Power and water assessments • Roadcut and earthworks assessments • Advancing Infrastructure assessment and site layout • Advance permit planning • Review and validate royalties • Capital and operating cost benchmarking	$1.2 M
Contingency	*Included above*
2025 Total ($CDN) including value added taxes:	**$8.5 M**

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28. CERTIFICATES OF QUALIFIED PERSONS

John Sims, CPG

I, John Sims, CPG., do hereby certify that:

a. I am President of Sims Resources LLC, of 945 Wyoming Street Unit 214 Missoula, MT 59801.

b. I am an author of this report entitled "The Los Reyes Project, México" with an effective date of October 15, 2024, prepared for Prime Mining Corp. (the "Technical Report").

c. I am a graduate of University of Montana, in 1992 with a BS Degree(s) in Geology and Mathematics. My relevant experience for the purpose of this Technical Report is:

   I have over 30 years of mining industry experience. My experience with respect to mineral resources and reserves includes resource exploration geologist in Chile, Honduras, Mexico, Tanzania and USA; exploration project manager in Nicaragua; mine site project manager and geologist at underground and open pit mines in western USA, Central and South America; 20 years of resource modelling and reserve optimization experience for deposits in Argentina, Australia, Chile, Bolivia, Ecuador, Ghana, Mauritania, Mexico, Russia, Tanzania and USA. I have 19 years of experience as a site and corporate Qualified Person which includes positions as a Senior Project Mine Geologist, then Director of Technical Services for Coeur d'Alene Mines Corporation, and as Director, then VP & SVP of Technical Services for Kinross Gold Corporation. I have contributed to, and project managed multi-disciplinary teams that required close interaction with mining engineers for mineral reserve estimation, as well as consideration of recovery methods, project infrastructure, costs and economics including Scoping, Prefeasibility and Feasibility studies.

   I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.

d. I am a professional geologist registered with the American Institute of Professional Geologists (AIPG) (License Number: 10924)

e. I visited the Los Reyes Project from November 11 to 16, 2022.

f. I am responsible for the overall preparation of the Technical Report.

g. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.

h. I have had no prior involvement with the property that is the subject of the Technical Report.

i. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.

j. At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

/s/ "John Sims"

John Sims, CPG

President of Sims Resources LLC

November 27, 2024

Damian Gregory, P.Eng.

I, Damian Gregory, state that:

a. I am a Principal Consultant for N. Harris Computer Corporation, DBA Datamine Canada (Snowden Optiro) at A-1300 Kelly Lake Road, Sudbury, Ontario, P3E 5P4, Canada.

b. This certificate applies to the technical report titled "The Los Reyes Project, México" with an effective date of October 15, 2024, prepared for Prime Mining Corp. (the "Technical Report").

c. I am a "qualified person" for the purposes of National Instrument 43-101 (the "Instrument"). My qualifications as a qualified person are as follows:

   i. I am a master's graduate of Laurentian University (2007) and have a bachelor degree from University of Mining and Geology, Bulgaria (1995)

   ii. I am a professional engineer registered in Ontario (License Number: 100107186)

   iii. My relevant mining experience after graduation is over 25 years. My consulting experience with open pit optimization is 15 years.

d. I have not completed a site visit.

e. I am responsible for Item 14.3.11 of the Technical Report.

f. I am independent of the issuer as described in Section 1.5 of the Instrument.

g. I have had no prior involvement with the property that is the subject of this Technical Report.

h. I have read National Instrument 43-101. The part of the Technical Report for which I am responsible has been prepared in compliance with the Instrument; and

i. At the effective date of the Technical Report, to best of my knowledge, information, and belief, the parts of Technical Report for which I am responsible for, contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Signed and dated this November 27, 2024, at St. Catharines, Ontario

/s/ "Damian Gregory"

Damian Gregory, P.Eng
Principal Consultant, Snowden Optiro
November 27, 2024

Chantal Jolette, P.Geo.

I, Chantal Jolette, P. Geo., do hereby certify that:

A. I am President and Principal Geologist with Qualitica Consulting Inc. of 1300 Kelly Lake Road, Unit 3A/C, Sudbury, ON P3E 5P4.
B. I am an author of this report entitled "The Los Reyes Project, Mexico" with an effective date of October 15, 2024 (the "Technical Report"), prepared for Prime Mining Corp. (the "Company").
C. I am a graduate of the University of Ottawa with a B.Sc Degree in Geology. My relevant experience for the purpose of this Technical Report is: Ms Jolette has twenty years of relevant analytical quality control experience in production and exploration environments, and in multiple commodity spaces. She has reviewed the quality assurance and quality control procedures, as well as the results of the control samples for the 2021-2024 drilling at the Los Reyes project (the "Los Reyes Project").
D. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
E. I am a professional geologist registered with Professional Geoscientists Ontario(License Number:1518) and the Ordre des Géologues du Quebec (License Number:02214)
F. I have not visited the Los Reyes Project Site.
G. I am responsible for Section 11 of the Technical Report.
H. I am independent of the Company applying the test set out in Section 1.5 of NI 43-101.
I. I have had no prior involvement with the property that is the subject of the Technical Report.
J. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F.
K. At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

/s/ "Chantal Jolette"

Chantal Jolette, P. Geo.

President and Principal Geologist, Qualitica Consulting Inc.

June 27, 2025

Caleb D. Cook, P.E.

I, Caleb Cook, P.E., do hereby certify that:

a. I am a Project Engineer/Engineering Manager with Kappes, Cassiday & Associates, an independent engineering and metallurgical consulting firm located at 7950 Security Circle, Reno, Nevada 89506.
b. I am an author of this report entitled "The Los Reyes Project, México" with an effective date of October 15, 2024, prepared for Prime Mining Corp. (the "Technical Report").
c. I am a Professional Engineer in the state of Nevada (No. 025803) and my qualifications include experience applicable to the subject matter of the Technical Report. In particular, I am a graduate of the University of Nevada with a B.S. in Chemical Engineering (2010) and have practiced my profession continuously since graduating. Most of my professional practice has focused on the development of gold-silver leaching projects.
d. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
e. I visited the Los Reyes Project on 29 January 2024. During the site visit I met with project personnel, reviewed drill core, discussed metallurgical test work and planned testing and visited proposed processing facilities locations.
f. I am responsible for Section 13 of the Technical Report.
g. I am independent of the Issuer applying the test set out in Section 1.5 of NI 43-101.
h. I have had no prior involvement with the property that is the subject of the Technical Report.
i. I have read NI 43-101, and the Technical Report has been prepared in compliance with NI 43-101 and Form 43-101F1.
j. At the effective date of the Technical Report, to the best of my knowledge, information, and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

/s/ "Caleb Cook"

Caleb Cook, P.E. Chemical Engineering
Project Engineer/Engineering Manager at
Kappes, Cassiday & Associates
November 27, 2024